# LM43602 3.5V 至 36V、2A 同步降压转换器

## 1 特性

- 27μA 稳压静态电流
- 可在轻负载条件下实现高效率（DCM 和 PFM）
- 符合 EN55022/CISPR 22 电磁干扰 (EMI) 标准
- 集成同步整流
- 可调频率范围：200kHz 至 2.2MHz（默认值为 500kHz）
- 与外部时钟频率同步
- 内部补偿
- 与几乎任一陶瓷、固态电解、钽和铝质电容器组合一同工作时保持稳定
- 电源正常标志
- 软启动进入预偏置负载
- 内部软启动：4.1ms
- 可由外部电容器延长的软启动时间
- 输出电压跟踪功能
- 程序系统欠压闭锁 (UVLO) 精确使能
- 具有断续模式的输出短路保护
- 过热关断保护
- 使用 LM43602 并借助 WEBENCH® 电源设计器创建定制设计方案

## 2 应用

- 工业用电源
- 电信系统
- AM 以下波段汽车应用
- 通用宽 $V_{IN}$ 稳压
- 高效负载点稳压

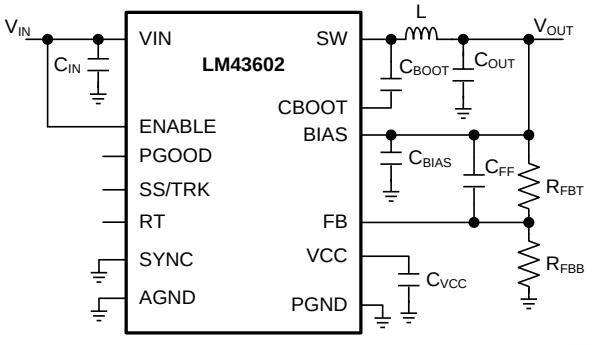
## 3 说明

LM43602 稳压器是一款易于使用的同步降压直流/直流转换器，能够驱动高达 2A 的负载电流，输入电压范围为 3.5V 至 36V（最大绝对值 42V）。LM43602 以极小的尺寸解决方案提供优异的效率、输出精度和压降电压。其扩展系列产品能够以引脚到引脚兼容封装提供 0.5A、1A 和 3A 负载电流选项。此器件采用峰值电流模式控制来实现简单控制环路补偿和逐周期电流限制。可选 功能 包括可编程开关频率、同步、电源正常标志、精确使能、内部软启动、可扩展软启动和跟踪，可为各种 应用提供灵活且易于使用的平台。轻负载时的断续和自动调频模式可提升轻负载效率。此系列只需要很少的外部组件，并且其端子排列方式可确保简单、最优的 PCB 布局。保护 功能 包括热关断、$V_{CC}$ 欠压锁定、逐周期电流限制和输出短路保护。LM43602 器件采用 16 引脚 HTSSOP 封装 (5.1mm × 6.6mm × 1.2mm) 和具有可湿性侧面的 16 引脚 VSON 封装。

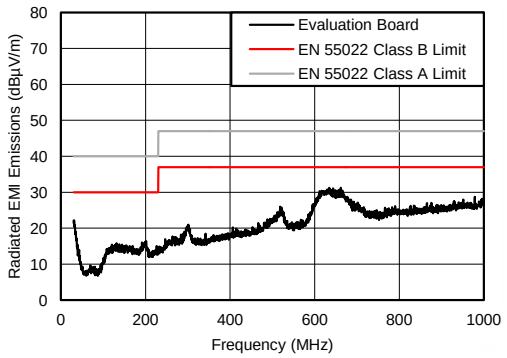
器件信息

| 订货编号 | 封装 | 封装尺寸 |
|---|---|---|
| LM43602 | HTSSOP (16) | 5.10mm x 6.60mm |
| | VSON (16) | 4.10mm × 5.10mm |

简化原理图




**LM43602PWPEVM 辐射发射图**
**$12_{VIN}$ 至 $3.3V_{OUT}$，**
**$F_S$ = 500kHz，$I_{OUT}$ = 2A**



# 目录



## 4 修订历史记录

注：之前版本的页码可能与当前版本有所不同。

**Changes from Revision B (February 2017) to Revision C** **Page**

- 无技术更改，仅做了编辑 ... 1
- Changed *Handling Ratings* to *ESD Ratings* per latest format requirements; move "storage temperature" to *Absolute Maximum Ratings* table ... 4

**Changes from Revision A (April 2014) to Revision B** **Page**

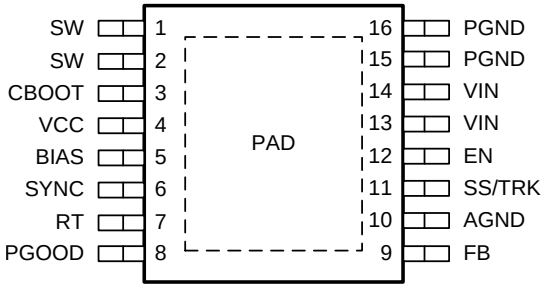
- 已添加 新封装 ... 1
- Added pinout drawing ... 3
- Added pin functions for VSON ... 3
- Updated BIAS Pin Abs Max ... 4
- Updating Recommended Operation Voltage for BIAS ... 4
- Added new Thermal Information (VSON) ... 5
- Changed PGOOD Resistance values on EC Table ... 6
- Updating EN Falling Threshold Figure 13 ... 10
- Updating Figure 14 EN Rising Threshold ... 10
- Updating Figure 15 EN Hysteresis ... 10
- Added Equation 25 ... 28
- Added Equation 26 ... 28

**Changes from Original (April 2014) to Revision A** **Page**

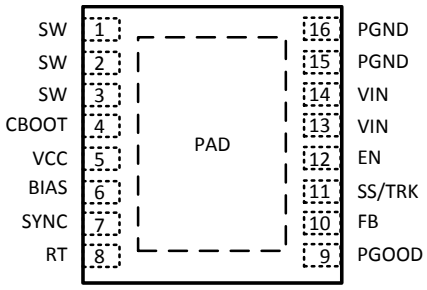
- 已更改 器件从产品预览改为量产数据 ... 1

# 5 Pin Configuration and Functions

**PWP Package**
**16-Pin HTSSOP**
**Top View**




**DSU Package**
**16-Pin VSON**
**Top View**




**Pin Functions**

| PIN | | | TYPE(1) | DESCRIPTION |
|---|---|---|---|---|
| NAME | NUMBER | | | |
| | TSSOP | VSON | | |
| SW | 1,2 | 1,2,3 | P | Switching output of the regulator. Internally connected to both power MOSFETs. Connect to power inductor. |
| CBOOT | 3 | 4 | P | Boot-strap capacitor connection for high-side driver. Connect a high quality 470-nF capacitor from CBOOT to SW. |
| VCC | 4 | 5 | P | Internal bias supply output for bypassing. Connect bypass capacitor from this pin to AGND. Do not connect external loading to this pin. Never short this pin to ground during operation. |
| BIAS | 5 | 6 | P | Optional internal LDO supply input. To improve efficiency, it is recommended to tie to $V_{OUT}$ when 3.3 V ≤ $V_{OUT}$ ≤ 28 V, or tie to an external 3.3 V or 5 V rail if available. When used, place a bypass capacitor (1 to 10 µF) from this pin to ground. Tie to ground when not in use. |
| SYNC | 6 | 7 | A | Clock input to synchronize switching action to an external clock. Use proper high speed termination to prevent ringing. Connect to ground if not used. |
| RT | 7 | 8 | A | Connect a resistor $R_T$ from this pin to AGND to program switching frequency. Leave floating for 500 kHz default switching frequency. |
| PGOOD | 8 | 9 | A | Open drain output for power-good flag. Use a 10 kΩ to 100 kΩ pull-up resistor to logic rail or other DC voltage no higher than 12 V. |
| FB | 9 | 10 | A | Feedback sense input pin. Connect to the midpoint of feedback divider to set $V_{OUT}$. Do not short this pin to ground during operation. |
| AGND | 10 | — | G | Analog ground pin. Ground reference for internal references and logic. Connect to system ground. |
| SS/TRK | 11 | 11 | A | Soft-start control pin. Leave floating for internal soft-start slew rate. Connect to a capacitor to extend soft start time. Connect to external voltage ramp for tracking. |
| EN | 12 | 12 | A | Enable input to the internal LDO and regulator. High = ON and low = OFF. Connect to VIN, or to VIN through resistor divider,or to an external voltage or logic source. Do not float. |
| VIN | 13,14 | 13,14 | P | Supply input pins to internal LDO and high side power FET. Connect to power supply and bypass capacitors $C_{IN}$. Path from VIN pin to high frequency bypass $C_{IN}$ and PGND must be as short as possible. |
| PGND | 15,16 | 15,16 | G | Power ground pins, connected internally to the low side power FET. Connect to system ground, PAD, AGND, ground pins of $C_{IN}$ and $C_{OUT}$. Path to $C_{IN}$ must be as short as possible. |
| PAD | — | — | — | Low impedance connection to AGND. Connect to PGND on PCB. Major heat dissipation path of the die. Must be used for heat sinking to ground plane on PCB. |

(1) P = Power, A = Analog, G = Ground

# 6 Specifications

## 6.1 Absolute Maximum Ratings(1)

over the recommended operating junction temperature ($T_J$) range of –40°C to +125°C (unless otherwise noted)

| | PARAMETER | MIN | MAX | UNIT |
|---|---|---|---|---|
| Input voltages | VIN to PGND | –0.3 | 42(2) | V |
| | EN to PGND | –0.3 | VIN + 0.3 | |
| | FB, RT, SS/TRK to AGND | –0.3 | 3.6 | |
| | PGOOD to AGND | –0.3 | 15 | |
| | SYNC to AGND | –0.3 | 5.5 | |
| | BIAS to AGND | –0.3 | 30 or $V_{IN}$(3) | |
| | AGND to PGND | –0.3 | 0.3 | |
| Output voltages | SW to PGND | –0.3 | $V_{IN}$ + 0.3 | V |
| | SW to PGND less than 10-ns transients | –3.5 | 42 | |
| | CBOOT to SW | –0.3 | 5.5 | |
| | VCC to AGND | –0.3 | 3.6 | |
| Operating junction temperature $T_J$ | | –40 | 125 | °C |
| Storage temperature, $T_{stg}$ | | –65 | 150 | °C |

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
(2) At maximum duty cycle of 0.01%
(3) Whichever is lower

## 6.2 ESD Ratings

| | | | VALUE | UNIT |
|---|---|---|---|---|
| $V_{(ESD)}$ | Electrostatic discharge | Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001(1) | ±1000 | V |
| | | Charged-device model (CDM), per JEDEC specification JESD22-C101(2) | ±500 | |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

## 6.3 Recommended Operating Conditions(1)

over the recommended operating junction temperature ($T_J$) range of –40°C to +125°C (unless otherwise noted)

| | PARAMETER | MIN | MAX | UNIT |
|---|---|---|---|---|
| Input voltages | VIN to PGND | 3.5 | 36 | V |
| | EN | –0.3 | $V_{IN}$ | |
| | FB | –0.3 | 1.1 | |
| | PGOOD | –0.3 | 12 | |
| | BIAS input not used | –0.3 | 0.3 | |
| | BIAS input used | 3.3 | 28 or $V_{IN}$(2) | |
| | AGND to PGND | –0.1 | 0.1 | |
| Output voltage | $V_{OUT}$ | 1 | 28 | V |
| Output current | $I_{OUT}$ | 0 | 2 | A |
| Temperature | Operating junction temperature range, $T_J$ | –40 | 125 | °C |

(1) Operating Ratings indicate conditions for which the device is intended to be functional, but do not ensure specific performance limits. For ensured specifications, see *Electrical Characteristics*.
(2) Whichever is lower

## 6.4 Thermal Information

| THERMAL METRIC (1)(2) | | LM43602 | | UNIT |
|---|---|---|---|---|
| | | HTSSOP | VSON | |
| | | (16 PINS) | (16 PINS) | |
| $R_{\theta JA}$ | Junction-to-ambient thermal resistance | 38.9 (3) | 31.3 | °C/W |
| $R_{\theta JC(top)}$ | Junction-to-case (top) thermal resistance | 24.3 | 22.8 | °C/W |
| $R_{\theta JB}$ | Junction-to-board thermal resistance | 19.9 | 9.6 | °C/W |
| $\psi_{JT}$ | Junction-to-top characterization parameter | 0.7 | 0.2 | °C/W |
| $\psi_{JB}$ | Junction-to-board characterization parameter | 19.7 | 9.6 | °C/W |
| $R_{\theta JC(bot)}$ | Junction-to-case (bottom) thermal resistance | 1.7 | 1.3 | °C/W |

(1) The package thermal impedance is calculated in accordance with JESD 51-7.
(2) Thermal Resistances were simulated on a 4 layer, JEDEC board.
(3) See Figure 64 for $\theta_{JA}$ vs Copper Area Curve.

## 6.5 Electrical Characteristics

Limits apply over the recommended operating junction temperature ($T_J$) range of –40°C to +125°C, unless otherwise stated. Minimum and Maximum limits are specified through test, design or statistical correlation. Typical values represent the most likely parametric norm at $T_J$ = 25°C, and are provided for reference purposes only. Unless otherwise stated, the following conditions apply: $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz.

| PARAMETER | | CONDITIONS | MIN | TYP | MAX | UNIT |
|---|---|---|---|---|---|---|
| **SUPPLY VOLTAGE (VIN PIN)** | | | | | | |
| $V_{IN-MIN-ST}$ | Minimum input voltage for start-up | | | | 3.8 | V |
| $I_{SHDN}$ | Shutdown quiescent current | $V_{EN}$ = 0 V | | 1.2 | 3.1 | µA |
| $I_{Q-NONSW}$ | Operating quiescent current (non-switching) from $V_{IN}$ | $V_{EN}$ = 3.3 V<br>$V_{FB}$ = 1.5 V<br>$V_{BIAS}$ = 3.4 V external | | 5 | 10 | µA |
| $I_{BIAS-NONSW}$ | Operating quiescent current (non-switching) from external $V_{BIAS}$ | $V_{EN}$ = 3.3 V<br>$V_{FB}$ = 1.5 V<br>$V_{BIAS}$ = 3.4 V external | | 85 | 130 | µA |
| $I_{Q-SW}$ | Operating quiescent current (switching) | $V_{EN}$ = 3.3 V<br>$I_{OUT}$ = 0 A<br>$R_T$ = open<br>$V_{BIAS}$ = $V_{OUT}$ = 3.3 V<br>$R_{FBT}$ = 1.0 Meg | | 27 | | µA |
| **ENABLE (EN PIN)** | | | | | | |
| $V_{EN-VCC-H}$ | Voltage level to enable the internal LDO output $V_{CC}$ | $V_{ENABLE}$ high level | 1.2 | | | V |
| $V_{EN-VCC-L}$ | Voltage level to disable the internal LDO output $V_{CC}$ | $V_{ENABLE}$ low level | | | 0.525 | V |
| $V_{EN-VOUT-H}$ | Precision enable level for switching and regulator output: $V_{OUT}$ | $V_{ENABLE}$ high level | 2 | 2.2 | 2.42 | V |
| $V_{EN-VOUT-HYS}$ | Hysteresis voltage between $V_{OUT}$ precision enable and disable thresholds | $V_{ENABLE}$ hysteresis | | –290 | | mV |
| $I_{LKG-EN}$ | Enable input leakage current | $V_{EN}$ = 3.3 V | | 0.85 | 1.75 | µA |
| **INTERNAL LDO (VCC and BIAS PINS)** | | | | | | |
| $V_{CC}$ | Internal LDO output voltage $V_{CC}$ | $V_{IN}$ ≥ 3.8 V | | 3.28 | | V |
| $V_{CC-UVLO}$ | Undervoltage lock out (UVLO) thresholds for $V_{CC}$ | $V_{CC}$ rising threshold | | 3.1 | | V |
| | | Hysteresis voltage between rising and falling thresholds | | –520 | | mV |
| $V_{BIAS-ON}$ | Internal LDO input change over threshold to BIAS | $V_{BIAS}$ rising threshold | | 2.94 | 3.15 | V |
| | | Hysteresis voltage between rising and falling thresholds | | –75 | | mV |

## Electrical Characteristics (continued)

Limits apply over the recommended operating junction temperature ($T_J$) range of –40°C to +125°C, unless otherwise stated. Minimum and Maximum limits are specified through test, design or statistical correlation. Typical values represent the most likely parametric norm at $T_J$ = 25°C, and are provided for reference purposes only. Unless otherwise stated, the following conditions apply: $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz.

| PARAMETER | | CONDITIONS | MIN | TYP | MAX | UNIT |
|---|---|---|---|---|---|---|
| **VOLTAGE REFERENCE (FB PIN)** | | | | | | |
| $V_{FB}$ | Feedback voltage | $T_J$ = 25ºC | 1.004 | 1.011 | 1.018 | V |
| | | $T_J$ = –40ºC to 85ºC | 0.994 | 1.011 | 1.026 | |
| | | $T_J$ = –40ºC to 125ºC | 0.994 | 1.011 | 1.030 | |
| $I_{LKG-FB}$ | Input leakage current at FB pin | FB = 1 V | | 0.2 | 65 | nA |
| **THERMAL SHUTDOWN** | | | | | | |
| $T_{SD}$ (1) | Thermal shutdown | Shutdown threshold | | 160 | | °C |
| | | Recovery threshold | | 150 | | °C |
| **CURRENT LIMIT AND HICCUP** | | | | | | |
| $I_{HS-LIMIT}$ | Peak inductor current limit | | 3.65 | 4.5 | 5.15 | A |
| $I_{LS-LIMIT}$ | Inductor current valley limit | | 1.75 | 2 | 2.25 | A |
| **SOFT START (SS/TRK PIN)** | | | | | | |
| $I_{SSC}$ | Soft-start charge current | | 1.25 | 2 | 2.75 | µA |
| $R_{SSD}$ | Soft-start discharge resistance | UVLO, TSD, OCP, or EN = 0 V | | 18 | | kΩ |
| **POWER GOOD (PGOOD PIN)** | | | | | | |
| $V_{PGOOD-HIGH}$ | Power-good flag overvoltage tripping threshold | % of FB voltage | | 110% | 113% | |
| $V_{PGOOD-LOW}$ | Power-good flag undervoltage tripping threshold | % of FB voltage | 77% | 88% | | |
| $V_{PGOOD-HYS}$ | Power-good flag recovery hysteresis | % of FB voltage | | 6% | | |
| $R_{PGOOD}$ | PGOOD pin pulldown resistance when power bad | $V_{EN}$ = 3.3 V | | 69 | 150 | Ω |
| | | $V_{EN}$ = 0 V | | 150 | 350 | |
| **MOSFETS (2)** | | | | | | |
| $R_{DS-ON-HS}$ | High-side MOSFET ON-resistance | $I_{OUT}$ = 1 A<br>$V_{BIAS}$ = $V_{OUT}$ = 3.3 V | | 120 | | mΩ |
| $R_{DS-ON-LS}$ | Low-side MOSFET ON-resistance | $I_{OUT}$ = 1 A<br>$V_{BIAS}$ = $V_{OUT}$ = 3.3 V | | 65 | | mΩ |

(1) Specified by design
(2) Measured at the pins

## 6.6 Timing Requirements

| | | MIN | NOM | MAX | UNIT |
|---|---|---|---|---|---|
| **CURRENT LIMIT AND HICCUP** | | | | | |
| $N_{OC}$ | Hiccup wait cycles when LS current limit tripped | | 32 | | Cycles |
| $T_{OC}$ | Hiccup retry delay time | | 5.5 | | ms |
| **SOFT START (SS/TRK PIN)** | | | | | |
| $T_{SS}$ | Internal soft-start time when SS pin open circuit | | 4.1 | | ms |
| **POWER GOOD (PGOOD PIN)** | | | | | |
| $T_{PGOOD-RISE}$ | Power-good flag rising transition deglitch delay | | 220 | | µs |
| $T_{PGOOD-FALL}$ | Power-good flag falling transition deglitch delay | | 220 | | µs |

## 6.7 Switching Characteristics

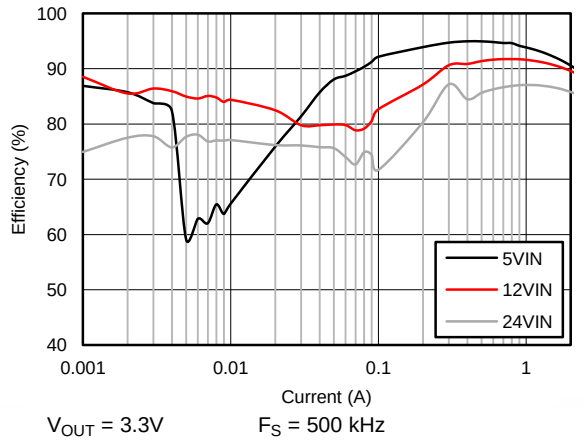
over operating free-air temperature range (unless otherwise noted)

| PARAMETER | | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|---|---|---|---|---|---|---|
| **SW (SW PIN)** | | | | | | |
| $t_{ON-MIN}$ (1) | Minimum high side MOSFET ON-time | | | 125 | 165 | ns |
| $t_{OFF-MIN}$ (1) | Minimum high side MOSFET OFF-time | | | 200 | 250 | ns |
| **OSCILLATOR (SW and SYNC PINS)** | | | | | | |
| $F_{OSC-DEFAULT}$ | Oscillator default frequency | RT pin open circuit | 425 | 500 | 580 | kHz |
| $F_{ADJ}$ | Minimum adjustable frequency | With 1% resistors at RT pin | | 200 | | kHz |
| | Maximum adjustable frequency | | | 2200 | | kHz |
| | Frequency adjust accuracy | | | 10% | | |
| $V_{SYNC-HIGH}$ | Sync clock high level threshold | | 2 | | | V |
| $V_{SYNC-LOW}$ | Sync clock low level threshold | | | | 0.4 | V |
| $D_{SYNC-MAX}$ | Sync clock maximum duty cycle | | | 90% | | |
| $D_{SYNC-MIN}$ | Sync clock minimum duty cycle | | | 10% | | |
| $T_{SYNC-MIN}$ | Mininum sync clock ON and OFF time | | | 80 | | ns |

(1) Specified by design

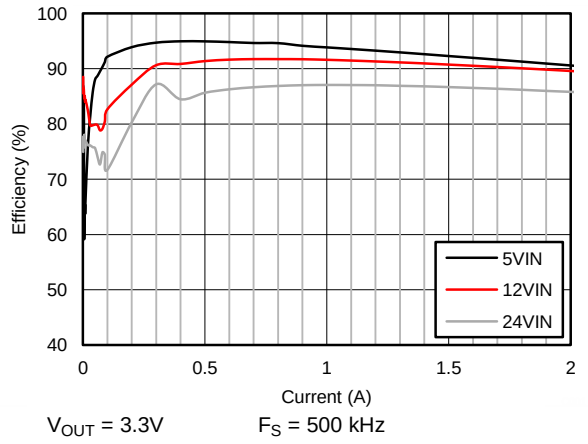
## 6.8 Typical Characteristics

Unless otherwise specified, $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz, L = 6.8 µH, $C_{OUT}$ = 120 µF, $C_{FF}$ = 100 pF. See *Application Performance Curves* for Bill of materials for other $V_{OUT}$ and $F_S$ combinations.



