

TEXAS INSTRUMENTS

[LMK00301](https://www.ti.com.cn/product/cn/lmk00301?qgpn=lmk00301)

[ZHCSH72J](https://www.ti.com.cn/cn/lit/pdf/ZHCSH72) – SEPTEMBER 2011 – REVISED MAY 2023

LMK00301 3GHz 10 路输出超低附加抖动 差动时钟缓冲器和电平转换器

1 特性

- 3:1 输入多路复用器
	- 两个通用输入运行频率高达 3.1GHz,且接受 lvpecl、lvds、cml、sstl、hstl、hcsl 或单端时钟
	- 一个晶体输入可接受 10MHz 至 40MHz 的晶体 或单端时钟
- 分为两组,每组具有五路差分输出
	- LVPECL, LVDS, HCSL 或高阻态(每个组可 选)
	- LMK03806 时钟源为 156.25MHz 时的 LVPECL 附加抖动:
		- 20fs RMS (10 kHz $\mathfrak{\&}$ 1MHz)
		- 51fs RMS (12 kHz $\overline{\mathfrak{D}}$ 20MHz)
- 频率范围:
	- $-$ LVPECL (DC $\mathfrak{\subseteq}$ 3100MHz)
	- $-$ LVDS (DC $\widetilde{\Xi}$ 2100MHz)
	- $-$ HCSL (DC $\widetilde{\Xi}$ 800MHz)
	- $-$ LVCMOS (DC $\widetilde{\Xi}$ 250MHz)
- 高 PSRR: 65dBc (LVPECL) 和 76 dBc (LVDS),156.25MHz
- 通过同步使能输入提供 LVCMOS 输出
- 由引脚控制的配置
- V_{CC} 内核电源:3.3V ± 5%
- 三个独立的 V_{CCO} 输出电源: 3.3V 或 2.5V ± 5%
- 工业温度范围:–40°C 至 +85°C

2 应用

- 面向 ADC、DAC、多千兆以太网、XAUI、光纤通 道、SATA/SAS、SONET/SDH、CPRI 和高频背板 的时钟分配和电平转换
- 交换机、路由器、线路接口卡、定时卡
- 服务器、计算、PCI express(PCIe 3.0、4.0、 5.0、6.0)
- 远程无线电单元和基带单元

3 说明

LMK00301 是一款 3GHz、10 路输出差动扇出缓冲 器,用于高频、低抖动时钟和数据分配以及电平转换。 可从两个通用输入或一个晶振输入中选择输入时钟。所 选择的输入时钟被分配到两组输出,每组输出包含 5 个差动输出和 1 个 LVCMOS 输出。两个差分输出组可 被独立配置为 LVPECL, LVDS 或 HCSL 驱动器, 或 者被禁用。LVCMOS 输出具有用于在启用或禁用时实 现无短脉冲运行的同步使能输入。LMK00301 由一个 3.3V 内核电源和三个独立的 3.3V 或 2.5V 输出电源供 电运行。

LMK00301 具有高性能、高功效而且用途广泛,因此 堪称替代固定输出缓冲器器件的理想选择,同时还能增 加系统中的时序余裕。LMK00301 提供一种设计版 本,即 LMK00301A,该版本在内核和输出电源域之间 没有电源时序要求。

封装信息(1)

- (1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附 录。
- (2) LMK00301A 是一款可订购的设计版本,可在数据表末尾的可 订购产品附录中找到。

功能方框图

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4 Revision History

注:以前版本的页码可能与当前版本的页码不同

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Changes from Revision G (May 2013) to Revision H (March 2016) Page

5 Device Comparison

(1) Requires power supply sequencing where all of the core and output supplies ramp at the same time or must be tied together.
(2) Does not have power supply sequencing requirements between the core and output supply domai

Does not have power supply sequencing requirements between the core and output supply domains.