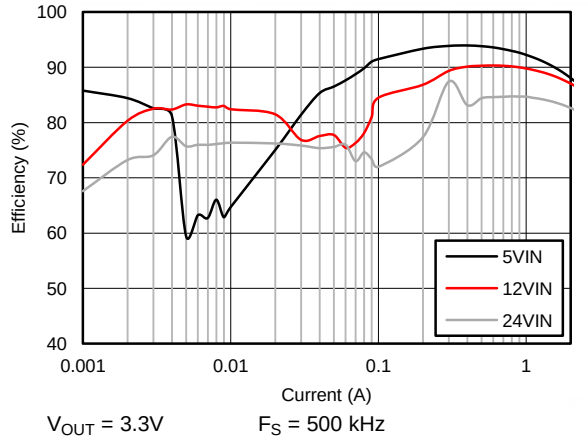

$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 1. Efficiency at Room Temperature**



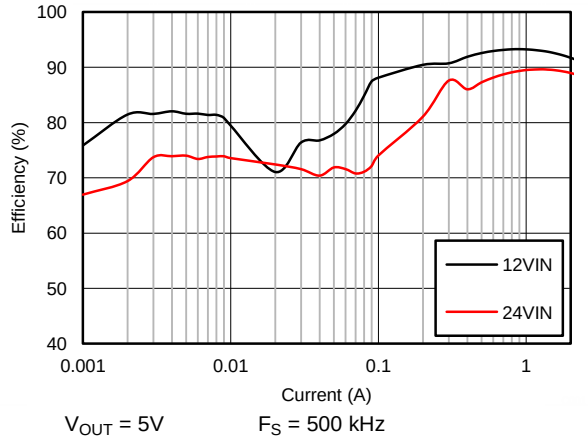

$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 2. Efficiency at Room Temperature**



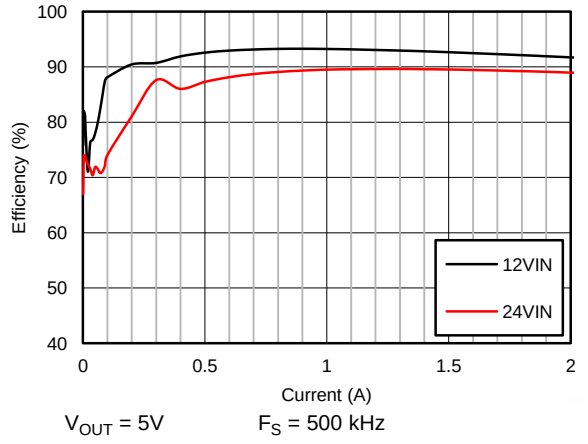

$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 3. Efficiency at 85°C**



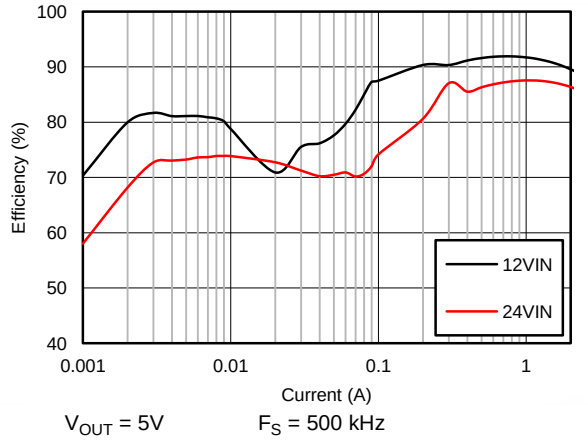

$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 4. Efficiency at Room Temperature**




$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 5. Efficiency at Room Temperature**

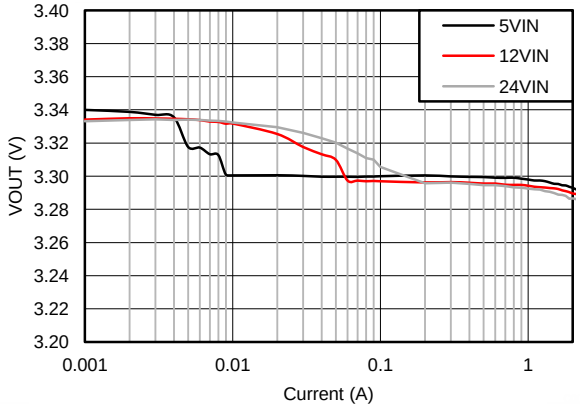



$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 6. Efficiency at 85°C**

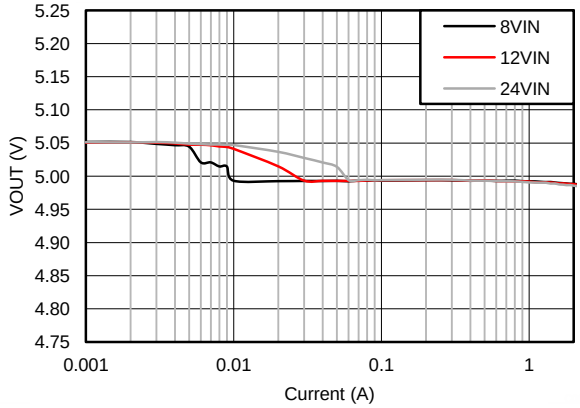
## Typical Characteristics (continued)

Unless otherwise specified, $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz, L = 6.8 µH, $C_{OUT}$ = 120 µF, $C_{FF}$ = 100 pF. See *Application Performance Curves* for Bill of materials for other $V_{OUT}$ and $F_S$ combinations.



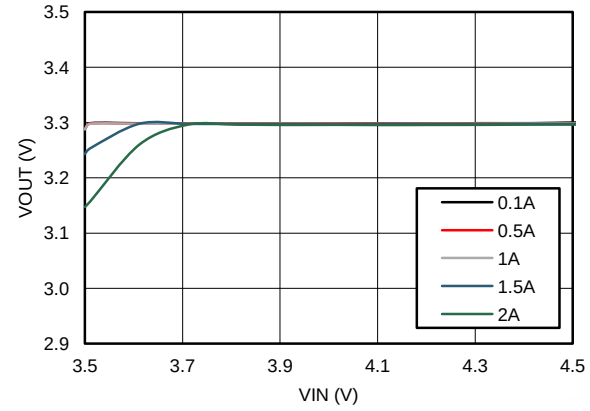

$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 7. $V_{OUT}$ Regulation**



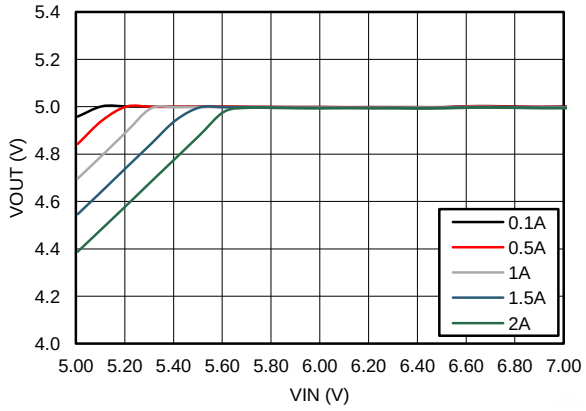

$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 8. $V_{OUT}$ Regulation**



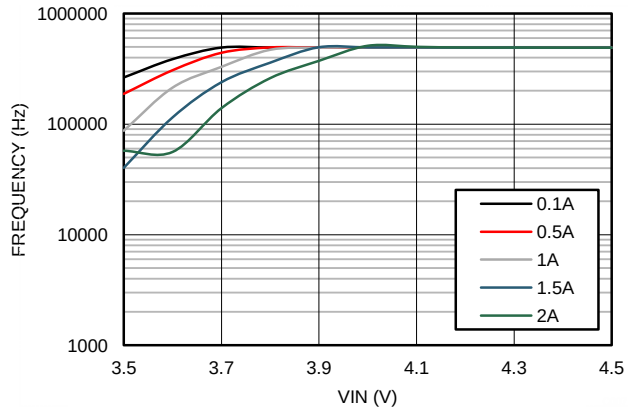

$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 9. Dropout Curve**



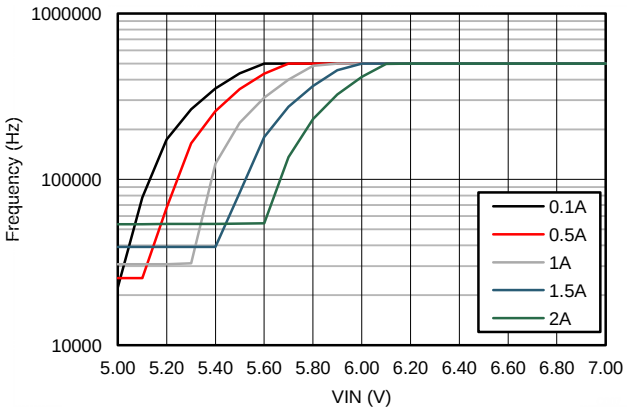

$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 10. Dropout Curve**




$V_{OUT}$ = 3.3V $F_S$ = 500 kHz

**Figure 11. Frequency vs VIN**




$V_{OUT}$ = 5V $F_S$ = 500 kHz

**Figure 12. Frequency vs VIN**

## Typical Characteristics (continued)

Unless otherwise specified, $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz, L = 6.8 µH, $C_{OUT}$ = 120 µF, $C_{FF}$ = 100 pF. See *Application Performance Curves* for Bill of materials for other $V_{OUT}$ and $F_S$ combinations.

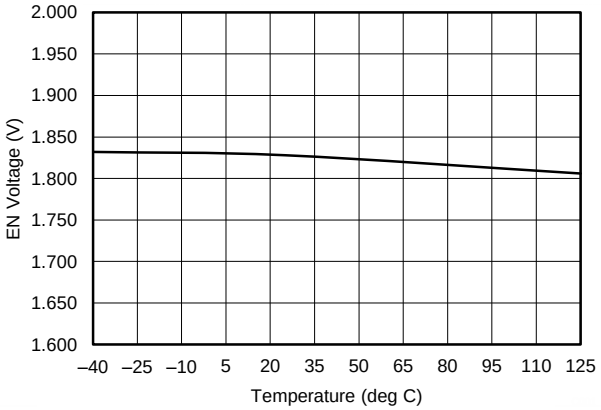



**Figure 13. EN Falling Threshold vs Junction Temperature**

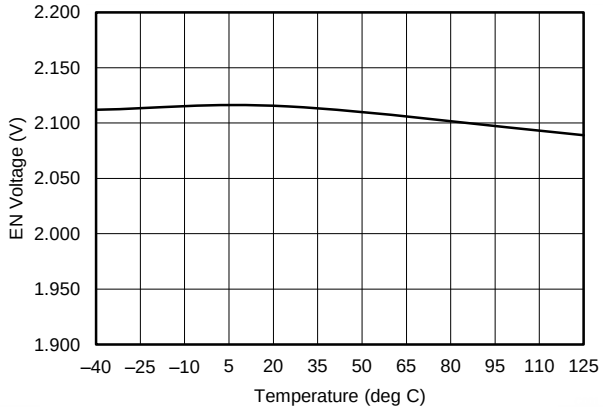



**Figure 14. EN Rising Threshold vs Junction Temperature**

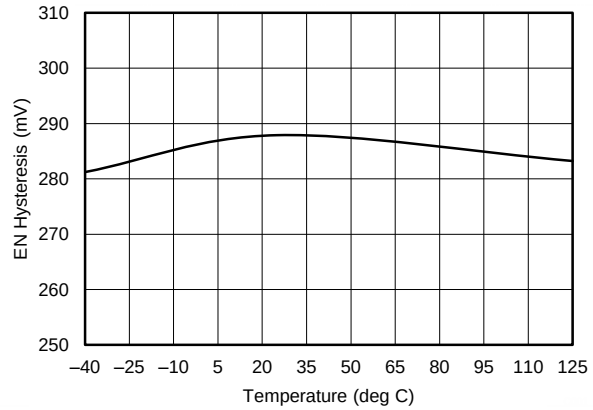



**Figure 15. EN Hysteresis vs Junction Temperature**

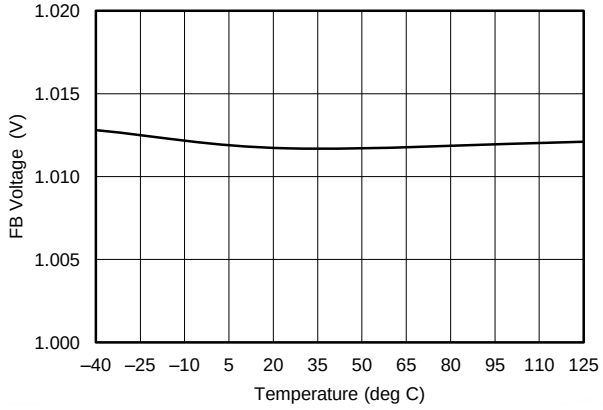



**Figure 16. FB Voltage vs Junction Temperature**

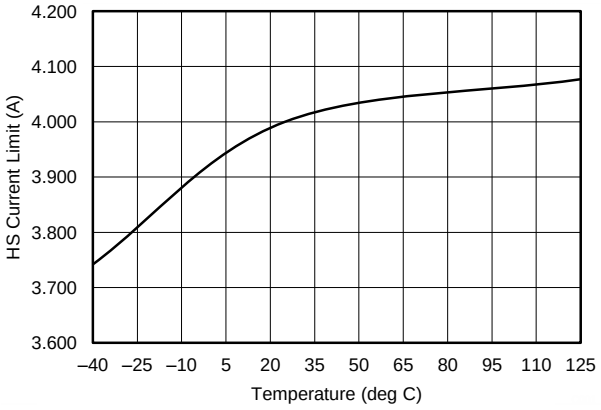



**Figure 17. HS Current Limit vs Junction Temperature**

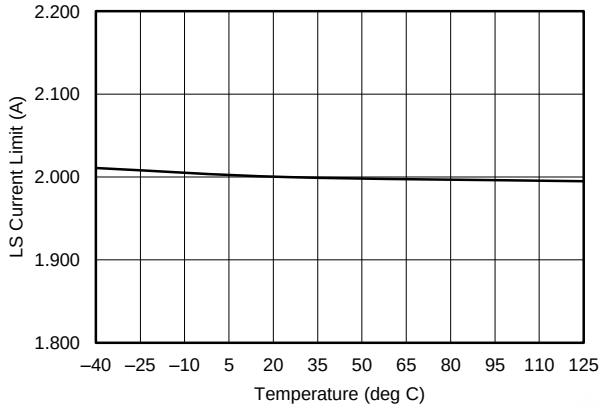



**Figure 18. LS Current Limit vs Junction Temperature**

## Typical Characteristics (continued)

Unless otherwise specified, $V_{IN}$ = 12 V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz, L = 6.8 µH, $C_{OUT}$ = 120 µF, $C_{FF}$ = 100 pF. See *Application Performance Curves* for Bill of materials for other $V_{OUT}$ and $F_S$ combinations.

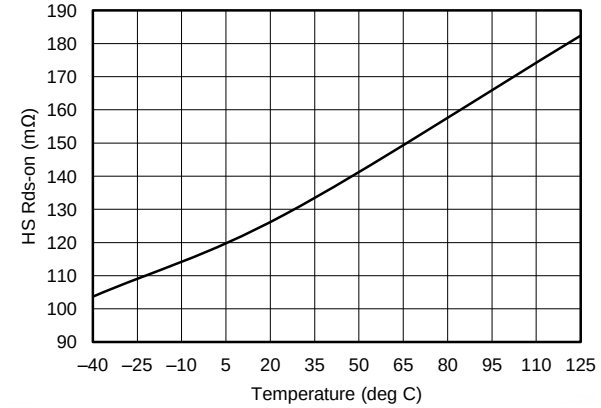



**Figure 19. High Side FET On Resistance vs Junction Temperature**

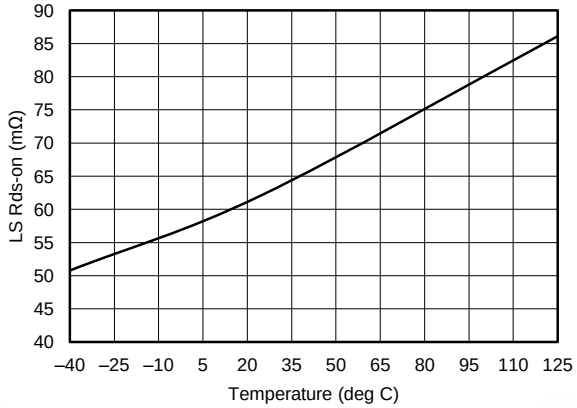



**Figure 20. Low Side FET On Resistance vs Junction Temperature**

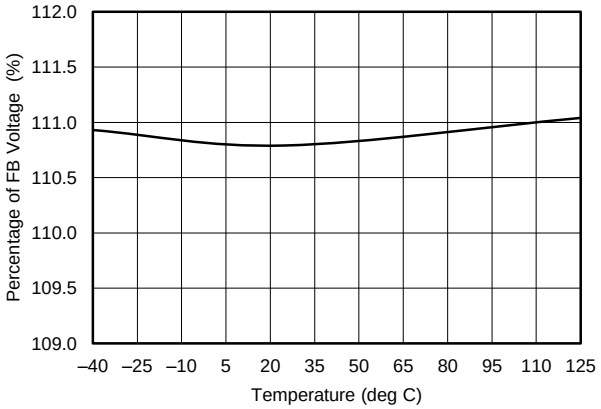



**Figure 21. PGOOD OVP Falling Threshold vs Junction Temperature**

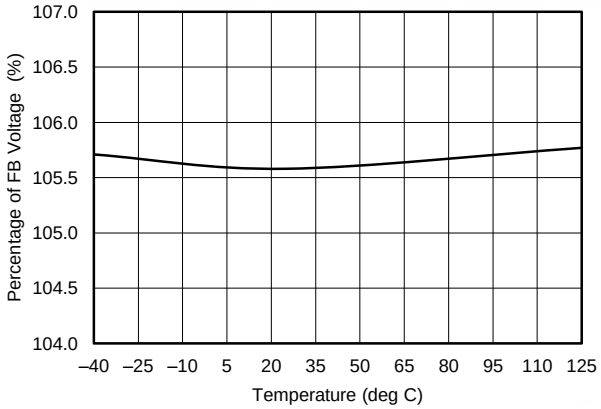



**Figure 22. PGOOD OVP Rising Threshold vs Junction Temperature**

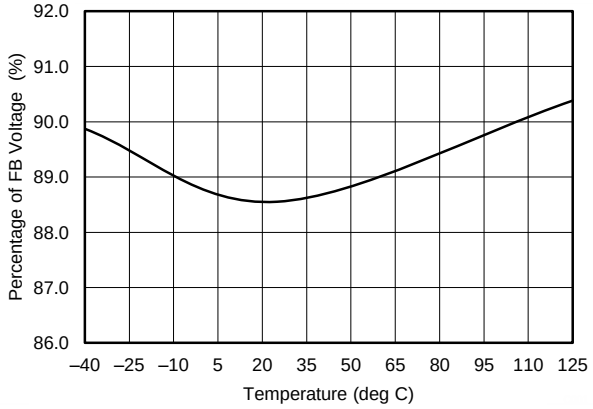



**Figure 23. PGOOD UVP Falling Threshold vs Junction Temperature**

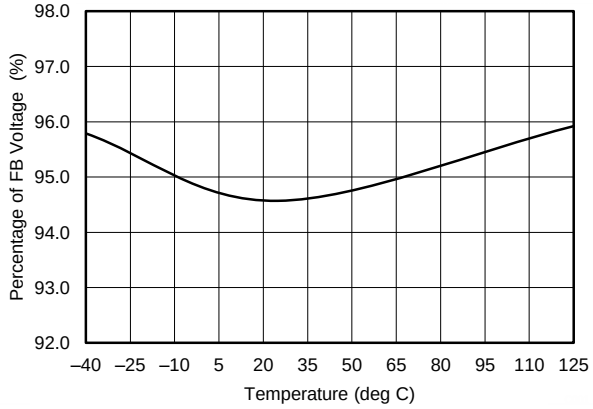



**Figure 24. PGOOD UVP Rising Threhsold vs Junction Temperature**

# 7 Detailed Description

## 7.1 Overview

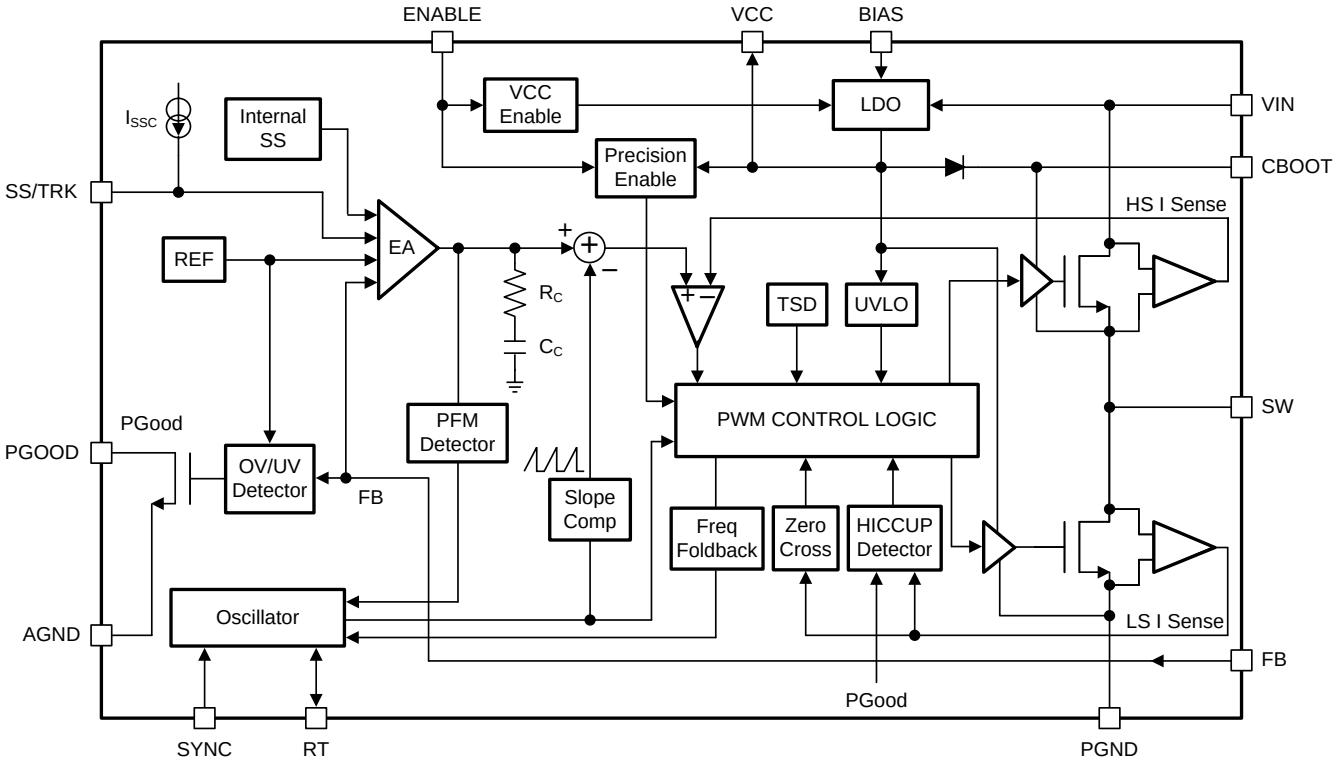
The LM43602 regulator is an easy to use synchronous step-down DC-DC converter that operates from 3.5 V to 36 V supply voltage. It is capable of delivering up to 2 A DC load current with exceptional efficiency and thermal performance in a very small solution size. An extended family is available in 0.5 A, 1A, and 3 A load options in pin to pin compatible packages.

The LM43602 employs fixed frequency peak current mode control with Discontinuous Conduction Mode (DCM) and Pulse Frequency Modulation (PFM) mode at light load to achieve high efficiency across the load range. The device is internally compensated, which reduces design time, and requires fewer external components. The switching frequency is programmable from 200 kHz to 2.2 MHz by an external resistor $R_T$. It is default at 500 kHz without $R_T$ resistor. The LM43602 is also capable of synchronization to an external clock within the 200-kHz to 2.2-MHz frequency range. The wide switching frequency range allows the device to be optimized to fit small board space at higher frequency, or high efficient power conversion at lower frequency.

Optional features are included for more comprehensive system requirements, including power-good (PGOOD) flag, precision enable, synchronization to external clock, extendable soft-start time, and output voltage tracking. These features provide a flexible and easy to use platform for a wide range of applications. Protection features include overtemperature shutdown, $V_{CC}$ undervoltage lockout (UVLO), cycle-by-cycle current limit, and short-circuit protection with hiccup mode.

The family requires few external components and the pin arrangement was designed for simple, optimum PCB layout. The LM43602 device is available in the 16-lead HTSSOP (PWP) and 16-pin VSON packages.

## 7.2 Functional Block Diagram



## 7.3 Feature Description

### 7.3.1 Fixed Frequency Peak Current-Mode Controlled Step-Down Regulator

The following operating description of the LM43602 will refer to the *Functional Block Diagram* and to the waveforms in Figure 25. The LM43602 is a step-down Buck regulator with both high-side (HS) switch and low-side (LS) switch (synchronous rectifier) integrated. The LM43602 supplies a regulated output voltage by turning on the HS and LS NMOS switches with controlled ON time. During the HS switch ON time, the SW pin voltage $V_{SW}$ swings up to approximately $V_{IN}$, and the inductor current $i_L$ increases with a linear slope ($V_{IN}$ - $V_{OUT}$) / L. When the HS switch is turned off by the control logic, the LS switch is turned on after a anti-shoot-through dead time. Inductor current discharges through the LS switch with a slope of -$V_{OUT}$ / L. The control parameter of buck converters are defined as Duty Cycle D = $t_{ON}$ / $T_{SW}$, where $t_{ON}$ is the HS switch ON time and $T_{SW}$ is the switching period. The regulator control loop maintains a constant output voltage by adjusting the duty cycle D. In an ideal Buck converter, where losses are ignored, D is proportional to the output voltage and inversely proportional to the input voltage: D = $V_{OUT}$ / $V_{IN}$.

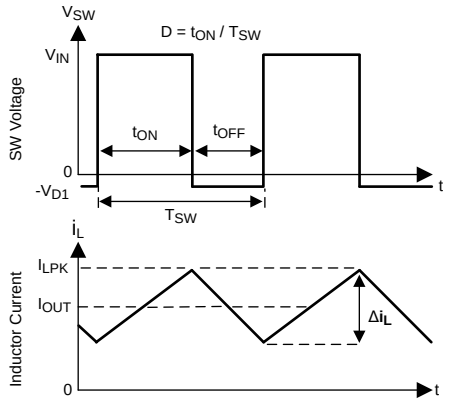



**Figure 25. SW Node and Inductor Current Waveforms in Continuous Conduction Mode (CCM)**

The LM43602 synchronous Buck converter employs peak current mode control topology. A voltage feedback loop is used to get accurate DC voltage regulation by adjusting the peak current command based on voltage offset. The peak inductor current is sensed from the HS switch and compared to the peak current to control the ON time of the HS switch. The voltage feedback loop is internally compensated, which allows for fewer external components, makes it easy to design, and provides stable operation with almost any combination of output capacitors. The regulator operates with fixed switching frequency in Continuous Conduction Mode (CCM) and Discontinuous Conduction Mode (DCM). At very light load, the LM43602 will operate in PFM to maintain high efficiency and the switching frequency will decrease with reduced load current.

### 7.3.2 Light Load Operation

DCM operation is employed in the LM43602 when the inductor current valley reaches zero. The LM43602 will be in DCM when load current is less than half of the peak-to-peak inductor current ripple in CCM. In DCM, the LS switch is turned off when the inductor current reaches zero. Switching loss is reduced by turning off the LS FET at zero current and the conduction loss is lowered by not allowing negative current conduction. Power conversion efficiency is higher in DCM than CCM under the same conditions.

In DCM, the HS switch ON time will reduce with lower load current. When either the minimum HS switch ON time ($t_{ON-MIN}$) or the minimum peak inductor current ($I_{PEAK-MIN}$) is reached, the switching frequency will decrease to maintain regulation. At this point, the LM43602 operates in PFM. In PFM, switching frequency is decreased by the control loop when load current reduces to maintain output voltage regulation. Switching loss is further reduced in PFM operation due to less frequent switching actions.

## Feature Description (continued)

In PFM operation, a small positive DC offset is required at the output voltage to activate the PFM detector. The lower the frequency in PFM, the more DC offset is needed at $V_{OUT}$. Please refer to the Typical Characteristics for typical DC offset at very light load. If the DC offset on $V_{OUT}$ is not acceptable for a given application, a static load at output is recommended to reduce or eliminate the offset. Lowering values of the feedback divider $R_{FBT}$ and $R_{FBB}$ can also serve as a static load. In conditions with low VIN and/or high frequency, the LM43602 may not enter PFM mode if the output voltage cannot be charged up to provide the trigger to activate the PFM detector. Once the LM43602 is operating in PFM mode at higher $V_{IN}$, it will remain in PFM operation when VIN is reduced

### 7.3.3 Adjustable Output Voltage

The voltage regulation loop in the LM43602 regulates output voltage by maintaining the voltage on FB pin ( $V_{FB}$) to be the same as the internal REF voltage ($V_{REF}$). A resistor divider pair is needed to program the ratio from output voltage $V_{OUT}$ to $V_{FB}$. The resistor divider is connected from the $V_{OUT}$ of the LM43602 to ground with the mid-point connecting to the FB pin.

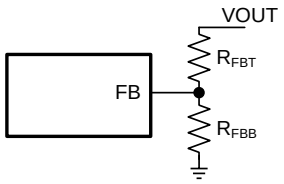



**Figure 26. Output Voltage Setting**

The voltage reference system produces a precise voltage reference over temperature. The internal REF voltage is 1.011 V typically. To program the output voltage of the LM43602 to be a certain value $V_{OUT}$, $R_{FBB}$ can be calculated with a selected $R_{FBT}$ by

$$R_{FBB} = \frac{V_{FB}}{V_{OUT} - V_{FB}} R_{FBT} \quad (1)$$

The choice of the $R_{FBT}$ depends on the application. $R_{FBT}$ in the range from 10 kΩ to 100 kΩ is recommended for most applications. A lower $R_{FBT}$ value can be used if static loading is desired to reduce $V_{OUT}$ offset in PFM operation. Lower $R_{FBT}$ will reduce efficiency at very light load. Less static current goes through a larger $R_{FBT}$ and might be more desirable when light load efficiency is critical. But $R_{FBT}$ larger than 1 MΩ is not recommended because it makes the feedback path more susceptible to noise. Larger $R_{FBT}$ value requires more carefully designed feedback path on the PCB. The tolerance and temperature variation of the resistor dividers affect the output voltage regulation. It is recommended to use divider resistors with 1% tolerance or better and temperature coefficient of 100 ppm or lower.

If the resistor divider is not connected properly, output voltage cannot be regulated since the feedback loop is broken. If the FB pin is shorted to ground, the output voltage will be driven close to $V_{IN}$, since the regulator sees very low voltage on the FB pin and tries to regulator it up. The load connected to the output could be damaged under such a condition. Do not short FB pin to ground when the LM43602 is enabled. It is important to route the feedback trace away from the noisy area of the PCB. For more layout recommendations, please refer to the Layout section.

### 7.3.4 Enable (EN)

Voltage on the EN pin ($V_{EN}$) controls the ON or OFF operation of the LM43602. Applying a voltage less than 0.4 V to the EN input shuts down the operation of the LM43602. In shutdown mode the quiescent current drops to typically 1.2 µA at $V_{IN}$ = 12 V.

The internal LDO output voltage $V_{CC}$ is turned on when $V_{EN}$ is higher than 1.2 V. The LM43602 switching action and output regulation are enabled when $V_{EN}$ is greater than 2.1 V (typical). The LM43602 supplies regulated output voltage when enabled and output current up to 2 A.

The EN pin is an input and cannot be open circuit or floating. The simplest way to enable the operation of the LM43602 is to connect the EN pin to VIN pins directly. This allows self-start-up of the LM43602 when $V_{IN}$ is within the operation range.

## Feature Description (continued)

Many applications will benefit from the employment of an enable divider $R_{ENT}$ and $R_{ENB}$ in Figure 27 to establish a precision system UVLO level for the stage. System UVLO can be used for supplies operating from utility power as well as battery power. It can be used for sequencing, ensuring reliable operation, or supply protection, such as a battery. An external logic signal can also be used to drive EN input for system sequencing and protection.

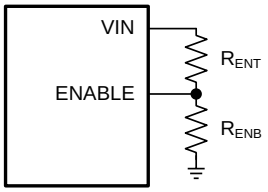



**Figure 27. System UVLO By Enable Dividers**

### 7.3.5 VCC, UVLO and BIAS

The LM43602 integrates an internal LDO to generate $V_{CC}$ for control circuitry and MOSFET drivers. The nominal voltage for $V_{CC}$ is 3.2 V. The VCC pin is the output of the LDO must be properly bypassed. A high quality ceramic capacitor with 2.2 µF to 10 µF capacitance and 6.3 V or higher rated voltage should be placed as close as possible to VCC and grounded to the exposed PAD and ground pins. The VCC output pin should not be loaded, left floating, or shorted to ground during operation. Shorting VCC to ground during operation may cause damage to the LM43602.

Under voltage lockout (UVLO) prevents the LM43602 from operating until the $V_{CC}$ voltage exceeds 3.15 V (typical). The $V_{CC}$ UVLO threshold has 575 mV of hysteresis (typically) to prevent undesired shuting down due to temperary $V_{IN}$ droops.

The internal LDO has two inputs: primary from VIN and secondary from BIAS input. The BIAS input powers the LDO when $V_{BIAS}$ is higher than the change-over threshold. Power loss of an LDO is calculated by $I_{LDO}$ * ($V_{IN-LDO}$ - $V_{OUT-LDO}$). The higher the difference between the input and output voltages of the LDO, the more power loss occur to supply the same output current. The BIAS input is designed to reduce the difference of the input and output voltages of the LDO to reduce power loss and improve LM43602 efficiency, especially at light load. It is recommended to tie the BIAS pin to $V_{OUT}$ when $V_{OUT}$ ≥ 3.3 V. The BIAS pin should be grounded in applications with $V_{OUT}$ less than 3.3 V. BIAS input can also come from an external voltage source, if available, to reduce power loss. When used, a 1 µF to 10 µF high quality ceramic capacitor is recommended to bypass the BIAS pin to ground.

### 7.3.6 Soft-Start and Voltage Tracking (SS/TRK)

The LM43602 has a flexible and easy to use start up rate control pin: SS/TRK. Soft-start feature is to prevent inrush current impacting the LM43602 and its supply when power is first applied. Soft-start is achieved by slowly ramping up the target regulation voltage when the device is first enabled or powered up.

The simplest way to use the part is to leave the SS/TRK pin open circuit or floating. The LM43602 will employ the internal soft-start control ramp and start up to the regulated output voltage in 4.1 ms typically.

In applications with a large amount of output capacitors, or higher $V_{OUT}$, or other special requirements the soft-start time can be extended by connecting an external capacitor $C_{SS}$ from SS/TRK pin to AGND. Extended soft-start time further reduces the supply current needed to charge up output capacitors and supply any output loading. An internal current source ($I_{SSC}$ = 2.2 µA) charges $C_{SS}$ and generates a ramp from 0 V to $V_{FB}$ to control the ramp-up rate of the output voltage. For a desired soft start time $t_{SS}$, the capacitance for $C_{SS}$ can be found by

$$C_{SS} = I_{SSC} \times t_{SS} \quad (2)$$

The LM43602 is capable of start up into prebiased output conditions. When the inductor current reaches zero, the LS switch will be turned off to avoid negative current conduction. This operation mode is also called diode emulation mode. It is built-in by the DCM operation in light loads. With prebiased output voltage, the LM43602 will wait until the soft-start ramp allows regulation above the prebiased voltage and then follow the soft-start ramp to regulation level.

## Feature Description (continued)

When an external voltage ramp is applied to the SS/TRK pin, the LM43602 FB voltage follows the ramp if the ramp magnitude is lower than the internal soft-start ramp. A resistor divider pair can be used on the external control ramp to the SS/TRK pin to program the tracking rate of the output voltage. The final voltage seen by the SS/TRK pin should not fall below 1.2 V to avoid abnormal operation.

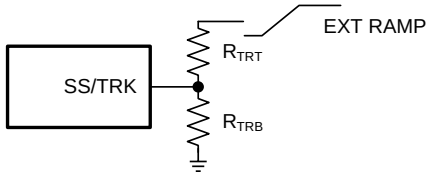



**Figure 28. Soft Start Tracking External Ramp**

$V_{OUT}$ tracked to external voltage ramps has options of ramping up slower or faster than the internal voltage ramp. $V_{FB}$ always follows the lower potential of the internal voltage ramp and the voltage on the SS/TRK pin. Figure 29 shows the case when $V_{OUT}$ ramps slower than the internal ramp, while Figure 30 shows when $V_{OUT}$ ramps faster than the internal ramp. Faster start up time may result in inductor current tripping current protection during start-up. Use with special care.

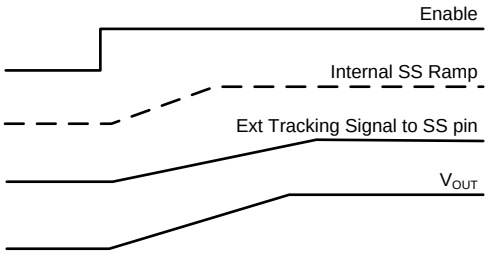



**Figure 29. Tracking with Longer Start-up Time Than The Internal Ramp**

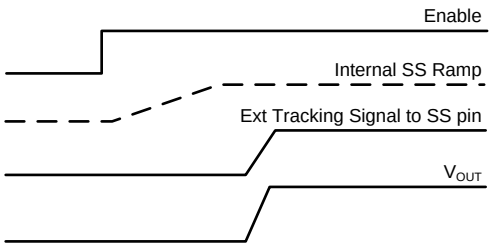



**Figure 30. Tracking with Shorter Start-up Time Than The Internal Ramp**

### 7.3.7 Switching Frequency (RT) and Synchronization (SYNC)

The switching frequency of the LM43602 can be programmed by the impedance $R_T$ from the RT pin to ground. The frequency is inversely proportional to the $R_T$ resistance. The RT pin can be left floating and the LM43602 will operate at 500 kHz default switching frequency. The RT pin is not designed to be shorted to ground. For a desired frequency, typical $R_T$ resistance can be found by Equation 3. Table 1 gives typical $R_T$ values with a given $F_S$.

$$R_T(k\Omega) = 40200 / Freq\ (kHz) - 0.6 \quad (3)$$

## Feature Description (continued)

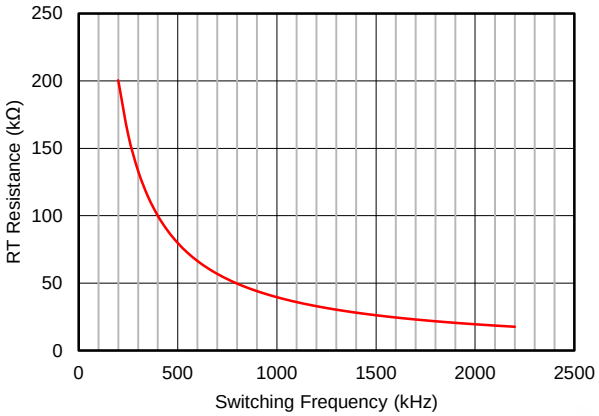



**Figure 31. RT vs Frequency Curve**

**Table 1. Typical Frequency Setting $R_T$ Resistance**

| $F_S$ (kHz) | $R_T$ (kΩ) |
|---|---|
| 200 | 200 |
| 350 | 115 |
| 500 | 78.7 |
| 750 | 53.6 |
| 1000 | 39.2 |
| 1500 | 26.1 |
| 2000 | 19.6 |
| 2200 | 17.8 |

The LM43602 switching action can also be synchronized to an external clock from 200 kHz to 2.2 MHz. Connect an external clock to the SYNC pin, with proper high speed termination, to avoid ringing. The SYNC pin should be grounded if not used.