6 Pin Configuration and Functions

图 **6-1. RHS Package 48-Pin WQFN Top View**

表 **6-1. Pin Functions**[\(3\)](#page-5-0)

表 **6-1. Pin Functions**(3) **(continued)**

(1) The output supply voltages or pins (V $_{\rm CCOA}$, V $_{\rm CCOB}$, and V $_{\rm CCOC}$) will be called V $_{\rm CCO}$ in general when no distinction is needed, or when the output supply can be inferred from the output bank/type.

(2) CMOS control input with internal pull-down resistor.

(3) Any unused output pin should be left floating with minimum copper length (see note in *[Clock Outputs](#page-23-0)*), or properly terminated if connected to a transmission line, disabled, or set to Hi-Z, if possible. See *[Clock Outputs](#page-23-0)* for output configuration and *[Termination and](#page-27-0) [Use of Clock Drivers](#page-27-0)* for output interface and termination techniques.

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾ (2)

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/Distributors for availability and specifications.

7.2 ESD Ratings

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process. Manufacturing with less than 500-V HBM is possible with the necessary precautions. Pins listed as ±2000 V may actually have higher performance.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process. Manufacturing with less than 250-V CDM is possible with the necessary precautions. Pins listed as ±750 V may actually have higher performance.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

(1) The output supply voltages or pins (V_{CCOA}, V_{CCOB}, and V_{CCOC}) will be called V_{CCO} in general when no distinction is needed, or when the output supply can be inferred from the output bank/type

(2) Vcco for any output bank should be less than or equal to Vcc (Vcco \leq Vcc).

7.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953.](https://www.ti.com/lit/pdf/spra953)

(2) Specification assumes 16 thermal vias connect the die attach pad to the embedded copper plane on the 4-layer JEDEC board. These vias play a key role in improving the thermal performance of the package. It is recommended that the maximum number of vias be used in the board layout.

7.5 Electrical Characteristics

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C $\leq T_A \leq 85$ °C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A $= 25^{\circ}$ C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.^{[\(1\)](#page-13-0)}

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C \leq T_A \leq 85°C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A $= 25^{\circ}$ C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.^{[\(1\)](#page-13-0)}

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C \leq T_A \leq 85°C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A = 25°C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.[\(1\)](#page-13-0)

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C \leqslant T_A \leqslant 85°C, CLKin driven differentially, input slew rate \geqslant 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A = 25°C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.^{[\(1\)](#page-13-0)}

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C \leqslant T_A \leqslant 85°C, CLKin driven differentially, input slew rate \geqslant 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A = 25°C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.[\(1\)](#page-13-0)

Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C \leq T_A \leq 85°C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A $= 25^{\circ}$ C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.^{[\(1\)](#page-13-0)}

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Unless otherwise specified: Vcc = 3.3 V ± 5%, Vcco = 3.3 V ± 5%, 2.5 V ± 5%, -40°C $\leq T_A \leq 85$ °C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Typical values represent most likely parametric norms at Vcc = 3.3 V, Vcco = 3.3 V, T_A = 25°C, and at the Recommended Operation Conditions at the time of product characterization and are not ensured.(1)

(1) The Electrical Characteristics tables list ensured specifications under the listed Recommended Operating Conditions except as otherwise modified or specified by the Electrical Characteristics Conditions and/or Notes. Typical specifications are estimations only and are not ensured.

(2) See *[Power Supply Recommendations](#page-32-0)* for more information on current consumption and power dissipation calculations. Characteristics for both LMK00301 and LMK00301A are the same unless specified under the test conditions.