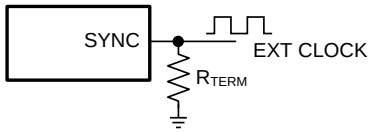



**Figure 32. Frequency Synchronization**

The recommendations for the external clock include: high level no lower than 2 V, low level no higher than 0.4 V, duty cycle between 10% and 90% and both positive and negative pulse width no shorter than 80 ns. When the external clock fails at logic high or low, the LM43602 will switch at the frequency programmed by the $R_T$ resistor after a time-out period. It is recommended to connect a resistor $R_T$ to the RT pin such that the internal oscillator frequency is the same as the target clock frequency when the LM43602 is synchronized to an external clock. This allows the regulator to continue operating at approximately the same switching frequency if the external clock fails.

The choice of switching frequency is usually a compromise between conversion efficiency and the size of the circuit. Lower switching frequency implies reduced switching losses (including gate charge losses, switch transition losses, etc.) and usually results in higher overall efficiency. However, higher switching frequency allows use of smaller LC output filters and hence a more compact design. Lower inductance also helps transient response (higher large signal slew rate of inductor current), and reduces the DCR loss. The optimal switching frequency is usually a trade-off in a given application and thus needs to be determined on a case-by-case basis. It is related to the input voltage, output voltage, most frequent load current level(s), external component choices, and circuit size requirement. The choice of switching frequency may also be limited if an operating condition triggers $T_{ON\text{-}MIN}$ or $T_{OFF\text{-}MIN}$.

## Feature Description (continued)

### 7.3.8 Minimum ON-time, Minimum OFF-time and Frequency Foldback at Drop-Out Conditions

Minimum ON-time, $T_{ON-MIN}$, is the smallest duration of time that the HS switch can be on. $T_{ON-MIN}$ is typically 125 ns in the LM43602. Minimum OFF-time, $T_{OFF-MIN}$, is the smallest duration that the HS switch can be off. $T_{OFF-MIN}$ is typically 200 ns in the LM43602.

In CCM operation, $T_{ON-MIN}$ and $T_{OFF-MIN}$ limits the voltage conversion range given a selected switching frequency. The minimum duty cycle allowed is

$$D_{MIN} = T_{ON-MIN} \times F_S \quad (4)$$

And the maximum duty cycle allowed is

$$D_{MAX} = 1 - T_{OFF-MIN} \times F_S \quad (5)$$

Given fixed $T_{ON-MIN}$ and $T_{OFF-MIN}$, the higher the switching frequency the narrower the range of the allowed duty cycle. In the LM43602, frequency foldback scheme is employed to extend the maximum duty cycle when $T_{OFF-MIN}$ is reached. The switching frequency will decrease once longer duty cycle is needed under low VIN conditions. The switching frequency can be decreased to approximately 1/10 of the programmed frequency by $R_T$ or the synchronization clock. Such wide range of frequency foldback allows the LM43602 output voltage stays in regulation with much lower supply voltage $V_{IN}$. This leads to a lower effective drop-out voltage. Please refer to Typical Characteristics for more details.

Given a output voltage, the choice of the switching frequency affects the allowed input voltage range, solution size and efficiency. The maximum operatable supply voltage can be found by

$$V_{IN-MAX} = V_{OUT} / (F_S * T_{ON-MIN}) \quad (6)$$

At lower supply voltage, the switching frequency will decrease once $T_{OFF-MIN}$ is tripped. The minimum $V_{IN}$ without frequency foldback can be approximated by

$$V_{IN-MIN} = V_{OUT} / (1 - F_S * T_{OFF-MIN}) \quad (7)$$

Taking considerations of power losses in the system with heavy load operation, $V_{IN-MIN}$ is higher than the result calculated in Equation 7 . With frequency foldback, $V_{IN-MIN}$ is lowered by decreased $F_S$.

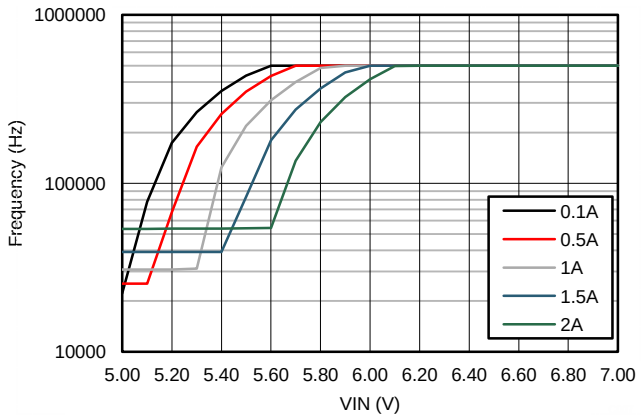



**Figure 33. $V_{OUT}$ = 5 V $F_s$ = 500 kHz Frequency Foldback at Dropout**

### 7.3.9 Internal Compensation and $C_{FF}$

The LM43602 is internally compensated with $R_C$ = 400 kΩ and $C_C$ = 50 pF as shown in Functional Block Diagram. The internal compensation is designed such that the loop response is stable over the entire operating frequency and output voltage range. Depending on the output voltage, the compensation loop phase margin can be low with all ceramic capacitors. An external feed-forward cap $C_{FF}$ is recommended to be placed in parallel with the top resistor divider $R_{FBT}$ for optimum transient performance.

## Feature Description (continued)

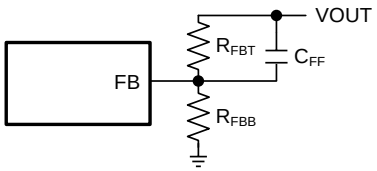



**Figure 34. Feed-forward Capacitor for Loop Compensation**

The feed-forward capacitor $C_{FF}$ in parallel with $R_{FBT}$ places an additional zero before the cross over frequency of the control loop to boost phase margin. The zero frequency can be found by

$$f_{Z\text{-}CFF} = 1 / ( 2\pi \times R_{FBT} \times C_{FF} ). \quad (8)$$

An additional pole is also introduced with $C_{FF}$ at the frequency of

$$f_{P\text{-}CFF} = 1 / ( 2\pi \times C_{FF} \times ( R_{FBT} // R_{FBB} )). \quad (9)$$

The $C_{FF}$ should be selected such that the bandwidth of the control loop without the $C_{FF}$ is centered between $f_{Z\text{-}CFF}$ and $f_{P\text{-}CFF}$. The zero $f_{Z\text{-}CFF}$ adds phase boost at the crossover frequency and improves transient response. The pole $f_{P\text{-}CFF}$ helps maintaining proper gain margin at frequency beyond the crossover.

Designs with different combinations of output capacitors need different $C_{FF}$. Different types of capacitors have different Equivalent Series Resistance (ESR). Ceramic capacitors have the smallest ESR and need the most $C_{FF}$. Electrolytic capacitors have much larger ESR and the ESR zero frequency

$$f_{Z\text{-}ESR} = 1 / ( 2\pi \times ESR \times C_{OUT}) \quad (10)$$

would be low enough to boost the phase up around the crossover frequency. Designs using mostly electrolytic capacitors at the output may not need any $C_{FF}$.

The $C_{FF}$ creates a time constant with $R_{FBT}$ that couples in the attenuated output voltage ripple to the FB node. If the $C_{FF}$ value is too large, it can couple too much ripple to the FB and affect $V_{OUT}$ regulation. It could also couple too much transient voltage deviation and falsely trip PGOOD thresholds. Therefore, $C_{FF}$ should be calculated based on output capacitors used in the system. At cold temperatures, the value of $C_{FF}$ might change based on the tolerance of the chosen component. This may reduce its impedance and ease noise coupling on the FB node. To avoid this, more capacitance can be added to the output or the value of $C_{FF}$ can be reduced. Please refer to the Detailed Design Procedure for the calculation of $C_{FF}$.

### 7.3.10 Bootstrap Voltage (BOOT)

The driver of the HS switch requires a bias voltage higher than $V_{IN}$ when the HS switch is ON. The capacitor connected between CBOOT and SW pins works as a charge pump to boost voltage on the CBOOT pin to ($V_{SW}$ + $V_{CC}$). The boot diode is integrated on the LM43602 die to minimize Bill-Of-Material (BOM). A synchronous switch is also integrated in parallel with the boot diode to reduce voltage drop on CBOOT. A high quality ceramic 0.47 µF 6.3 V or higher capacitor is recommended for $C_{BOOT}$.

### 7.3.11 Power Good (PGOOD)

The LM43602 has a built in power-good flag shown on PGOOD pin to indicate whether the output voltage is within its regulation level. The PGOOD signal can be used for start-up sequencing of multiple rails or fault protection. The PGOOD pin is an open-drain output that requires a pull-up resistor to an appropriate DC voltage. Voltage seen by the PGOOD pin should never exceed 12 V. A Resistor divider pair can be used to divide voltage down from a higher potential. A typical range of pull-up resistor value is 10 kΩ to 100 kΩ.

When the FB voltage is within the power-good band, +4% above and -7% below the internal reference $V_{REF}$ typically, the PGOOD switch will be turned off and the PGOOD voltage will be pulled up to the voltage level defined by the pull up resistor or divider. When the FB voltage is outside of the tolerance band, +10% above or -13% below $V_{REF}$ typically, the PGOOD switch will be turned on and the PGOOD pin voltage will be pulled low to indicate power bad. Both rising and falling edges of the power-good flag have a built-in 220 µs (typical) deglitch delay.

## Feature Description (continued)

### 7.3.12 Over Current and Short Circuit Protection

The LM43602 is protected from over-current conditions by cycle-by-cycle current limiting on both peak and valley of the inductor current. Hiccup mode will be activated if a fault condition persists to prevent over heating.

High-side MOSFET over-current protection is implemented by the nature of the Peak Current Mode control. The HS switch current is sensed when the HS is turned on after a set blanking time. The HS switch current is compared to the output of the Error Amplifier (EA) minus slope compensation every switching cycle. Please refer to Functional Block Diagram for more details. The peak current of the HS switch is limited by the maximum EA output voltage minus the slope compensation at every switching cycle. The slope compensation magnitude at the peak current is proportional to the duty cycle.

When the LS switch is turned on, the current going through it is also sensed and monitored. The LS switch will not be turned OFF at the end of a switching cycle if its current is above the LS current limit $I_{LS\text{-}LIMIT}$. The LS switch will be kept ON so that inductor current keeps ramping down, until the inductor current ramps below the LS current limit. Then the LS switch will be turned OFF and the HS switch will be turned on after a dead time. If the current of the LS switch is higher than the LS current limit for 32 consecutive cycles and the power-good flag is low, hiccup current protection mode will be activated. In hiccup mode, the regulator will be shutdown and kept off for 5.5 ms typically before the LM43602 tries to start again. If over-current or short-circuit fault condition still exist, hiccup will repeat until the fault condition is removed. Hiccup mode reduces power dissipation under severe over-current conditions, prevents over heating and potential damage to the device.

Hiccup is only activated when power-good flag is low. Under non-severe over-current conditions when $V_{OUT}$ has not fallen outside of the PGOOD tolerance band, the LM43602 will reduce the switching frequency and keep the inductor current valley clamped at the LS current limit level. This operation mode allows slight over current operation during load transients without tripping hiccup. If power-good flag becomes low, hiccup operation will start after LS current limit is tripped 32 consecutive cycles.

### 7.3.13 Thermal Shutdown

Thermal shutdown is a built-in self protection to limit junction temperature and prevent damages due to over heating. Thermal shutdown turns off the device when the junction temperature exceeds 160°C typically to prevent further power dissipation and temperature rise. Junction temperature will reduce after thermal shutdown. The LM43602 will attempt to restart when the junction temperature drops to 150°C.

## 7.4 Device Functional Modes

### 7.4.1 Shutdown Mode

The EN pin provides electrical ON and OFF control for the LM43602. When $V_{EN}$ is below 0.4 V, the device is in shutdown mode. Both the internal LDO and the switching regulator are off. In shutdown mode the quiescent current drops to 2.3 µA typically with $V_{IN}$ = 24 V. The LM43602 also employs under voltage lock out protection. If $V_{CC}$ voltage is below the UVLO level, the output of the regulator will be turned off.

### 7.4.2 Stand-by Mode

The internal LDO has a lower enable threshold than the regulator. When $V_{EN}$ is above 1.2 V and below the precision enable falling threshold (1.8 V typically), the internal LDO regulates the $V_{CC}$ voltage at 3.2 V. The precision enable circuitry is turned on once $V_{CC}$ is above the UVLO threshold. The switching action and voltage regulation are not enabled unless $V_{EN}$ rises above the precision enable threshold (2.1 V typically).

### 7.4.3 Active Mode

The LM43602 is in Active Mode when $V_{EN}$ is above the precision enable threshold and $V_{CC}$ is above its UVLO level. The simplest way to enable the LM43602 is to connect the EN pin to $V_{IN}$. This allows self start-up of the LM43602 when the input voltage is in the operation range: 3.5 V to 36 V. Please refer to Enable (EN) and VCC, UVLO and BIAS for details on setting these operating levels.

In Active Mode, depending on the load current, the LM43602 will be in one of four modes:

1. Continuous conduction mode (CCM) with fixed switching frequency when load current is above half of the peak-to-peak inductor current ripple;

## Device Functional Modes (continued)

2. Discontinuous conduction mode (DCM) with fixed switching frequency when load current is lower than half of the peak-to-peak inductor current ripple in CCM operation;
3. Pulse Frequency Modulation (PFM) when switching frequency is decreased at very light load;
4. Fold-back mode when switching frequency is decreased to maintain output regulation at lower supply voltage $V_{IN}$.

### 7.4.4 CCM Mode

Constant Current Mode (CCM) operation is employed in the LM43602 when the load current is higher than half of the peak-to-peak inductor current. In CCM peration, the frequency of operation is fixed unless the the minimum HS switch ON-time ($T_{ON\_MIN}$) or OFF-time ($T_{OFF\_MIN}$) is exceeded. Output voltage ripple will be at a minimum in this mode and the maximum output current of 2 A can be supplied by the LM43602.

### 7.4.5 Light Load Operation

When the load current is lower than half of the peak-to-peak inductor current in CCM, the LM43602 will operate in Discontinuous Conduction Mode (DCM), also known as Diode Emulation Mode (DEM). In DCM operation, the LS FET is turned off when the inductor current drops to 0 A to improve efficiency. Both switching losses and conduction losses are reduced in DCM, comparing to forced PWM operation at light load.

At even lighter current loads, Pulse Frequency Mode (PFM) is activated to maintain high efficiency operation. When the HS switch ON-time reduces to $T_{ON\_MIN}$ or peak inductor current reduces to its minimum $I_{PEAK-MIN}$, the switching frequency will reduce to maintain proper regulation. Efficiency is greatly improved by reducing switching and gate drive losses.

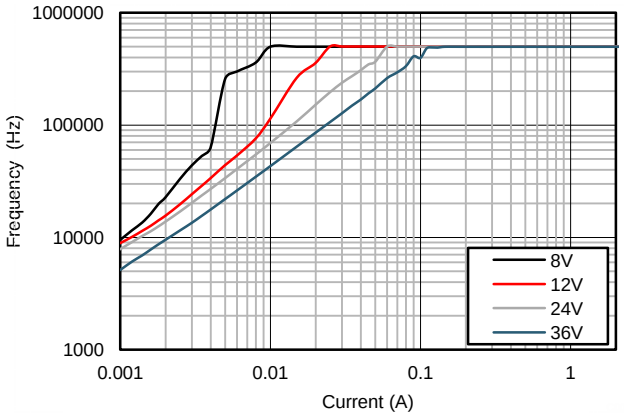



**Figure 35. $V_{OUT}$ = 5 V $F_s$ = 500 kHz Pulse Frequency Mode Operation**

### 7.4.6 Self-Bias Mode

For highest efficiency of operation, it is recommended that the BIAS pin be connected directly to $V_{OUT}$ when $V_{OUT}$ ≥ 3.3 V. In this Self-Bias Mode of operation, the difference between the input and output voltages of the internal LDO are reduced and therefore the total efficiency of the LM43602 is improved. These efficiency gains are more evident during light load operation. During this mode of operation, the LM43602 operates with a minimum quiescent current of 27 µA (typical). Please refer to VCC, UVLO and BIAS for more details.

# 8 Applications and Implementation

## 8.1 Application Information

The LM43602 is a step down DC-to-DC regulator. It is typically used to convert a higher DC voltage to a lower DC voltage with a maximum output current of 2 A. The following design procedure can be used to select components for the LM43602. Alternately, the WEBENCH® software may be used to generate complete designs. When generating a design, the WEBENCH® software utilizes iterative design procedure and accesses comprehensive databases of components. Please go to ti.com for more details.

This section presents a simplified discussion of the design process.

## 8.2 Typical Applications

The LM43602 only requires a few external components to convert from a wide voltage range of supply to a fixed output voltage. Figure 36 shows a basic schematic when BIAS is connected to $V_{OUT}$ and this is recommended for $V_{OUT} \geq 3.3$ V. For $V_{OUT} < 3.3$ V, BIAS should be connected to ground, as shown in Figure 37.

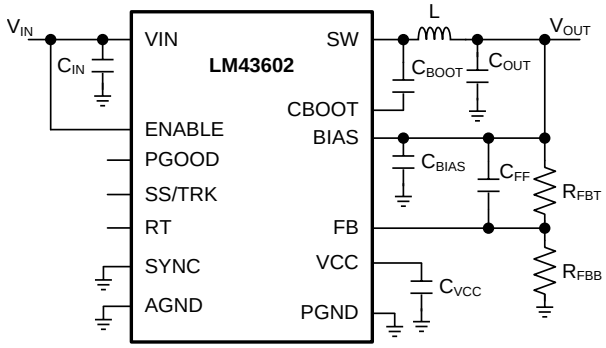



**Figure 36. LM43602 Basic Schematic for $V_{OUT} \geq 3.3$ V, tie BIAS to $V_{OUT}$**

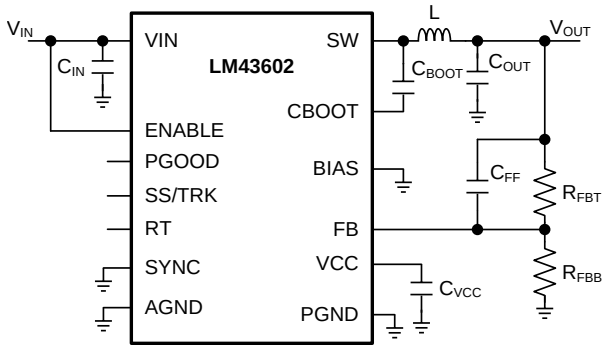



**Figure 37. LM43602 Basic Schematic for $V_{OUT} < 3.3$ V, tie BIAS to ground**

The LM43602 also integrates a full list of optional features to aid system design requirements such as: precision enable, $V_{CC}$ UVLO, programmable soft-start, output voltage tracking, programmable switching frequency, clock synchronization and power-good indication. Each application can select the features for a more comprehensive design. A schematic with all features utilized is shown in Figure 38.

## Typical Applications (continued)

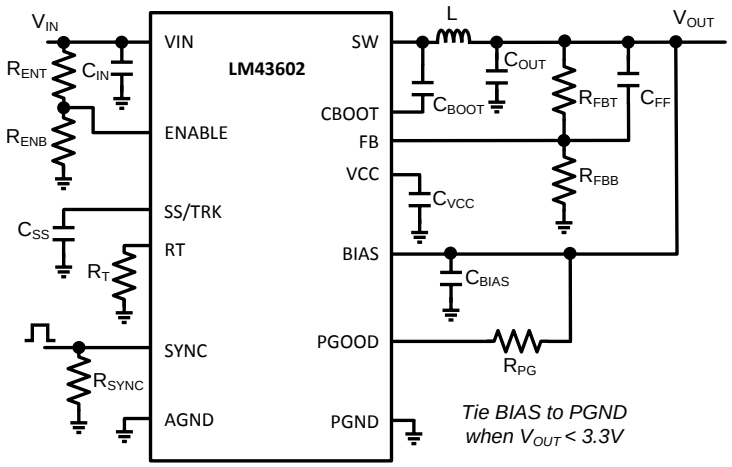



**Figure 38. LM43602 Schematic with All Features**

The external components have to fulfill the needs of the application, but also the stability criteria of the device's control loop. The LM43602 is optimized to work within a range of external components. The LC output filter's inductance and capacitance have to be considered in conjunction, creating a double pole, responsible for the corner frequency of the converter (see Output Filter And Loop Stability section). Table 2 can be used to simplify the output filter component selection.

**Table 2. L, $C_{OUT}$ and $C_{FF}$ Typical Values**

| $F_S$ (kHz) | $V_{OUT}$ (V) | L (µH)(1) | $C_{OUT}$ (µF)(2) | $C_{FF}$ (pF)(3)(4) | $R_T$ (kΩ) | $R_{FBB}$ (kΩ)(3)(4) |
|---|---|---|---|---|---|---|
| 200 | 1 | 8.2 | 560 | none | 200 | 100 |
| 500 | 1 | 3.3 | 470 | none | 80.6 or open | 100 |
| 1000 | 1 | 1.5 | 220 | none | 39.2 | 100 |
| 2200 | 1 | 0.68 | 150 | none | 17.8 | 100 |
| 200 | 3.3 | 18 | 250 | 56 | 200 | 432 |
| 500 | 3.3 | 6.8 | 150 | 47 | 80.6 or open | 432 |
| 1000 | 3.3 | 4.7 | 100 | 33 | 39.2 | 432 |
| 2200 | 3.3 | 1.8 | 47 | 22 | 17.8 | 432 |
| 200 | 5 | 22 | 200 | 68 | 200 | 249 |
| 500 | 5 | 10 | 100 | 47 | 80.6 or open | 249 |
| 1000 | 5 | 4.7 | 47 | 47 | 39.2 | 249 |
| 2200 | 5 | 2.2 | 33 | 33 | 17.8 | 249 |
| 200 | 12 | 68 | 68 | See note(5) | 200 | 90.9 |
| 500 | 12 | 27 | 47 | 68 | 80.6 or open | 90.9 |
| 1000 | 12 | 15 | 33 | 47 | 39.2 | 90.9 |
| 200 | 24 | 68 | 68 | See note(5) | 200 | 43.2 |
| 500 | 24 | 27 | 47 | See note(5) | 80.6 or open | 43.2 |
| 1000 | 24 | 15 | 33 | See note(5) | 39.2 | 43.2 |

(1) Inductance value is calculated based on typical VIN value of 12V.
(2) All the $C_{OUT}$ values are after derating. Add more when using ceramics
(3) $R_{FBT}$ = 0 Ω for $V_{OUT}$ = 1 V. $R_{FBT}$ = 1 MΩ for all other $V_{OUT}$ setting.
(4) For designs with $R_{FBT}$ other than 1 MΩ, please adjust $C_{FF}$ such that ($C_{FF}$ × $R_{FBT}$) is unchanged and adjust $R_{FBB}$ such that ($R_{FBT}$ / $R_{FBB}$) is unchanged.
(5) High ESR $C_{OUT}$ will give enough phase boost and $C_{FF}$ not needed.

## Typical Applications (continued)

### 8.2.1 Design Requirements

Detailed design procedure is described based on a design example. For this design example, use the parameters listed in Table 3 as the input parameters.

**Table 3. Design Example Parameters**

| DESIGN PARAMETER | VALUE |
|---|---|
| Input voltage $V_{IN}$ | 12 V typical, range from 3.5 V to 36 V |
| Output voltage $V_{OUT}$ | 3.3 V |
| Input ripple voltage | 400 mV |
| Output ripple voltage | 30 mV |
| Output current rating | 2 A |
| Operating frequency | 500 kHz |
| Soft-start time | 10 ms |

### 8.2.2 Detailed Design Procedure

#### *8.2.2.1 Custom Design With WEBENCH® Tools*

Click here to create a custom design using the LM43602 device with the WEBENCH® Power Designer.

1. Start by entering the input voltage ($V_{IN}$), output voltage ($V_{OUT}$), and output current ($I_{OUT}$) requirements.
2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at www.ti.com/WEBENCH.

#### *8.2.2.2 Output Voltage Set-Point*

The output voltage of the LM43602 device is externally adjustable using a resistor divider network. The divider network is comprised of top feedback resistor $R_{FBT}$ and bottom feedback resistor $R_{FBB}$. The following equation is used to determine the output voltage of the converter:

$$R_{FBB} = \frac{V_{FB}}{V_{OUT} - V_{FB}} R_{FBT} \quad (11)$$

Choose the value of the $R_{FBT}$ to be 1 MΩ to minimize quiescent current to improve light load efficiency in this application. With the desired output voltage set to be 3.3 V and the $V_{FB}$ = 1.011 V, the $R_{FBB}$ value can then be calculated using Equation 11. The formula yields a value of 434.78 kΩ. Choose the closest available value of 432 kΩ for the $R_{FBB}$. Please refer to Adjustable Output Voltage for more details.

#### *8.2.2.3 Switching Frequency*

The default switching frequency of the LM43602 device is set at 500 kHz when RT pin is open circuit. The switching frequency is selected to be 500 kHz in this application for one less passive components. If other frequency is desired, use Equation 12 to calculate the required value for $R_T$.

$$R_T(k\Omega) = 40200 / \text{Freq (kHz)} - 0.6 \quad (12)$$

For 500 kHz, the calculated $R_T$ is 79.8 kΩ and standard value 80.6 kΩ can also be used to set the switching frequency at 500 kHz.

#### 8.2.2.4 Input Capacitors

The LM43602 device requires high frequency input decoupling capacitor(s) and a bulk input capacitor, depending on the application. The typical recommended value for the high frequency decoupling capacitor is 4.7 µF to 10 µF. A high-quality ceramic type X5R or X7R with sufficiency voltage rating is recommended. The voltage rating must be greater than the maximum input voltage. To compensate the derating of ceramic capactors, a voltage rating of twice the maximum input voltage is recommended. Additionally, some bulk capacitance can be required, especially if the LM43602 circuit is not located within approximately 5 cm from the input voltage source. This capacitor is used to provide damping to the voltage spiking due to the lead inductance of the cable or trace. The value for this capacitor is not critical but must be rated to handle the maximum input voltage including ripple. For this design, a 10 µF, X7R dielectric capacitor rated for 100 V is used for the input decoupling capacitor. The equivalent series resistance (ESR) is approximately 3 mΩ, and the current-rating is 3 A. Include a capacitor with a value of 0.1 µF for high-frequency filtering and place it as close as possible to the device pins.

**NOTE**

DC Bias effect: High capacitance ceramic capacitors have a DC Bias effect, which will have a strong influence on the final effective capacitance. Therefore the right capacitor value has to be chosen carefully. Package size and voltage rating in combination with dielectric material are responsible for differences between the rated capacitor value and the effective capacitance.

#### 8.2.2.5 Inductor Selection

The first criterion for selecting an output inductor is the inductance itself. In most buck converters, this value is based on the desired peak-to-peak ripple current, $\Delta i_L$, that flows in the inductor along with the DC load current. As with switching frequency, the selection of the inductor is a tradeoff between size and cost. Higher inductance gives lower ripple current and hence lower output voltage ripple with the same output capacitors. Lower inductance could result in smaller, less expensive component. An inductance that gives a ripple current of 20% to 40% of the 2 A at the typical supply voltage is a good starting point. $\Delta I_L$ = (1/5 to 2/5) x $I_{OUT}$. The peak-to-peak inductor current ripple can be found by Equation 13 and the range of inductance can be found by Equation 14 with the typical input voltage used as $V_{IN}$.

$$\Delta i_L = \frac{(V_{IN} - V_{OUT}) \times D}{L \times F_S} \tag{13}$$

$$\frac{(V_{IN} - V_{OUT}) \times D}{0.4 \times F_S \times I_{L-MAX}} \le L \le \frac{(V_{IN} - V_{OUT}) \times D}{0.2 \times F_S \times I_{L-MAX}} \tag{14}$$

D is the duty cycle of the converter which in a buck converter can be approximated as D = $V_{IN}/V_{OUT}$, assuming no loss power conversion. By calculating in terms of amperes, volts, and megahertz, the inductance value will come out in micro henries. The inductor ripple current ratio is defined by:

$$r = \frac{\Delta i_L}{I_{OUT}} \tag{15}$$

The second criterion is the inductor saturation current rating. The inductor should be rated to handle the maximum load current plus the ripple current:

$$I_{L\text{-}PEAK} = I_{LOAD\text{-}MAX} + \Delta i_L / 2 \tag{16}$$

The LM43602 has both valley current limit and peak current limit. During an instantaneous short, the peak inductor current can be high due to a momentary increase in duty cycle. The inductor current rating should be higher than the HS current limit. It is advised to select an inductor with a larger core saturation margin and preferably a softer roll off of the inductance value over load current.

In general, it is preferable to choose lower inductance in switching power supplies, because it usually corresponds to faster transient response, smaller DCR, and reduced size for more compact designs. But too low of an inductance can generate too large of an inductor current ripple such that over current protection at the full load could be falsely triggered. It also generates more conduction loss, since the RMS current is slightly higher relative that with lower current ripple at the same DC current. Larger inductor current ripple also implies larger output voltage ripple with the same output capacitors. With peak current mode control, it is not recommended to have too small of an inductor current ripple. A larger peak current ripple improves the comparator signal to noise ratio.

Once the inductance is determined, the type of inductor must be selected. Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates hard, which means that inductance collapses abruptly when the peak design current is exceeded. The 'hard' saturation results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate!

For the design example, a standard 6.8 μH inductor from Wurth, Coiltronics, or Vishay can be used for the 3.3 V output with plenty of current rating margin.

#### *8.2.2.6 Output Capacitor Selection*

The device is designed to be used with a wide variety of LC filters. It is generally desired to use as little output capacitance as possible to keep cost and size down. The output capacitor (s), COUT, should be chosen with care since it directly affects the steady state output voltage ripple, loop stability and the voltage over/undershoot during load current transients.

The output voltage ripple is essentially composed of two parts. One is caused by the inductor current ripple going through the Equivalent Series Resistance (ESR) of the output capacitors:

$$\Delta V_{OUT\text{-}ESR} = \Delta i_L \times ESR \tag{17}$$

The other is caused by the inductor current ripple charging and discharging the output capacitors:

$$\Delta V_{OUT\text{-}C} = \Delta i_L / ( 8 \times F_S \times C_{OUT} ) \tag{18}$$

The two components in the voltage ripple are not in phase, so the actual peak-to-peak ripple is smaller than the sum of the two peaks.

Output capacitance is usually limited by transient performance specifications if the system requires tight voltage regulation in the presence of large current steps and fast slew rates. When a fast large load transient happens, output capacitors provide the required charge before the inductor current can slew to the appropriate level. The initial output voltage step is equal to the load current step multiplied by the ESR. VOUT continues to droop until the control loop response increases or decreases the inductor current to supply the load. To maintain a small over- or undershoot during a transient, small ESR and large capacitance are desired. But these also come with higher cost and size. Thus, the motivation is to seek a fast control loop response to reduce the output voltage deviation.

For a given input and output requirement, the following inequality gives an approximation for an absolute minimum output cap required:

$$C_{OUT} > \frac{1}{(F_S \times r \times \Delta V_{OUT} / I_{OUT})} \times \left[ \left( \frac{r^2}{12} \times (1 + D') \right) + (D' \times (1 + r)) \right] \tag{19}$$

Along with this for the same requirement, the max ESR should be calculated as per the following inequality

$$ESR < \frac{D'}{F_S \times C_{OUT}} \times \left( \frac{1}{r} + 0.5 \right) \tag{20}$$

where

r = Ripple ratio of the inductor ripple current ($\Delta I_L$ / $I_{OUT}$)

$\Delta V_{OUT}$ = Target output voltage undershoot

D' = 1 – Duty cycle

$F_S$ = Switching Frequency

$I_{OUT}$ = Load Current

A general guide line for $C_{OUT}$ range is that $C_{OUT}$ should be larger than the minimum required output capacitance calculated by Equation 19, and smaller than 10 times the minimum required output capacitance or 1 mF. In applications with $V_{OUT}$ less than 3.3 V, it is critical that low ESR output capacitors are selected. This will limit potential output voltage overshoots as the input voltage falls below the device normal operating range. To optimize the transient behavior a feed-forward capacitor could be added in parallel with the upper feedback resistor. For this design example, three 47 µF,10 V, X7R ceramic capacitors are used in parallel.

#### 8.2.2.7 Feed-Forward Capacitor

The LM43602 is internally compensated and the internal R-C values are 400 kΩ and 50 pF respectively. Depending on the $V_{OUT}$ and frequency $F_S$, if the output capacitor $C_{OUT}$ is dominated by low ESR (ceramic types) capacitors, it could result in low phase margin. To improve the phase boost an external feedforward capacitor $C_{FF}$ can be added in parallel with $R_{FBT}$. $C_{FF}$ is chosen such that phase margin is boosted at the crossover frequency without $C_{FF}$. A simple estimation for the crossover frequency without $C_{FF}$ ($f_x$) is shown in Equation 21, assuming $C_{OUT}$ has very small ESR.

$$f_x = \frac{4.35}{V_{OUT} \times C_{OUT}} \tag{21}$$

The following equation for $C_{FF}$ was tested:

$$C_{FF} = \frac{1}{2\pi f_x} \times \frac{1}{\sqrt{R_{FBT} \times (R_{FBT} \,//\, R_{FBB})}} \tag{22}$$

This equation indicates that the crossover frequency is geometrically centered on the zero and pole frequencies caused by the $C_{FF}$ capacitor.

For designs with higher ESR, $C_{FF}$ is not neeed when $C_{OUT}$ has very high ESR and $C_{FF}$ calculated from Equation 22 should be reduced with medium ESR. Table 2 can be used as a quick starting point.

For the application in this design example, a 100 pF COG capacitor is selected.

#### 8.2.2.8 Bootstrap Capacitors

Every LM43602 design requires a bootstrap capacitor, $C_{BOOT}$. The recommended bootstrap capacitor is 0.47 µF and rated at 6.3 V or higher. The bootstrap capacitor is located between the SW pin and the CBOOT pin. The bootstrap capacitor must be a high-quality ceramic type with X7R or X5R grade dielectric for temperature stability.

#### 8.2.2.9 VCC Capacitor

The VCC pin is the output of an internal LDO for LM43602. The input for this LDO comes from either VIN or BIAS (please refer to Functional Block Diagram for LM43602). To insure stability of the part, place a minimum of 2.2 µF, 10 V capacitor from this pin to ground.

#### 8.2.2.10 BIAS Capacitors

For an output voltage of 3.3 V and greater, the BIAS pin can be connected to the output in order to increase light load efficiency. This pin is an input for the VCC LDO. When BIAS is not connected, the input for the VCC LDO will be internally connected into VIN. Since this is an LDO, the voltage differences between the input and output will affect the efficiency of the LDO. If necessary, a capacitor with a value of 1 µF can be added close to the BIAS pin as an input capacitor for the LDO.

#### 8.2.2.11 Soft-Start Capacitors

The user can left the SS/TRK pin floating and the LM43602 will implement a soft start time of 4.1 ms typically. In order to use an external soft start capacitor, the capacitor should be sized such that the soft start time will be longer than 4.1 ms. Use the following equation in order to calculate the soft start capacitor value:

$$C_{SS} = I_{SSC} \times t_{SS} \tag{23}$$

Where,

$C_{SS}$ = Soft start capacitor value (µF)

$I_{SS}$ = Soft start charging current (µA)

$t_{SS}$ = Desired soft start time (s)

For the desired soft start time of 10 ms and soft start charging current of 2.0 µA, the equation above yield a soft start capacitor value of 0.020 µF.

#### *8.2.2.12 Under Voltage Lockout Set-Point*

The undervoltage lockout (UVLO) is adjusted using the external voltage divider network of $R_{ENT}$ and $R_{ENB}$. $R_{ENT}$ is connected between VIN and the EN pin of the LM43602 device. $R_{ENB}$ is connected between the EN pin and the GND pin. The UVLO has two thresholds, one for power up when the input voltage is rising and one for power down or brown outs when the input voltage is falling. The following equation can be used to determine the VIN (UVLO) level.

$$V_{IN\text{-}UVLO\text{-}RISING} = V_{ENH} \times (R_{ENB} + R_{ENT}) / R_{ENB} \quad (24)$$

The EN rising threshold ($V_{ENH}$) for LM43602 is set to be 2.2 V (typical). Choose the value of $R_{ENB}$ to be 1 MΩ to minimize input current from the supply. If the desired VIN UVLO level is at 5.0 V, then the value of $R_{ENT}$ can be calculated using the equation below:

$$R_{ENT} = (V_{IN\text{-}UVLO\text{-}RISING} / V_{ENH} - 1) \times R_{ENB} \quad (25)$$

The above equation yields a value of 1.27 MΩ. The resulting falling UVLO threshold, equals 4.3 V, can be calculated by below equation, where EN falling threshold ($V_{ENL}$) is 1.9 V (typical).

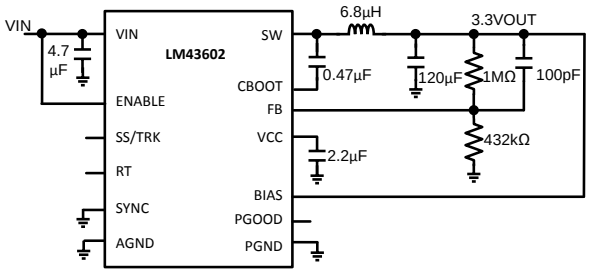
$$V_{IN\text{-}UVLO\text{-}FALLING} = V_{ENL} \times (R_{ENB} + R_{ENT}) / R_{ENB} \quad (26)$$

#### *8.2.2.13 PGOOD*

A typical pull-up resistor value is 10 kΩ to 100 kΩ from PGOOD pin to a voltage no higher than 12 V. If it is desired to pull up PGOOD pin to a voltage higher than 12 V, a resistor can be added from PGOOD pin to ground to divide the voltage seen by the PGOOD pin to a value no higher than 12 V.

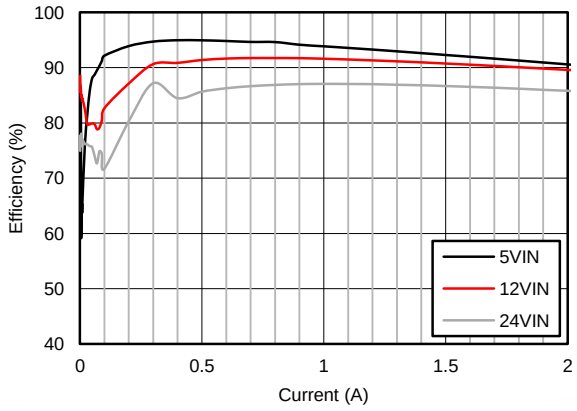
### 8.2.3 Application Performance Curves

Unless otherwise specified, $V_{IN}$ = 12V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz. Please refer to Application Performance Curves for Bill of materials for each $V_{OUT}$ and $F_S$ combination.