- (3) Power supply ripple rejection, or PSRR, is defined as the single-sideband phase spur level (in dBc) modulated onto the clock output when a single-tone sinusoidal signal (ripple) is injected onto the Vcco supply. Assuming no amplitude modulation effects and small index modulation, the peak-to-peak deterministic jitter (DJ) can be calculated using the measured single-sideband phase spur level (PSRR) as follows: DJ (ps pk-pk) = $[(2 * 10^{(\text{PSRR}/20)}) / (\pi * f_{\text{CLK}})] * 1E12$
- (4) See *[Differential Voltage Measurement Terminology](#page-20-0)* for definition of V_{ID} and V_{OD} voltages.
- (5) The ESR requirements stated must be met to ensure that the oscillator circuitry has no startup issues. However, lower ESR values for the crystal may be necessary to stay below the maximum power dissipation (drive level) specification of the crystal. Refer to *[Crystal](#page-26-0) [Interface](#page-26-0)* for crystal drive level considerations.
- (6) For the 100 MHz and 156.25 MHz clock input conditions, Additive RMS Jitter (J_{ADD}) is calculated using Method #1: J_{ADD} = SQRT(J_{OUT}) 2 - J $_{\rm SOURCE}$ 2), where J $_{\rm OUT}$ is the total RMS jitter measured at the output driver and J $_{\rm SOURCE}$ is the RMS jitter of the clock source applied to CLKin. For the 625 MHz clock input condition, Additive RMS Jitter is approximated using Method #2: J_{ADD} = SQRT(2*10^{dBc/10}) / (2* π *f_{CLK}), where dBc is the phase noise power of the Output Noise Floor integrated from 1 to 20 MHz bandwidth. The phase noise power can be calculated as: d Bc = Noise Floor + $10[*] \log_{10}(20 \text{ MHz} - 1 \text{ MHz})$. The additive RMS jitter was approximated for 625 MHz using Method #2 because the RMS jitter of the clock source was not sufficiently low enough to allow practical use of Method #1. Refer to the "Noise Floor vs. CLKin Slew Rate" and "RMS Jitter vs. CLKin Slew Rate" plots in *[Typical](#page-14-0) [Characteristics](#page-14-0)*.
- (7) 156.25 MHz LVPECL clock source from LMK03806 with 20 MHz crystal reference (crystal part number: ECS-200-20-30BU-DU). Typical J_{SOURCE} = 190 fs RMS (10 kHz to 1 MHz) and 195 fs RMS (12 kHz to 20 MHz). Refer to the LMK03806 data sheet for more information.
- (8) The noise floor of the output buffer is measured as the far-out phase noise of the buffer. Typically this offset is \geqslant 10 MHz, but for lower frequencies this measurement offset can be as low as 5 MHz due to measurement equipment limitations.
- (9) Phase noise floor will degrade as the clock input slew rate is reduced. Compared to a single-ended clock, a differential clock input (LVPECL, LVDS) will be less susceptible to degradation in noise floor at lower slew rates due to its common mode noise rejection. However, it is recommended to use the highest possible input slew rate for differential clocks to achieve optimal noise floor performance at the device outputs.
- (10) Specification is ensured by characterization and is not tested in production.
- (11) See *[Typical Characteristics](#page-14-0)* for output operation over frequency.
- (12) AC timing parameters for HCSL or CMOS are dependent on output capacitive loading.
- (13) Output Enable Time is the number of input clock cycles it takes for the output to be enabled after REFout_EN is pulled high. Similarly, Output Disable Time is the number of input clock cycles it takes for the output to be disabled after REFout_EN is pulled low. The REFout_EN signal should have an edge transition much faster than that of the input clock period for accurate measurement.
- (14) Output skew is the propagation delay difference between any two outputs with identical output buffer type and equal loading while operating at the same supply voltage and temperature conditions.
- (15) Parameter is specified by design, not tested in production.
- (16) 100 MHz and 156.25 MHz input source from Rohde & Schwarz SMA100A Low-Noise Signal Generator and Sine-to-Square-wave Conversion block

(17) For clock input frequency ≥ 100 MHz, CLKinX can be driven with single-ended (LVCMOS) input swing up to 3.3 Vpp. For clock input frequency < 100 MHz, the single-ended input swing should be limited to 2 Vpp max to prevent input saturation (refer to *[Driving the](#page-24-0) [Clock Inputs](#page-24-0)* for interfacing 2.5 V/3.3 V LVCMOS clock input < 100 MHz to CLKinX).