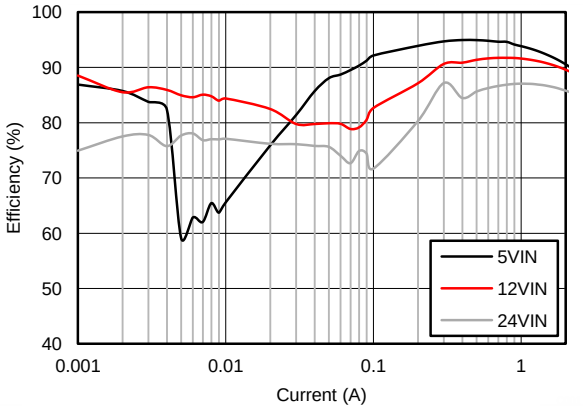

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 39. BOM for $V_{OUT}$ = 3.3 V $F_S$ = 500 kHz**



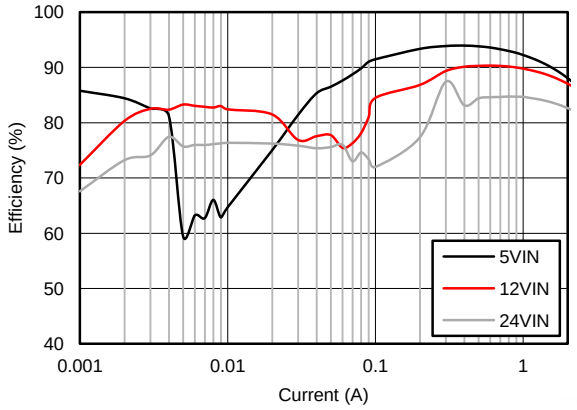

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 40. Efficiency at Room Temperature**



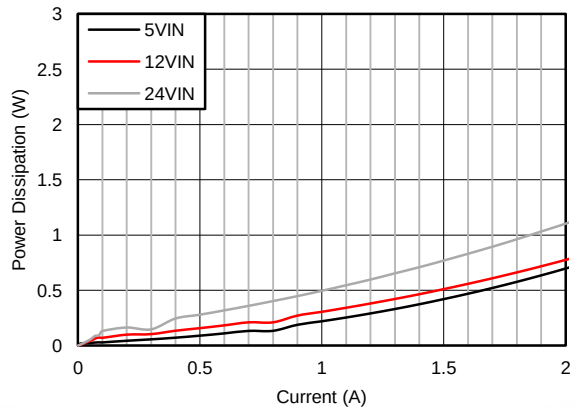

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 41. Efficiency at Room Temperature**



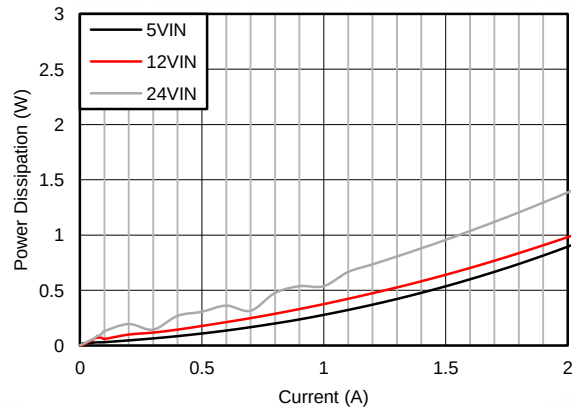

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 42. Efficiency at 85°C**




$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

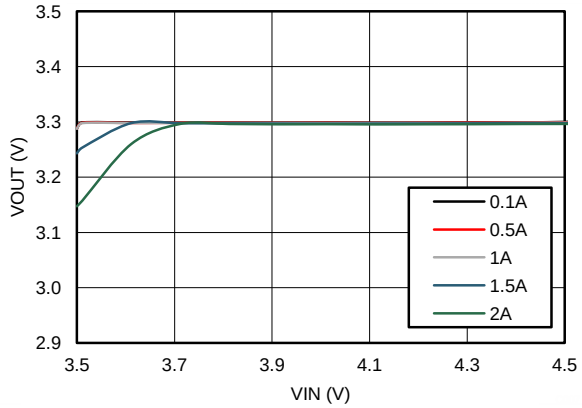
**Figure 43. Power Loss at Room Temperature**




$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz $V_{IN}$ = 24 V

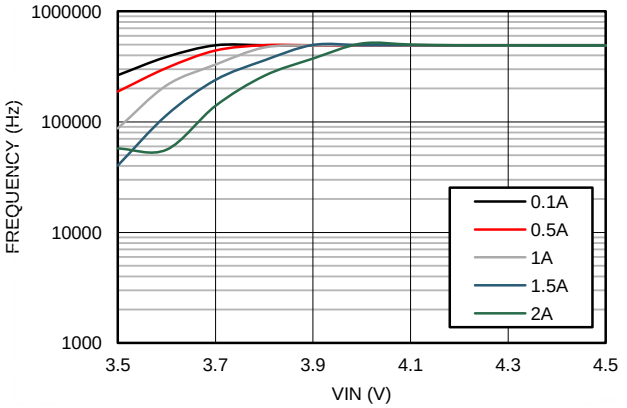
**Figure 44. Power Loss at 85°C**

Unless otherwise specified, $V_{IN}$ = 12V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz. Please refer to Application Performance Curves for Bill of materials for each $V_{OUT}$ and $F_S$ combination.



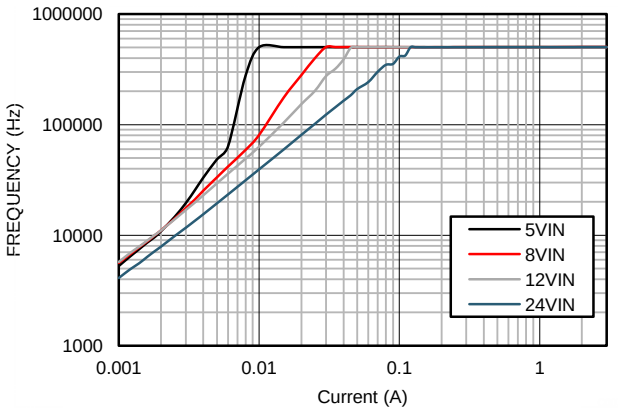

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 45. Dropout Voltage**



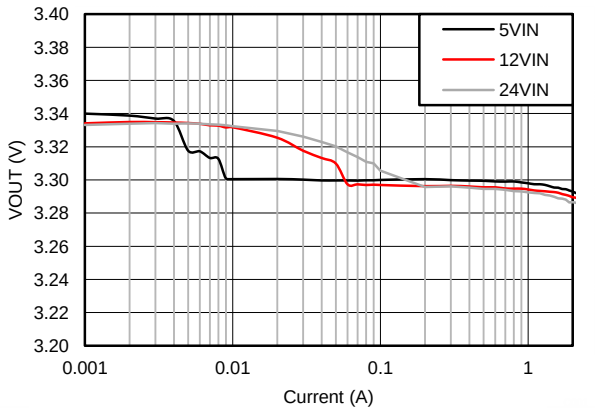

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 46. Frequency vs VIN**



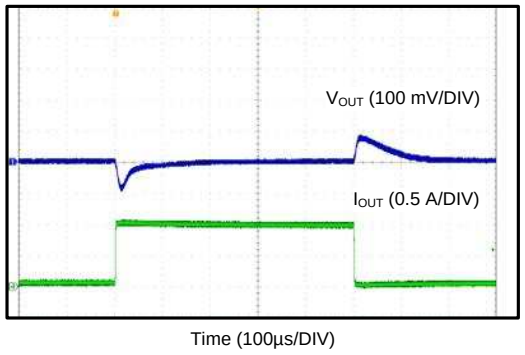

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 47. Frequency vs Load**



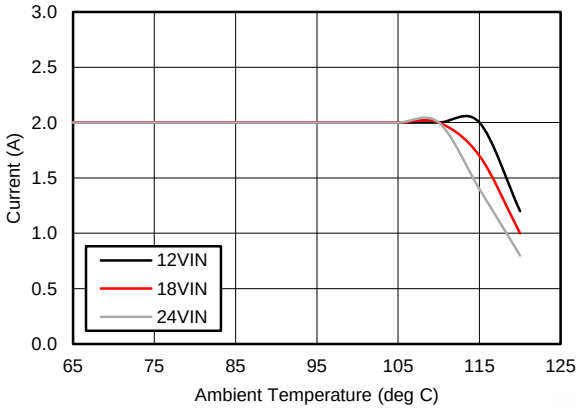

$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

**Figure 48. Regulation Curve**




$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz VIN =12 V

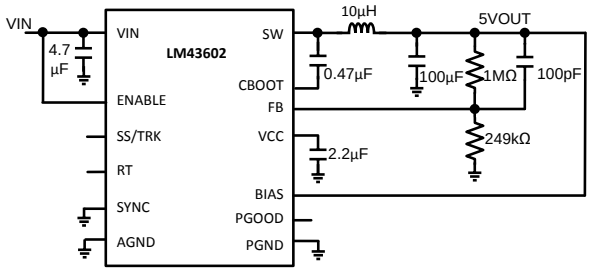
**Figure 49. Load Transient**




$V_{OUT}$ = 3.3 V $F_S$ = 500 kHz

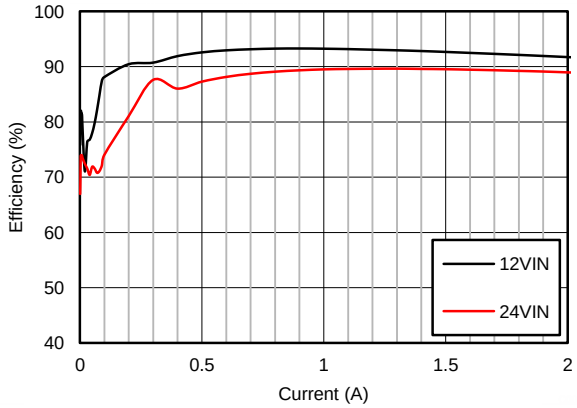
**Figure 50. Derating Curve**

Unless otherwise specified, $V_{IN}$ = 12V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz. Please refer to Application Performance Curves for Bill of materials for each $V_{OUT}$ and $F_S$ combination.



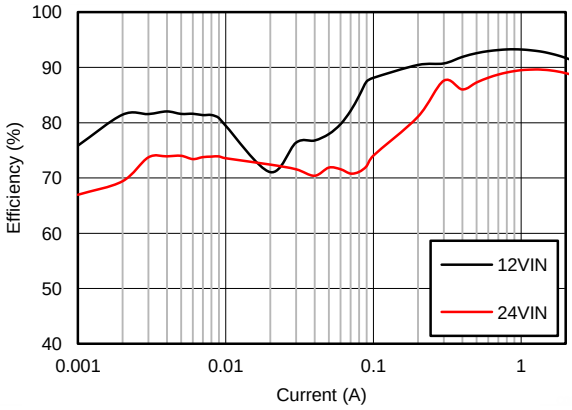

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 51. BOM for $V_{OUT}$ = 5 V $F_S$ = 500 kHz**



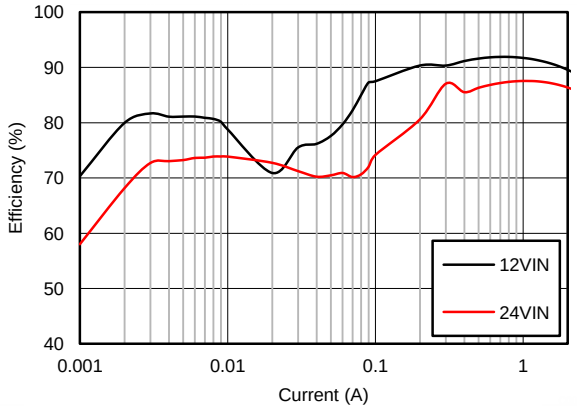

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 52. Efficiency at Room Temperature**



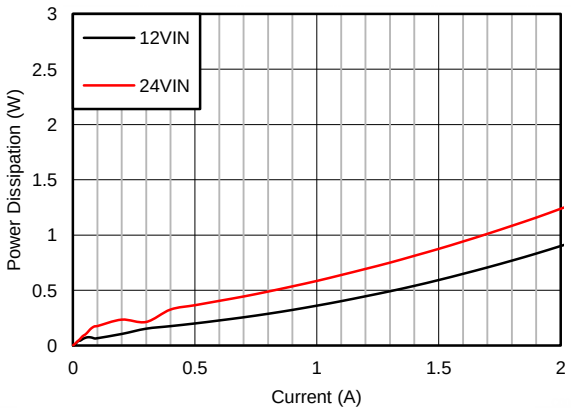

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 53. Efficiency at Room Temperature**



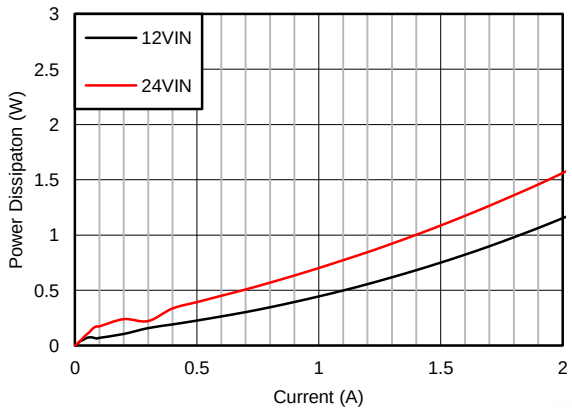

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 54. Efficiency at 85°C Ambient Temperature**




$V_{OUT}$ = 5 V $F_S$ = 500 kHz

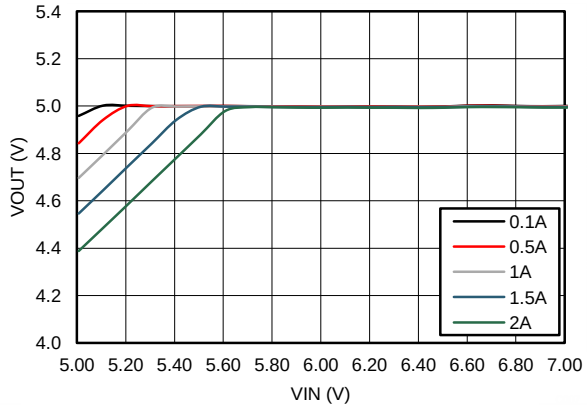
**Figure 55. Power Dissipation at Room Temperature**




$V_{OUT}$ = 5 V $F_S$ = 500 kHz

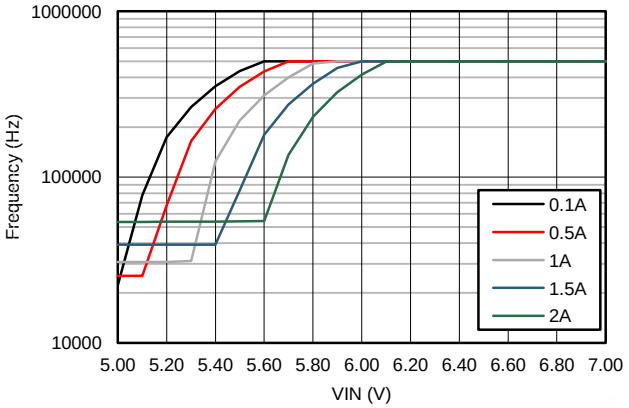
**Figure 56. Power Dissipation at 85C Ambient Temperature**

Unless otherwise specified, $V_{IN}$ = 12V, $V_{OUT}$ = 3.3 V, $F_S$ = 500 kHz. Please refer to Application Performance Curves for Bill of materials for each $V_{OUT}$ and $F_S$ combination.



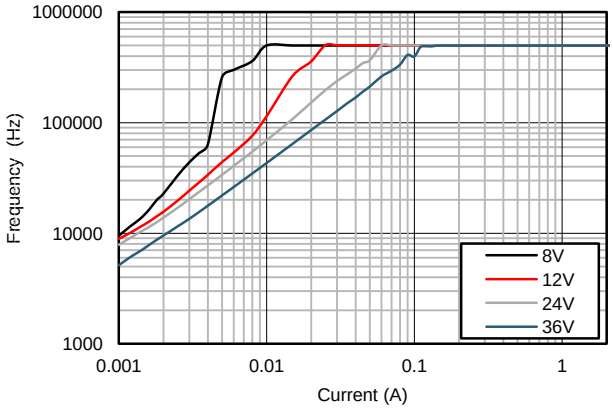

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 57. Dropout Voltage**



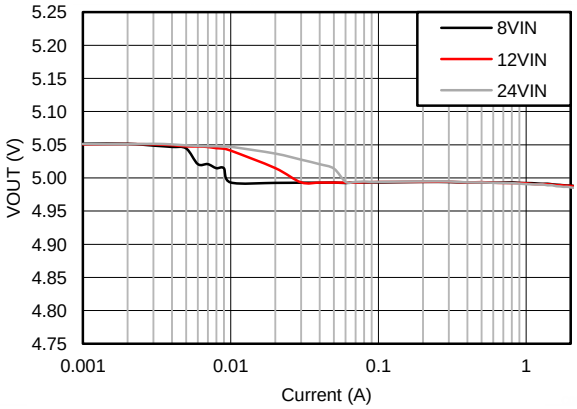

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 58. Frequency vs VIN**



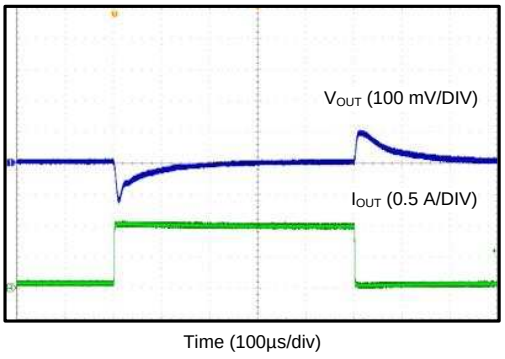

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 59. Frequency vs Load**



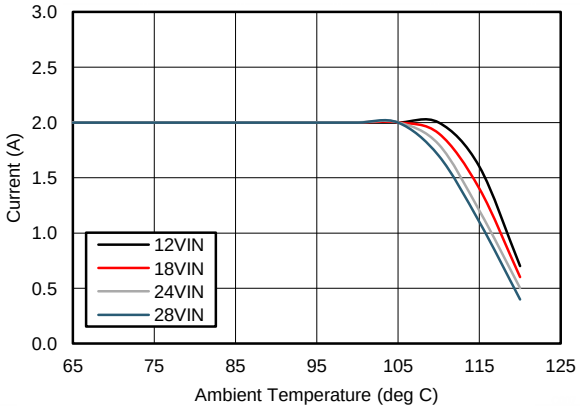

$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 60. Regulation Curve**




$V_{OUT}$ = 5 V $F_S$ = 1 MHz $V_{IN}$ = 12V

**Figure 61. Load Transient 0.1A to 1A**




$V_{OUT}$ = 5 V $F_S$ = 500 kHz

**Figure 62. Derating Curve**

# 9 Power Supply Recommendations

The LM43602 is designed to operate from an input voltage supply range between 3.5 V and 60 V. This input supply should be well regulated and able to withstand maximum input current and maintain a stable voltage. The resistance of the input supply rail should be low enough that an input current transient does not cause a high enough drop at the LM43602 supply voltage that can cause a false UVLO fault triggering and system reset.

If the input supply is located more than a few inches from the LM43602 additional bulk capacitance may be required in addition to the ceramic bypass capacitors. The amount of bulk capacitance is not critical, but a 47 µF or 100 µF electrolytic capacitor is a typical choice.

# 10 Layout

The performance of any switching converter depends as much upon the layout of the PCB as the component selection. The following guidelines will help users design a PCB with the best power conversion performance, thermal performance, and minimized generation of unwanted EMI.

## 10.1 Layout Guidelines

1. Place ceramic high frequency bypass $C_{IN}$ as close as possible to the LM43602 VIN and PGND pins. Grounding for both the input and output capacitors should consist of localized top side planes that connect to the PGND pins and PAD.
2. Place bypass capacitors for VCC and BIAS close to the pins and ground the bypass capacitors to device ground.
3. Minimize trace length to the FB pin net. Both feedback resistors, $R_{FBT}$ and $R_{FBB}$ should be located close to the FB pin. Place Cff directly in parallel with $R_{FBT}$. If $V_{OUT}$ accuracy at the load is important, make sure $V_{OUT}$ sense is made at the load. Route $V_{OUT}$ sense path away from noisy nodes and preferably through a layer on the other side of a shieldig layer.
4. Use ground plane in one of the middle layers as noise shielding and heat dissipation path.
5. Have a single point ground connection to the plane. The ground connections for the feedback, soft-start, and enable components should be routed to the ground plane. This prevents any switched or load currents from flowing in the analog ground traces. If not properly handled, poor grounding can result in degraded load regulation or erratic output voltage ripple behavior.
6. Make $V_{IN}$, $V_{OUT}$ and ground bus connections as wide as possible. This reduces any voltage drops on the input or output paths of the converter and maximizes efficiency.
7. Provide adequate device heat-sinking. Use an array of heat-sinking vias to connect the exposed pad to the ground plane on the bottom PCB layer. If the PCB has multiple copper layers, these thermal vias can also be connected to inner layer heat-spreading ground planes. Ensure enough copper area is used for heat-sinking to keep the junction temperature below 125°C.

### 10.1.1 Compact Layout for EMI Reduction

Radiated EMI is generated by the high di/dt components in pulsing currents in switching converters. The larger area covered by the path of a pulsing current, the more EMI is generated. The key to minimize radiated EMI is to identify pulsing current path and minimize the area of the path. In Buck converters,the pulsing current path is from the $V_{IN}$ side of the input capacitors to HS switch, to the LS switch, and then return to the ground of the input capacitors, as shown in Figure 63.

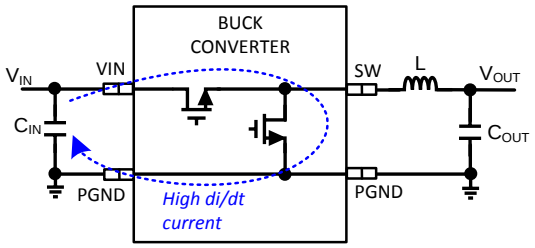



**Figure 63. Buck Converter High Δi/Δt Path**

## Layout Guidelines (continued)

High frequency ceramic bypass capacitors at the input side provide primary path for the high di/dt components of the pulsing current. Placing ceramic bypass capacitor(s) as close as possible to the VIN and PGND pins is the key to EMI reduction.

The SW pin connecting to the inductor should be as short as possible, and just wide enough to carry the load current without excessive heating. Short, thick traces or copper pours (shapes) should be used for high current condution path to minimize parasitic resistance. The output capacitors should be place close to the $V_{OUT}$ end of the inductor and closely grounded to PGND pin and exposed PAD.

The bypass capacitors on VCC and BIAS pins should be placed as close as possible to the pins respectively and closely grounded to PGND and the exposed PAD.

### 10.1.2 Ground Plane and Thermal Considerations

It is recommended to use one of the middle layers as a solid ground plane. Ground plane provides shielding for sensitive circuits and traces. It also provides a quiet reference potential for the control circuitry. The AGND and PGND pins should be connected to the ground plane using vias right next to the bypass capacitors. PGND pins are connected to the source of the internal LS switch. They should be connected directly to the grounds of the input and output capacitors. The PGND net contains noise at switching frequency and may bounce due to load variations. PGND trace, as well as PVIN and SW traces, should be constrained to one side of the ground plane. The other side of the ground plane contains much less noise and should be used for sensitive routes.

It is recommended to provide adequate device heat sinking by utilizing the PAD of the IC as the primary thermal path. Use a minimum 4 by 4 array of 10 mil thermal vias to connect the PAD to the system ground plane heat sink. The vias should be evenly distributed under the PAD. Use as much copper as possible for system ground plane on the top and bottom layers for the best heat dissipation. Use a four-layer board with the copper thickness for the four layers, starting from the top one, 2 oz / 1 oz / 1 oz / 2 oz. Four layer boards with enough copper thickness provides low current conduction impedance, proper shielding and lower thermal resistance.

The thermal characteristics of the LM46002 are specified using the parameter RθJA, which characterize the junction temperature of the silicon to the ambient temperature in a specific system. Although the value of $\theta_{JA}$ is dependant on many variables, it still can be used to approximate the operating junction temperature of the device. To obtain an estimate of the device junction temperature, one may use the following relationship:

$$T_J = P_D \times \theta_{JA} + T_A \quad (27)$$

where

$T_J$ = Junction temperature in °C

$P_D = V_{IN} \times I_{IN} \times (1 - \text{Efficiency}) - 1.1 \times I_{OUT} \times \text{DCR}$

DCR = Inductor DC parasitic resistance in Ω

$\theta_{JA}$ = Junction-to-ambient thermal resistance of the device in °C/W

$T_A$ = Ambient temperature in °C.

The maximum operating junction temperature of the LM43602 is 125°C. $\theta_{JA}$ is highly related to PCB size and layout, as well as enviromental factors such as heat sinking and air flow. Figure 64 shows measured results of $R_{\theta JA}$ with different copper area on a 2-layer board and a 4-layer board.

## Layout Guidelines (continued)

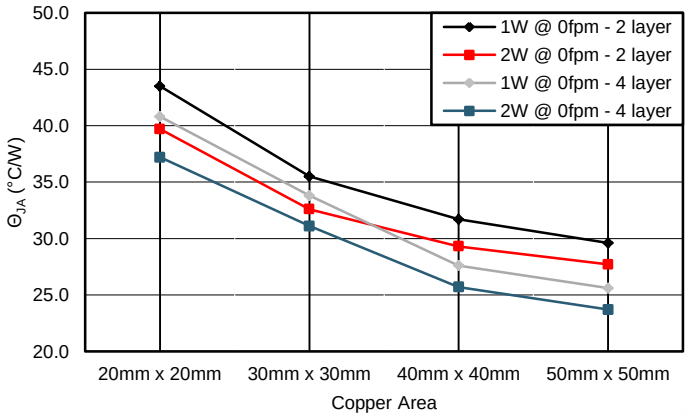



**Figure 64. $R_{\theta JA}$ vs Copper Area**
**2 oz Copper on Outer Layers and 1oz Copper on Inner Layers**

### 10.1.3 Feedback Resistors

To reduce noise sensitivity of the output voltage feedback path, it is important to place the resistor divider and $C_{FF}$ close to the FB pin, rather than close to the load. The FB pin

is the input to the error amplifier, so it is a high impedance node and very sensitive to noise. Placing the resistor divider and $C_{FF}$ closer to the FB pin reduces the trace length of FB signal and reduces noise coupling. The output node is a low impedance node, so the trace from $V_{OUT}$ to the resistor divider can be long if short path is not available.

If voltage accuracy at the load is important, make sure voltage sense is made at the load. Doing so will correct for voltage drops along the traces and provide the best output accuracy. The voltage sense trace from the load to the feedback resistor divider should be routed away from the SW node path and the inductor to avoid contaminating the feedback signal with switch noise, while also minimizing the trace length. This is most important when high-value resistors are used to set the output voltage. This provides further shielding for the voltage feedback path from EMI noises.

## 10.2 Layout Example

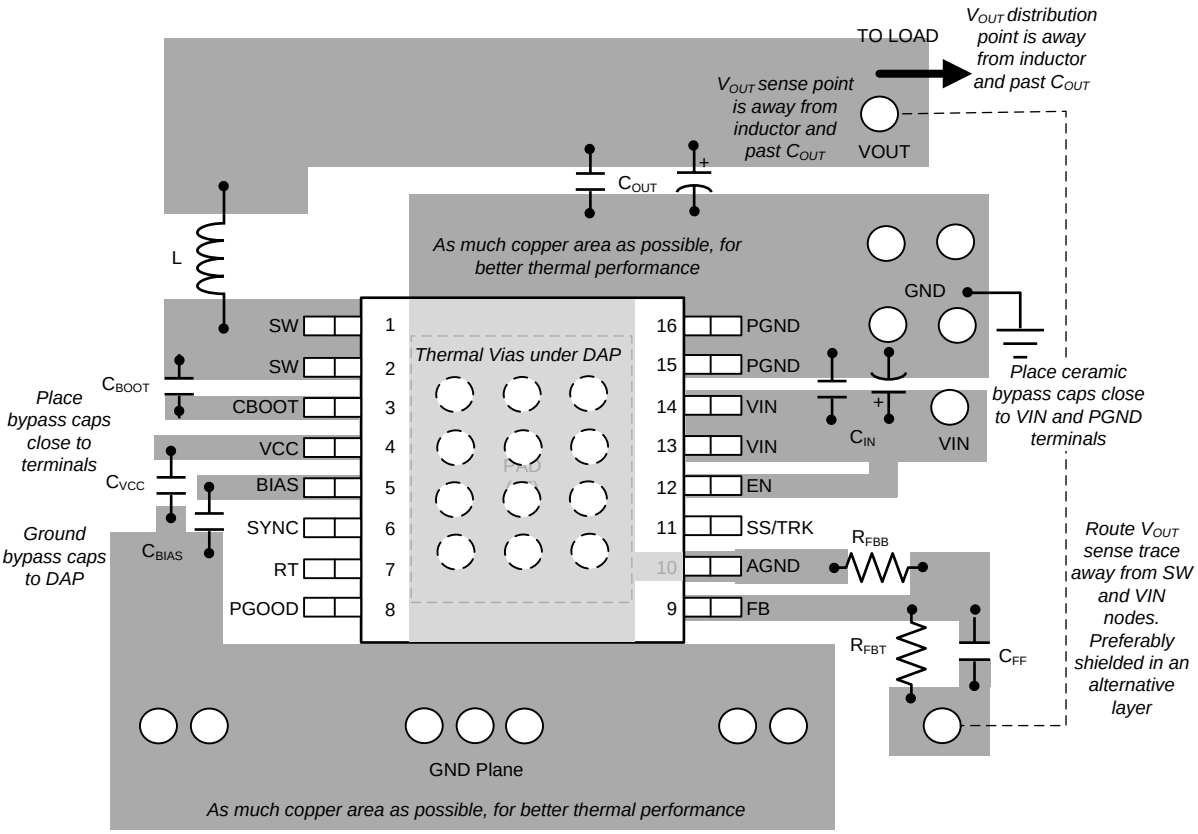



**Figure 65. LM43602 Board Layout Recommendations**

# 11 器件和文档支持

## 11.1 器件支持

### 11.1.1 开发支持

#### *11.1.1.1 使用 WEBENCH® 工具创建定制设计*

请单击此处，使用 LM43602 器件并借助 WEBENCH® 电源设计器创建定制设计方案。

1. 在开始阶段键入输出电压 ($V_{IN}$)、输出电压 ($V_{OUT}$) 和输出电流 ($I_{OUT}$) 要求。
2. 使用优化器拨盘优化关键设计参数，如效率、封装和成本。
3. 将生成的设计与德州仪器 (TI) 的其他解决方案进行比较。

WEBENCH Power Designer 提供一份定制原理图以及罗列实时价格和组件可用性的物料清单。

在多数情况下，可执行以下操作：

- 运行电气仿真，观察重要波形以及电路性能
- 运行热性能仿真，了解电路板热性能
- 将定制原理图和布局方案导出至常用 CAD 格式
- 打印设计方案的 PDF 报告并与同事共享

有关 WEBENCH 工具的详细信息，请访问 www.ti.com/WEBENCH。

## 11.2 文档支持

### 11.2.1 相关文档

请参阅如下相关文档：

- 《*LM43602 EVM 用户指南*》(
- 《*使用新的热指标*》 应用 报告 (SBVA025)。
- 《*采用前馈电容优化内部补偿 DC-DC 转换器的瞬态响应*》（文献编号：SLVA289）。
- 《*轻松抑制 DC-DC 转换器中的传导性 EMI*》（文献编号：SNVA489）。
- AN-1149《*开关电源布局指南*》 SNVA021
- AN-1229《*Simple Switcher PCB 布局指南*》 SNVA054
- 《*构建电源 - 布局注意事项*》 SLUP230
- 《*使用 LM4360x 与 LM4600x 简化低辐射 EMI 布局*》 SNVA721
- AN-2020《*热设计：学会洞察先机，不做事后诸葛*》 SNVA419
- AN-1520《*外露焊盘封装实现最佳热阻性的电路板布局指南*》 SNVA183
- 《*半导体和 IC 封装热指标*》SPRA953
- 《*使用 LM43603 和 LM43602 简化热设计*》 SNVA719
- 《*PowerPAD™ 热增强型封装*》 SLMA002
- 《*PowerPAD 速成*》SLMA004
- 《*使用新的热指标*》 SBVA025

## 11.3 相关链接

表 **4.** 相关链接

| 器件 | 产品文件夹 | 样片与购买 | 技术文档 | 工具和软件 | 支持和社区 |
|---|---|---|---|---|---|
| LM43603 | 请单击此处 | 请单击此处 | 请单击此处 | 请单击此处 | 请单击此处 |

## 11.4 接收文档更新通知

要接收文档更新通知，请转至 TI.com 上的器件产品文件夹。单击右上角的*通知我* 进行注册，即可每周接收产品信息更改摘要。有关更改的详细信息，请查看任何已修订文档中包含的修订历史记录。

## 11.5 社区资源

**下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商“按照原样”提供。这些内容并不构成 TI 技术规范，并且不一定反映 TI 的观点；请参阅 TI 的 《使用条款》。**

**TI E2E™ 在线社区** ***TI 的工程师对工程师 (E2E) 社区。*** **此社区的创建目的在于促进工程师之间的协作。在 e2e.ti.com 中，您可以咨询问题、分享知识、拓展思路并与同行工程师一道帮助解决问题。**

**设计支持** ***TI 参考设计支持*** **可帮助您快速查找有帮助的 E2E 论坛、设计支持工具以及技术支持的联系信息。**

## 11.6 商标

《PowerPAD, E2E are trademarks of Texas Instruments.
WEBENCH is a registered trademark of Texas Instruments.
All other trademarks are the property of their respective owners.

## 11.7 静电放电警告

ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序，可能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级，大至整个器件故障。 精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

## 11.8 Glossary

SLYZ022 — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 机械、封装和可订购信息

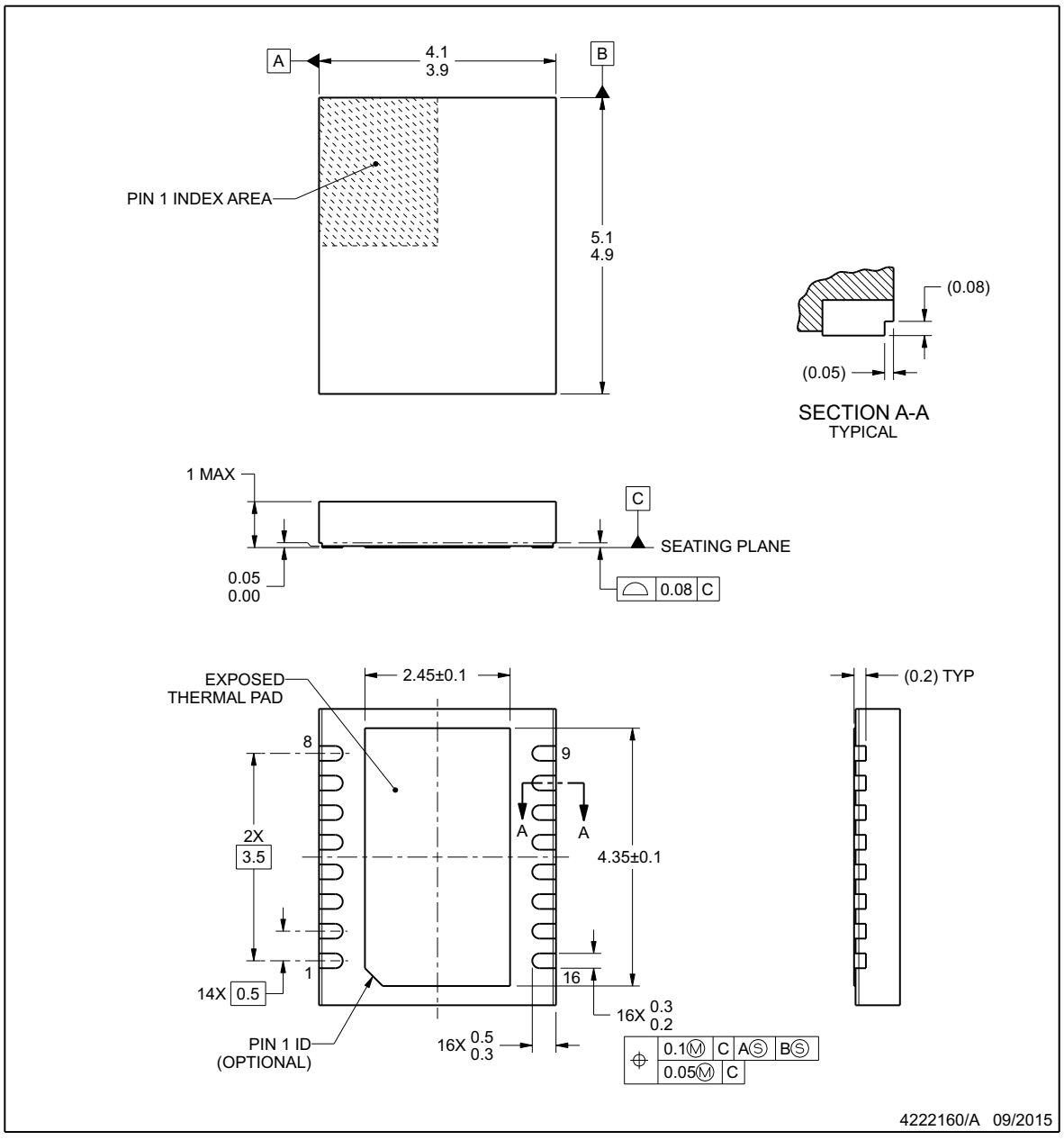
以下页中包括机械封装、封装和可订购信息。这些信息是针对指定器件可提供的最新数据。这些数据如有变更，恕不另行通知和修订此文档。如欲获取此产品说明书的浏览器版本，请参阅左侧的导航。

# PACKAGE OUTLINE

## DSU0016A

## VSON - 1 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



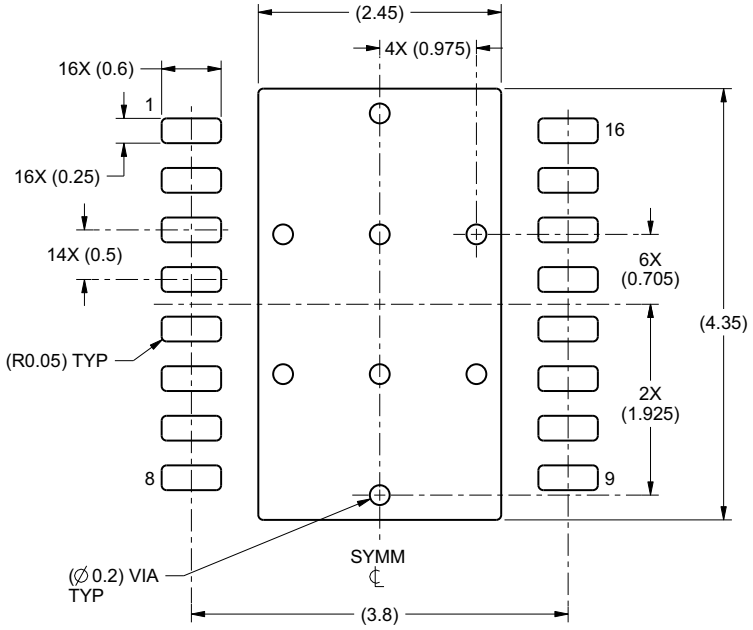

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

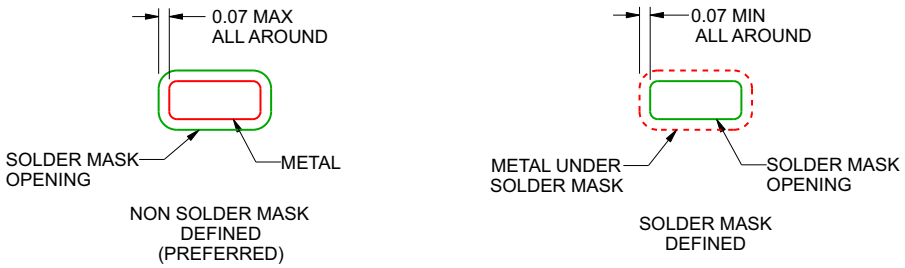
## EXAMPLE BOARD LAYOUT

**DSU0016A** — **VSON - 1 mm max height**

PLASTIC SMALL OUTLINE - NO LEAD




LAND PATTERN EXAMPLE
SCALE:15X




SOLDER MASK DETAILS

4222160/A 09/2015

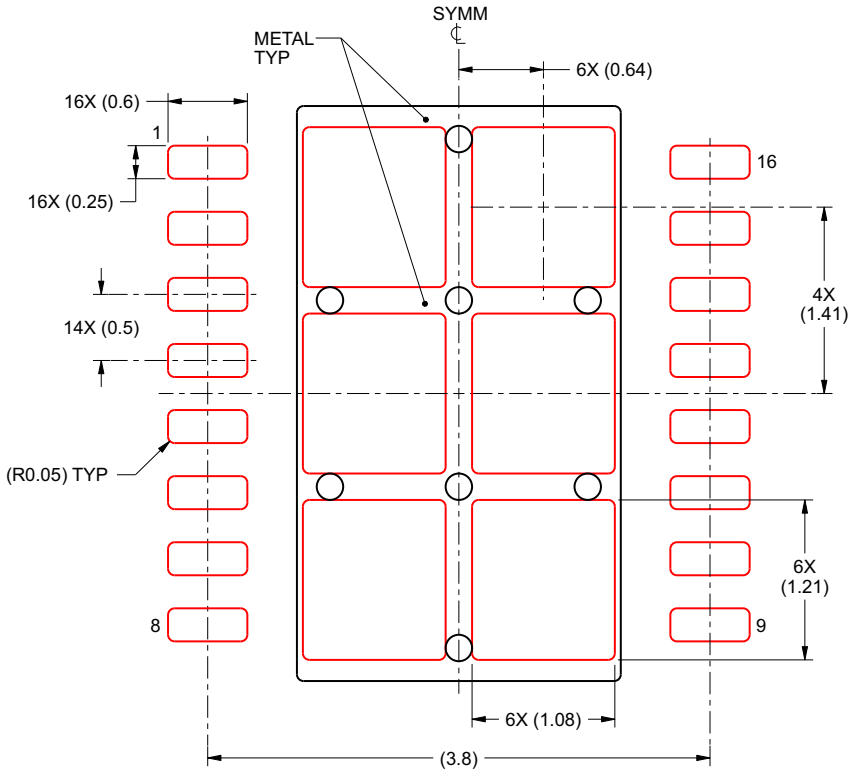
NOTES: (continued)

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

## EXAMPLE STENCIL DESIGN

**DSU0016A** — **VSON - 1 mm max height**

PLASTIC SMALL OUTLINE - NO LEAD




SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD
74% PRINTED SOLDER COVERAGE BY AREA
SCALE:20X

4222160/A 09/2015

NOTES: (continued)

5. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

## PACKAGING INFORMATION

| Orderable Device | Status (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan (2) | Lead finish/ Ball material (6) | MSL Peak Temp (3) | Op Temp (°C) | Device Marking (4/5) | Samples |
|---|---|---|---|---|---|---|---|---|---|---|---|
| LM43602DSUR | ACTIVE | SON | DSU | 16 | 3000 | RoHS & Green | SN | Level-2-260C-1 YEAR | -40 to 125 | LM43602 | Samples |
| LM43602DSUT | ACTIVE | SON | DSU | 16 | 250 | RoHS & Green | SN | Level-2-260C-1 YEAR | -40 to 125 | LM43602 | Samples |
| LM43602PWP | ACTIVE | HTSSOP | PWP | 16 | 90 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | LM43602 | Samples |
| LM43602PWPR | ACTIVE | HTSSOP | PWP | 16 | 2000 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | LM43602 | Samples |
| LM43602PWPT | ACTIVE | HTSSOP | PWP | 16 | 250 | RoHS & Green | NIPDAU | Level-2-260C-1 YEAR | -40 to 125 | LM43602 | Samples |

(1) The marketing status values are defined as follows:
**ACTIVE:** Product device recommended for new designs.
**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.
**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