7.6 Typical Characteristics

Unless otherwise specified: V_{CC} = 3.3 V, V_{CCO} = 3.3 V, T_A = 25°C, CLKin driven differentially, input slew rate ≥ 3 V/ns. Consult 表 [7-1](#page-19-0) at the end of *Typical Characteristics* for graph notes.

See Note 1 in Graph Notes table

图 **7-21. HCSL Phase Noise at 100 MHz**

See Note 1 in Graph Notes table

See Note 1 in Graph Notes table

图 **7-23. LVPECL Phase Noise at 100 MHz**

表 **7-1. Graph Notes**

8 Parameter Measurement Information

8.1 Differential Voltage Measurement Terminology

The differential voltage of a differential signal can be described by two different definitions causing confusion when reading data sheets or communicating with other engineers. This section will address the measurement and description of a differential signal so that the reader will be able to understand and discern between the two different definitions when used.

The first definition used to describe a differential signal is the absolute value of the voltage potential between the inverting and non-inverting signal. The symbol for this first measurement is typically V_{ID} or V_{OD} depending on if an input or output voltage is being described.

The second definition used to describe a differential signal is to measure the potential of the non-inverting signal with respect to the inverting signal. The symbol for this second measurement is V_{SS} and is a calculated parameter. Nowhere in the IC does this signal exist with respect to ground, it only exists in reference to its differential pair. V_{SS} can be measured directly by oscilloscopes with floating references, otherwise this value can be calculated as twice the value of V_{OD} as described in the first description.

图 8-1 illustrates the two different definitions side-by-side for inputs and 图 8-2 illustrates the two different definitions side-by-side for outputs. The V_{ID} (or V_{OD}) definition show the DC levels, V_{IH} and V_{OL} (or V_{OH} and V_{OL}), that the non-inverting and inverting signals toggle between with respect to ground. V_{SS} input and output definitions show that if the inverting signal is considered the voltage potential reference, the non-inverting signal voltage potential is now increasing and decreasing above and below the non-inverting reference. Thus the peakto-peak voltage of the differential signal can be measured.

 V_{ID} and V_{OD} are often defined as volts (V) and V_{SS} is often defined as volts peak-to-peak (V_{PP}).

图 **8-1. Two Different Definitions for Differential Input Signals**

See also [AN-912 Common Data Transmission Parameters and their Definitions](https://www.ti.com/lit/pdf/SNLA036).

9 Detailed Description

9.1 Overview

The LMK00301 is a 10-output differential clock fanout buffer with low additive jitter that can operate up to 3.1 GHz. It features a 3:1 input multiplexer with an optional crystal oscillator input, two banks of 5 differential outputs with multi-mode buffers (LVPECL, LVDS, HCSL, or Hi-Z), one LVCMOS output, and three independent output buffer supplies. The input selection and output buffer modes are controlled through pin strapping. The device is offered in a 48-pin WQFN package and leverages much of the high-speed, low-noise circuit design employed in the LMK04800 family of clock conditioners.

9.2 Functional Block Diagram

图 **9-1. Functional Block Diagram**

9.3 Feature Description

9.3.1 V_{CC} and V_{CCO} Power Supplies

The LMK00301 has separate 3.3-V core (V_{CC}) and three independent 3.3-V or 2.5-V output power supplies (V_{CCOA}, V_{CCOB}, V_{CCOC}) supplies. Output supply operation at 2.5 V enables lower power consumption and output-level compatibility with 2.5-V receiver devices. The output levels for LVPECL (V_{OH}, V_{OL}) and LVCMOS (V_{OH}) are referenced to its respective V_{CCO} supply, while the output levels for LVDS and HCSL are relatively constant over the specified V_{CCO} range. See *[Power Supply Recommendations](#page-32-0)* for additional supply related considerations, such as power dissipation, power supply bypassing, and power-supply ripple rejection (PSRR).