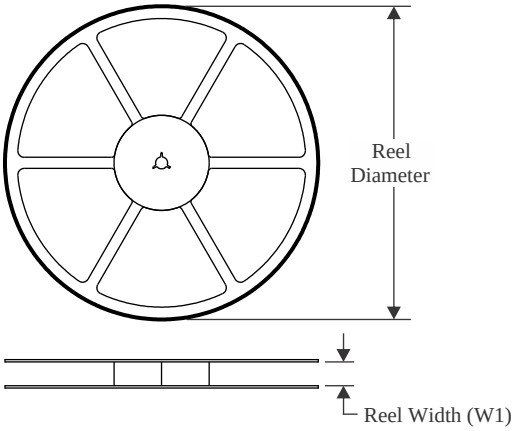
(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

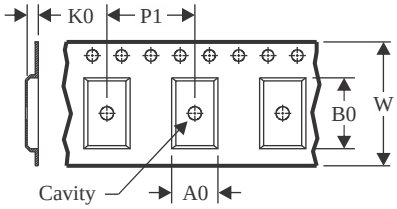
(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

## TAPE AND REEL INFORMATION

**REEL DIMENSIONS**

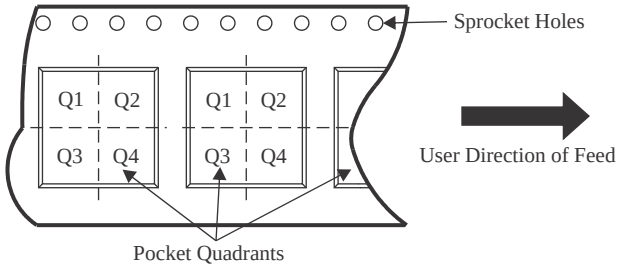



**TAPE DIMENSIONS**




| | |
|---|---|
| A0 | Dimension designed to accommodate the component width |
| B0 | Dimension designed to accommodate the component length |
| K0 | Dimension designed to accommodate the component thickness |
| W | Overall width of the carrier tape |
| P1 | Pitch between successive cavity centers |

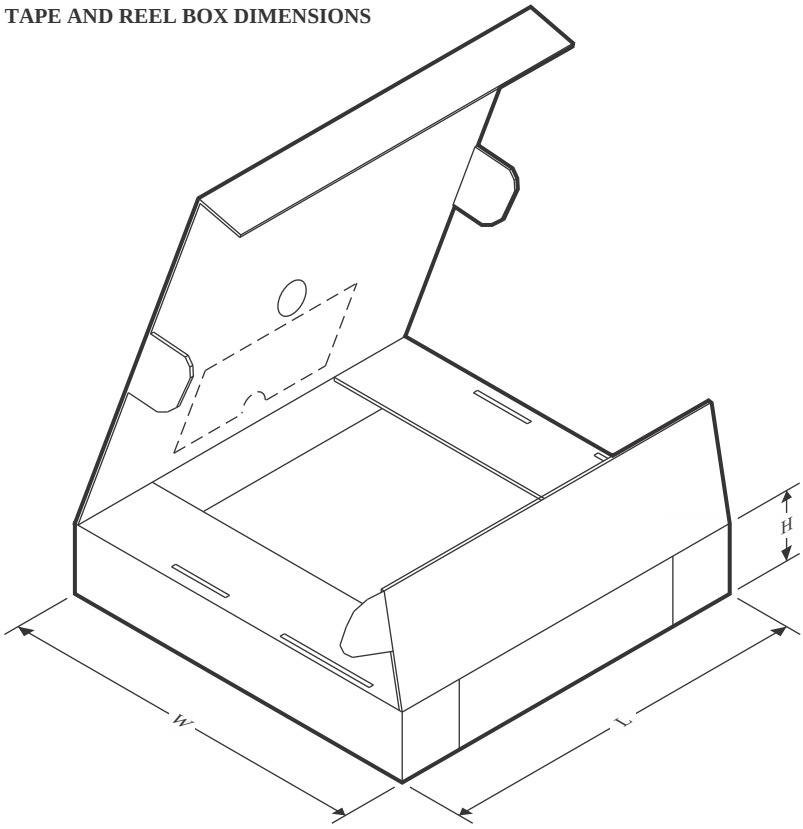
**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**




*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | A0 (mm) | B0 (mm) | K0 (mm) | P1 (mm) | W (mm) | Pin1 Quadrant |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| LM43602DSUR | SON | DSU | 16 | 3000 | 330.0 | 12.4 | 4.3 | 5.3 | 1.3 | 8.0 | 12.0 | Q1 |
| LM43602DSUT | SON | DSU | 16 | 250 | 180.0 | 12.4 | 4.3 | 5.3 | 1.3 | 8.0 | 12.0 | Q1 |
| LM43602PWPR | HTSSOP | PWP | 16 | 2000 | 330.0 | 12.4 | 6.9 | 5.6 | 1.6 | 8.0 | 12.0 | Q1 |

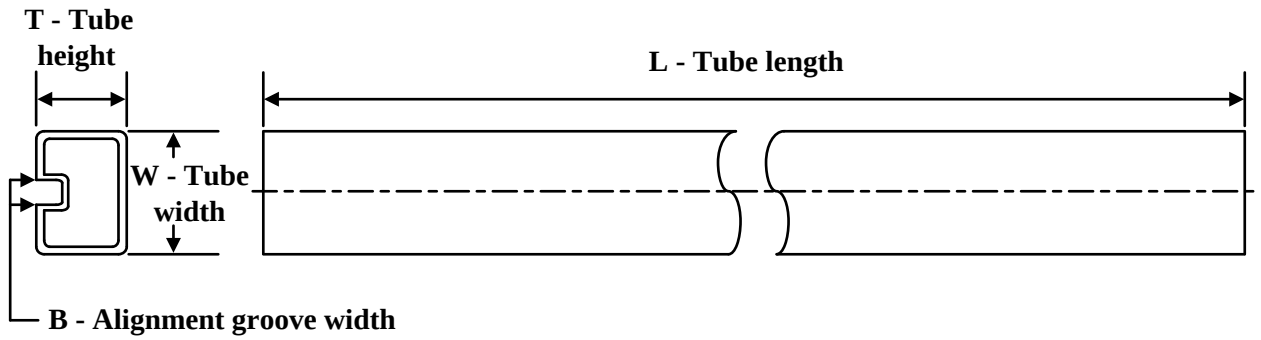
TAPE AND REEL BOX DIMENSIONS




*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
|---|---|---|---|---|---|---|---|
| LM43602DSUR | SON | DSU | 16 | 3000 | 367.0 | 367.0 | 38.0 |
| LM43602DSUT | SON | DSU | 16 | 250 | 213.0 | 191.0 | 35.0 |
| LM43602PWPR | HTSSOP | PWP | 16 | 2000 | 350.0 | 350.0 | 43.0 |

## TUBE




*All dimensions are nominal

| Device | Package Name | Package Type | Pins | SPQ | L (mm) | W (mm) | T (µm) | B (mm) |
|---|---|---|---|---|---|---|---|---|
| LM43602PWP | PWP | HTSSOP | 16 | 90 | 530 | 10.2 | 3600 | 3.5 |

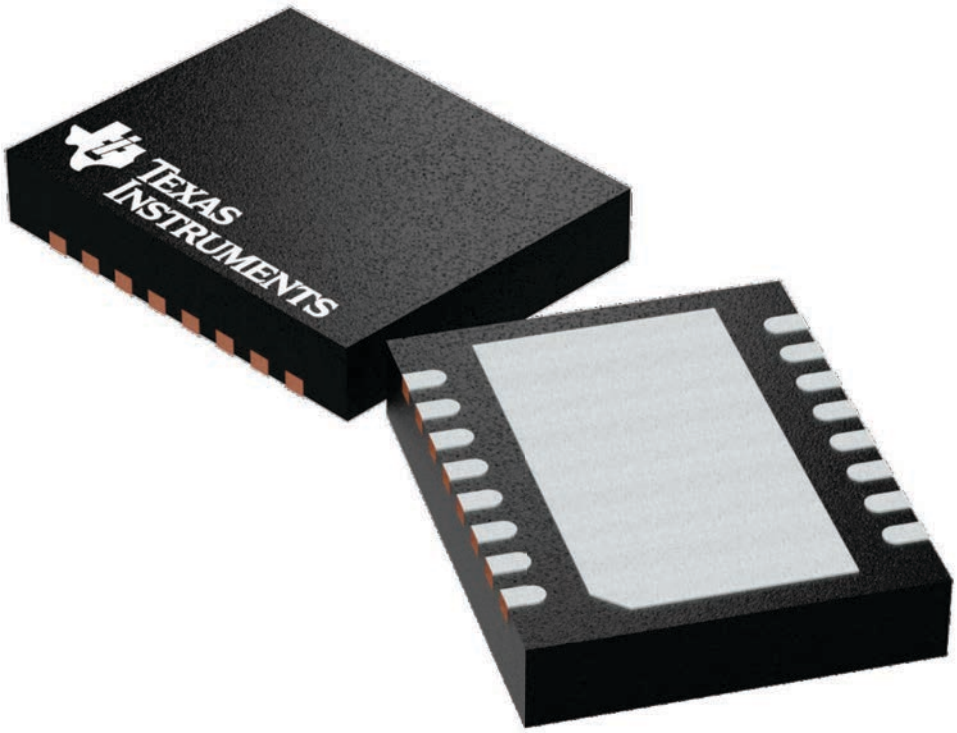
# GENERIC PACKAGE VIEW

## DSU 16

## VSON - 1 mm max height

**4 x 5, 0.5 mm pitch**

PLASTIC SMALL OUTLINE - NO LEAD




Images above are just a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.

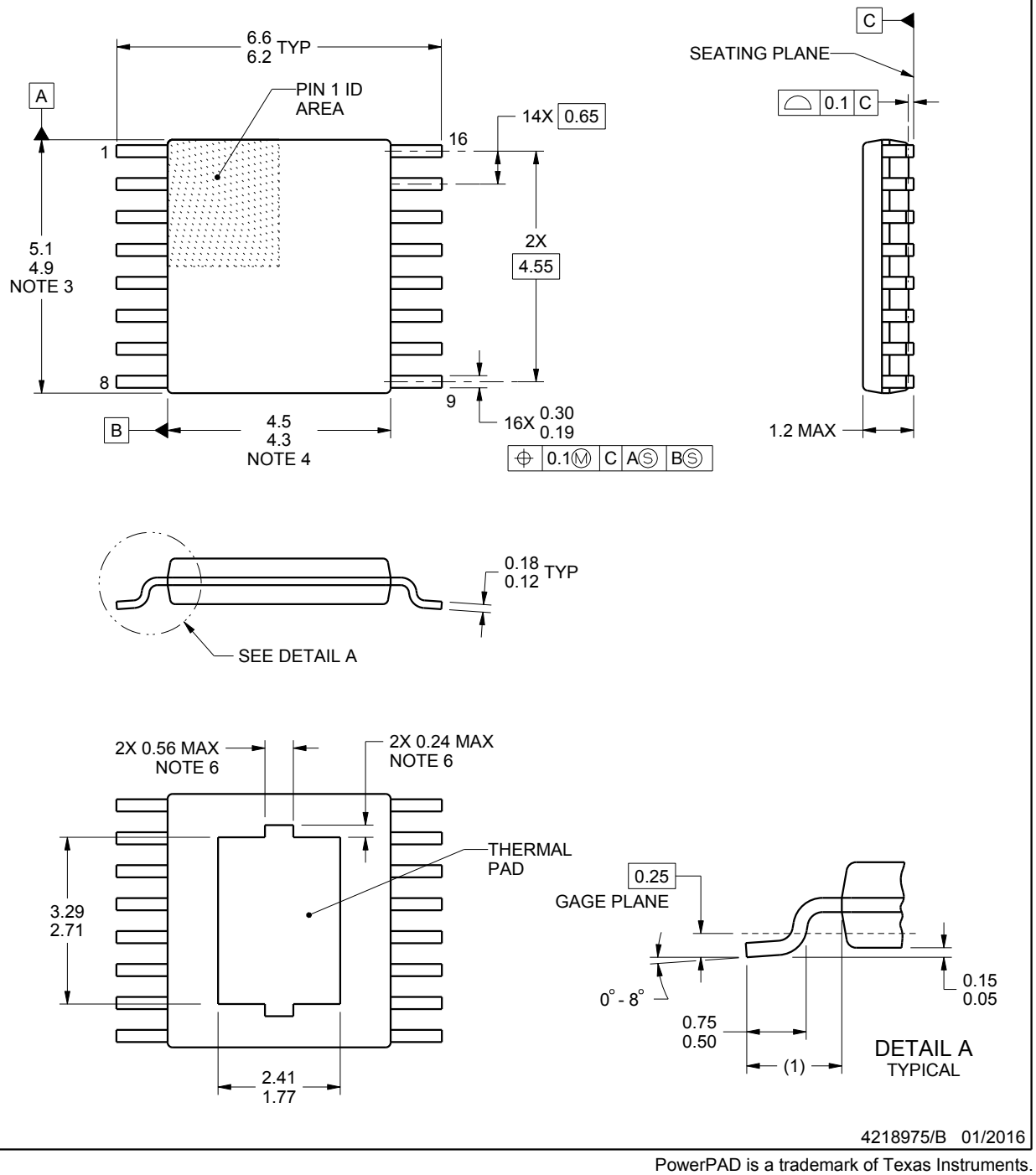
4224715/A

# PACKAGE OUTLINE

## PWP0016G

## PowerPAD™ TSSOP - 1.2 mm max height

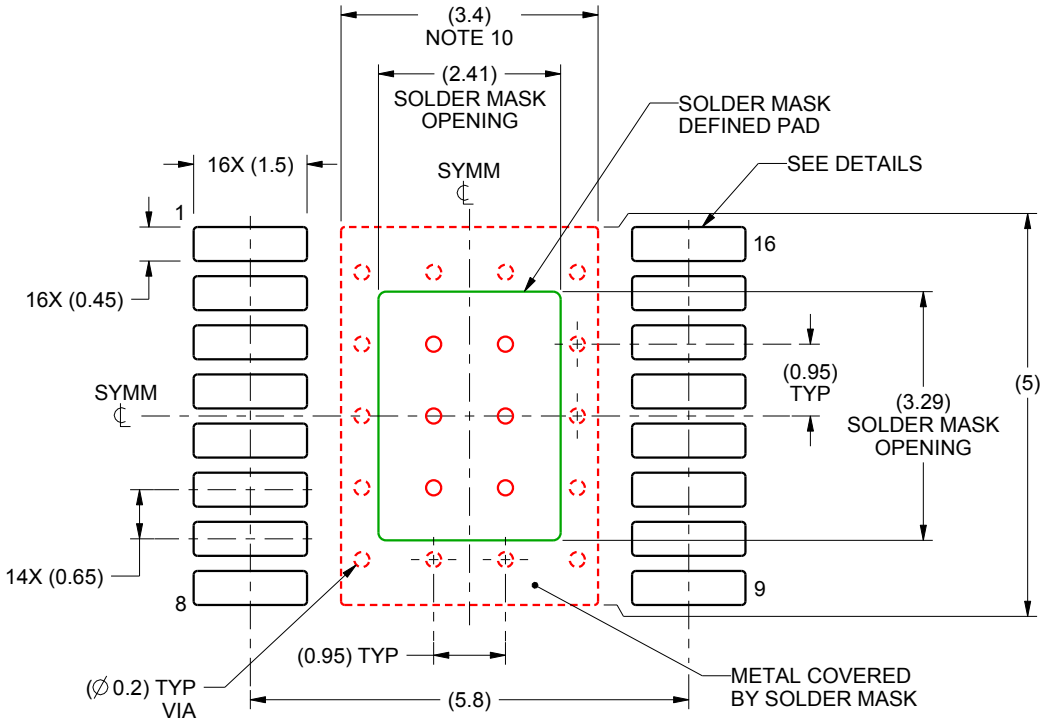
PLASTIC SMALL OUTLINE



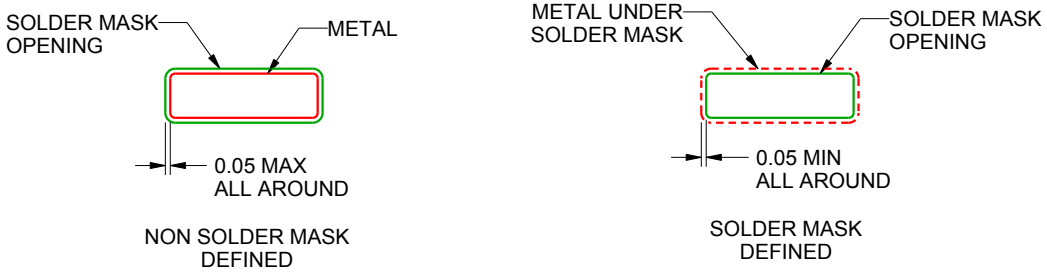

PowerPAD is a trademark of Texas Instruments.

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-153.
6. Features may not present.




LAND PATTERN EXAMPLE
SCALE:10X

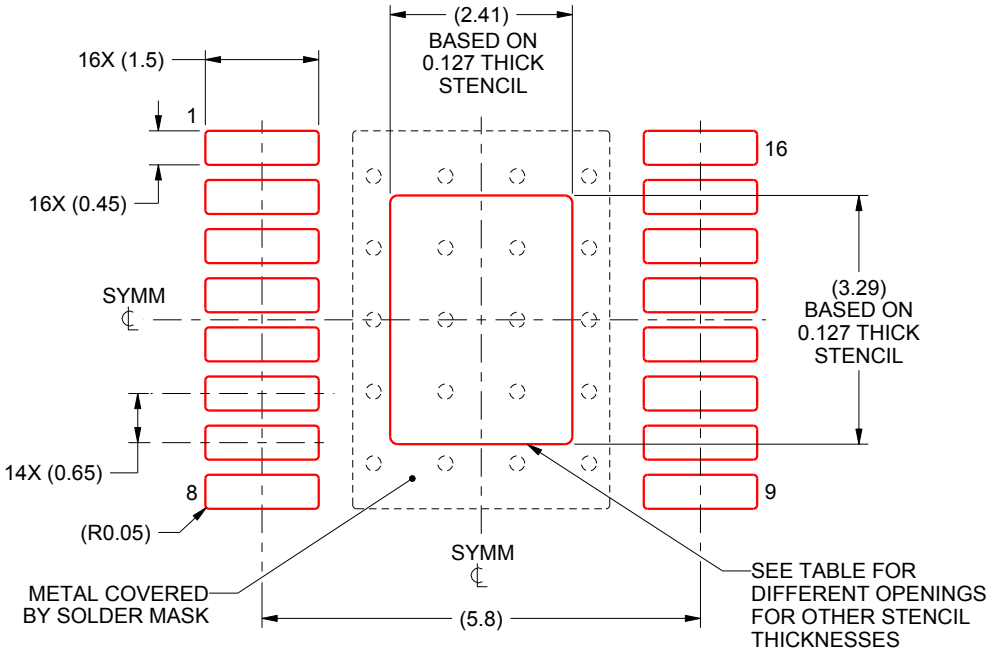



SOLDER MASK DETAILS
PADS 1-16

4218975/B 01/2016

NOTES: (continued)

7. Publication IPC-7351 may have alternate designs.
8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
9. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
10. Size of metal pad may vary due to creepage requirement.




SOLDER PASTE EXAMPLE
EXPOSED PAD
100% PRINTED SOLDER COVERAGE BY AREA
SCALE:10X

| STENCIL THICKNESS | SOLDER STENCIL OPENING |
|---|---|
| 0.1 | 2.69 X 3.68 |
| 0.127 | 2.41 X 3.29 (SHOWN) |
| 0.152 | 2.20 X 3.00 |
| 0.178 | 2.04 X 2.78 |

4218975/B 01/2016

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

# 重要声明和免责声明

TI“按原样”提供技术和可靠性数据（包括数据表）、设计资源（包括参考设计）、应用或其他设计建议、网络工具、安全信息和其他资源，不保证没有瑕疵且不做出任何明示或暗示的担保，包括但不限于对适销性、某特定用途方面的适用性或不侵犯任何第三方知识产权的暗示担保。

这些资源可供使用 TI 产品进行设计的熟练开发人员使用。您将自行承担以下全部责任：(1) 针对您的应用选择合适的 TI 产品，(2) 设计、验证并测试您的应用，(3) 确保您的应用满足相应标准以及任何其他功能安全、信息安全、监管或其他要求。

这些资源如有变更，恕不另行通知。TI 授权您仅可将这些资源用于研发本资源所述的 TI 产品的应用。严禁对这些资源进行其他复制或展示。您无权使用任何其他 TI 知识产权或任何第三方知识产权。您应全额赔偿因在这些资源的使用中对 TI 及其代表造成的任何索赔、损害、成本、损失和债务，TI 对此概不负责。

TI 提供的产品受 TI 的销售条款或 ti.com 上其他适用条款/TI 产品随附的其他适用条款的约束。TI 提供这些资源并不会扩展或以其他方式更改 TI 针对 TI 产品发布的适用的担保或担保免责声明。

TI 反对并拒绝您可能提出的任何其他或不同的条款。

邮寄地址：Texas Instruments, Post Office Box 655303, Dallas, Texas 75265