备注

Take care to ensure the V_{CCO} voltages do not exceed the V_{CC} voltage to prevent turning-on the internal ESD protection circuitry.

9.4 Device Functional Modes

9.4.1 Clock Inputs

The input clock can be selected from CLKin0/CLKin0*, CLKin1/CLKin1*, or OSCin. Clock input selection is controlled using the CLKin_SEL[1:0] inputs as shown in 表 9-1. See *[Driving the Clock Inputs](#page-24-0)* for clock input requirements. When CLKin0 or CLKin1 is selected, the crystal circuit is powered down. When OSCin is selected, the crystal oscillator circuit starts up and the clock are distributed to all outputs. See *[Crystal Interface](#page-26-0)* for more information. Alternatively, OSCin may be driven by a single-ended clock (up to 250 MHz) instead of a crystal.

表 **9-1. Input Selection CLKin_SEL1 CLKin_SEL0 SELECTED INPUT** 0 CLKin0, CLKin0* 0 1 1 CLKin1, CLKin1* 1 X OSCin

表 9-2 shows the output logic state versus input state when either CLKin0/CLKin0^{*} or CLKin1/CLKin1^{*} is selected. When OSCin is selected, the output state will be an inverted copy of the OSCin input state.

表 **9-2. CLKin Input vs Output States**

9.4.2 Clock Outputs

The differential output buffer type for Bank A and Bank B outputs can be separately configured using the CLKoutA TYPE[1:0] and CLKoutB TYPE[1:0] inputs, respectively, as shown in 表 9-3. For applications where all differential outputs are not required, any unused output pin should be left floating with a minimum copper length (see note below) to minimize capacitance and potential coupling and reduce power consumption. If an entire output bank will not be used, TI recommends to disable (Hi-Z) the bank to reduce power. See *[Termination](#page-27-0) [and Use of Clock Drivers](#page-27-0)* for more information on output interface and termination techniques.

备注

For best soldering practices, the minimum trace length for any unused output pin should extend to include the pin solder mask. This way during reflow, the solder has the same copper area as connected pins. This allows for good, uniform fillet solder joints helping to keep the IC level during reflow.

表 **9-3. Differential Output Buffer Type Selection**

9.4.2.1 Reference Output

The reference output (REFout) provides a LVCMOS copy of the selected input clock. The LVCMOS output high level is referenced to the V_{CCO} voltage. REFout can be enabled or disabled using the enable input pin, REFout EN, as shown in $\frac{1}{\mathcal{R}}$ 9-4.

The REFout EN input is internally synchronized with the selected input clock by the SYNC block. This synchronizing function prevents glitches and runt pulses from occurring on the REFout clock when enabled or disabled. REFout is enabled within three cycles (t_{FN}) of the input clock after REFout EN is toggled high. REFout will be disabled within three cycles (t_{DIS}) of the input clock after REFout_EN is toggled low.

When REFout is disabled, the use of a resistive loading can be used to set the output to a predetermined level. For example, if REFout is configured with a 1-kΩ load to ground, then the output will be pulled to low when disabled.

10 Application and Implementation

备注

以下应用部分中的信息不属于 TI 器件规格的范围,TI 不担保其准确性和完整性。TI 的客 户应负责确定 器件是否适用于其应用。客户应验证并测试其设计,以确保系统功能。

10.1 Application Information

A common PCIe application, such as a server card, consists of several building blocks, which all need a reference clock. In the mostly used Common RefClk architecture, the clock is distributed from a single source to both RX and TX. This requires either a clock generator with high output count or a buffer like the LMK00301. The buffer simplifies the clocking tree and provides a cost and space optimized solution. While using a buffer to distribute the clock, consider the additive jitter. The LMK00301 is an ultra-low additive jitter PCIe clock buffer suitable for all current and future PCIe generations.

10.2 Typical Application

10.2.1 Design Requirements

10.2.1.1 Driving the Clock Inputs

The LMK00301 has two universal inputs (CLKin0/CLKin0* and CLKin1/CLKin1*) that can accept AC-coupled or DC-coupled, 3.3-V or 2.5-V LVPECL, LVDS, CML, SSTL, and other differential and single-ended signals that meet the input requirements specified in *[Electrical Characteristics](#page-7-0)* . The device can accept a wide range of signals due to its wide input common-mode voltage range (V_{CM}) and input voltage swing (V_{ID}) / dynamic range. For 50% duty cycle and DC-balanced signals, AC coupling may also be employed to shift the input signal to within the V_{CM} range. Refer to *[Termination and Use of Clock Drivers](#page-27-0)* for signal interfacing and termination techniques.

To achieve the best possible phase noise and jitter performance, it is mandatory for the input to have high slew rate of 3 V/ns (differential) or higher. Driving the input with a lower slew rate will degrade the noise floor and jitter. For this reason, TI recommends a differential signal input over a single-ended signal because this signal typically

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provides higher slew rate and common-mode-rejection. See the *Noise Floor vs CLKin Slew Rate* and *RMS Jitter vs CLKin Slew Rate* plots in *[Typical Characteristics](#page-14-0)* section.

While TI recommends to drive the CLKin/CLKin^{*} pair with a differential signal input, it is possible to drive the pair with a single-ended clock, provided the clock conforms to the Single-Ended Input specifications for CLKin pins listed in the *[Electrical Characteristics](#page-7-0)*. For large single-ended input signals, such as 3.3-V or 2.5-V LVCMOS, place a 50-Ω load resistor near the input for signal attenuation to prevent input overdrive as well as for line termination to minimize reflections. Again, the single-ended input slew rate should be as high as possible to minimize performance degradation. The CLKin input has an internal bias voltage of about 1.4 V, so the input can be AC coupled as shown in 图 10-2. The output impedance of the LVCMOS driver plus Rs should be close to 50 Ω to match the characteristic impedance of the transmission line and load termination.

图 **10-2. Single-Ended LVCMOS Input, AC Coupling**

A single-ended clock may also be DC coupled to CLKinX as shown in \boxtimes 10-3. Place a 50- Ω load resistor near the CLKinX input for signal attenuation and line termination. Half of the single-ended swing of the driver (V_{OPP}) 2) drives CLKinX, therefore CLKinX* should be externally biased to the midpoint voltage of the attenuated input swing ($(V_{O,PP} / 2) \times 0.5$). The external bias voltage should be within the specified input common-mode voltage (V_{CM}) range. This can be achieved using external biasing resistors in the kΩ range (R_{B1} and R_{B2}) or another low-noise voltage reference. This will ensure the input swing crosses the threshold voltage at a point where the input slew rate is the highest.

If the LVCMOS driver cannot achieve sufficient swing with a DC-terminated, 50-Ω load at the CLKinX input as shown in \boxtimes 10-3, then consider connecting the 50- Ω load termination to ground through a capacitor (C_{AC}). This AC termination blocks the DC load current on the driver, so the voltage swing at the input is determined by the voltage divider formed by the source (Ro+Rs) and 50- Ω load resistors. The value for C_{AC} depends on the trace delay, Td, of the 50-Ω transmission line;

$$
CAC \geq 3 \times Td / 50 \Omega
$$
\n\n

CMOS	W	500 Trace	V _{OPP} /2
Divier	W	500 Trace	VCC
Divier	U	1	
U	U	1	
U	U	1	
U	U	1	
U	U	1	
U	U	1	
U	U	1	
U	U	1	
U	U	1	

\n\n\n\n

If the crystal oscillator circuit is not used, it is possible to drive the OSCin input with an single-ended external clock as shown in \mathbb{R} [10-4.](#page-26-0) The input clock should be AC coupled to the OSCin pin, which has an internallygenerated input bias voltage, and the OSCout pin should be left floating. While OSCin provides an alternative input to multiplex an external clock, TI recommends to use either universal input (CLKinX) because the inputs offer higher operating frequency, better common-mode and power supply noise rejection, and greater performance over supply voltage and temperature variations.

图 **10-4. Driving OSCin with a Single-Ended Input**

10.2.1.2 Crystal Interface

The LMK00301 has an integrated crystal oscillator circuit that supports a fundamental mode, AT-cut crystal. \boxtimes 10-5 shows the crystal interface.

图 **10-5. Crystal Interface**

The load capacitance (C_L) is specific to the crystal, but usually on the order of 18 pF to 20 pF. While C_L is specified for the crystal, the OSCin input capacitance $(C_{1N} = 4$ pF typical) of the device and PCB stray capacitance (C_{STRAY} approximately 1 pF to 3 pF) can affect the discrete load capacitor values, C₁ and C₂.

For the parallel resonant circuit, the discrete capacitor values can be calculated as follows:

$$
C_{L} = (C_{1} \times C_{2}) / (C_{1} + C_{2}) + C_{IN} + C_{STRAY}
$$
 (2)

Typically, C₁ = C₂ for optimum symmetry, so 方程式 2 can be rewritten in terms of C₁ only:

$$
C_{L} = C_{1}^{2} / (2 \times C_{1}) + C_{IN} + C_{STRAY}
$$
 (3)

Finally, solve for C_1 :

 $C_1 = (C_L - C_{IN} - C_{STRAY}) \times 2$ (4)

[Electrical Characteristics](#page-7-0) provides crystal interface specifications with conditions that ensure start-up of the crystal, but it does not specify crystal power dissipation. The designer will need to ensure the crystal power dissipation does not exceed the maximum drive level specified by the crystal manufacturer. Overdriving the crystal can cause premature aging, frequency shift, and eventual failure. Drive level should be held at a sufficient level necessary to start-up and maintain steady-state operation.

The power dissipated in the crystal, P_{XTAL} , can be computed by:

$$
P_{\text{XTAL}} = I_{\text{RMS}}^2 \times R_{\text{ESR}} \times (1 + C_0/C_L)^2
$$

where

- \cdot I_{RMS} is the RMS current through the crystal.
- R_{ESR} is the maximum equivalent series resistance specified for the crystal
- \cdot C_L is the load capacitance specified for the crystal
- C_0 is the minimum shunt capacitance specified for the crystal

I_{RMS} can be measured using a current probe (for example, Tektronix CT-6 or equivalent) placed on the leg of the crystal connected to OSCout with the oscillation circuit active.

As shown in \boxtimes [10-5,](#page-26-0) an external resistor, R_{LIM}, can be used to limit the crystal drive level, if necessary. If the power dissipated in the selected crystal is higher than the drive level specified for the crystal with R_{LIM} shorted, then a larger resistor value is mandatory to avoid overdriving the crystal. However, if the power dissipated in the crystal is less than the drive level with R_{LIM} shorted, then a zero value for R_{LIM} can be used. As a starting point, a suggested value for R_{LIM} is 1.5 kΩ.

10.2.2 Detailed Design Procedure

10.2.2.1 Termination and Use of Clock Drivers

When terminating clock drivers keep in mind these guidelines for optimum phase noise and jitter performance:

- Transmission line theory should be followed for good impedance matching to prevent reflections.
- Clock drivers should be presented with the proper loads.
	- LVDS outputs are current drivers and require a closed current loop.
	- HCSL drivers are switched current outputs and require a DC path to ground through 50-Ω termination.
	- LVPECL outputs are open emitter and require a DC path to ground.
- Receivers should be presented with a signal biased to their specified DC bias level (common-mode voltage) for proper operation. Some receivers have self-biasing inputs that automatically bias to the proper voltage level; in this case, the signal should normally be AC coupled.

It is possible to drive a non-LVPECL or non-LVDS receiver with a LVDS or LVPECL driver as long as the above guidelines are followed. Check the data sheet of the receiver or input being driven to determine the best termination and coupling method to be sure the receiver is biased at the optimum DC voltage (common-mode voltage).

10.2.2.1.1 Termination for DC Coupled Differential Operation

For DC coupled operation of an LVDS driver, terminate with 100 Ω as close as possible to the LVDS receiver as shown in $\overline{\otimes}$ 10-6.

图 **10-6. Differential LVDS Operation, DC Coupling, No Biasing by the Receiver**

(5)

For DC coupled operation of an HCSL driver, terminate with 50 Ω to ground near the driver output as shown in 图 10-7. Series resistors, Rs, may be used to limit overshoot due to the fast transient current. Because HCSL drivers require a DC path to ground, AC coupling is not allowed between the output drivers and the 50 Ω termination resistors.

图 **10-7. HCSL Operation, DC Coupling**

For DC coupled operation of an LVPECL driver, terminate with 50 Ω to Vcco - 2 V as shown in \boxtimes 10-8. Alternatively terminate with a Thevenin equivalent circuit as shown in \boxtimes 10-9 for Vcco (output driver supply voltage) = 3.3 V and 2.5 V. In the Thevenin equivalent circuit, the resistor dividers set the output termination voltage (V_{TT}) to Vcco - 2 V.

图 **10-8. Differential LVPECL Operation, DC Coupling**

图 **10-9. Differential LVPECL Operation, DC Coupling, Thevenin Equivalent**

10.2.2.1.2 Termination for AC Coupled Differential Operation

AC coupling allows for shifting the DC bias level (common-mode voltage) when driving different receiver standards. Since AC coupling prevents the driver from providing a DC bias voltage at the receiver, it is important to ensure the receiver is biased to its ideal DC level.

When driving differential receivers with an LVDS driver, the signal may be AC coupled by adding DC blocking capacitors; however the proper DC bias point needs to be established at both the driver side and the receiver side. The recommended termination scheme depends on whether the differential receiver has integrated termination resistors or not.

When driving a differential receiver without internal 100 Ω differential termination, the AC coupling capacitors should be placed between the load termination resistor and the receiver to allow a DC path for proper biasing of the LVDS driver. This is shown in \boxtimes 10-10. The load termination resistor and AC coupling capacitors should be placed as close as possible to the receiver inputs to minimize stub length. The receiver can be biased internally or externally to a reference voltage within the receiver' s common mode input range through resistors in the kilo-ohm range.

When driving a differential receiver with internal 100 Ω differential termination, a source termination resistor should be placed before the AC coupling capacitors for proper DC biasing of the driver as shown in \boxtimes 10-11. However, with a 100 Ω resistor at the source and the load (that is, double terminated), the equivalent resistance seen by the LVDS driver is 50 Ω which causes the effective signal swing at the input to be reduced by half. If a self-terminated receiver requires input swing greater than 250 mVpp (differential) as well as AC coupling to its inputs, then the LVDS driver with the double-terminated arrangement in \boxtimes 10-11 may not meet the minimum input swing requirement; alternatively, the LVPECL or HCSL output driver format with AC coupling is recommended to meet the minimum input swing required by the self-terminated receiver.

When using AC coupling with LVDS outputs, there may be a start-up delay observed in the clock output due to capacitor charging. The examples in \boxtimes 10-10 and \boxtimes 10-11 use 0.1-μF capacitors, but this value may be adjusted to meet the start-up requirements for the particular application.

LVPECL drivers require a DC path to ground. When AC coupling an LVPECL signal use 160- Ω emitter resistors (or 91 Ω for Vcco = 2.5 V) close to the LVPECL driver to provide a DC path to ground as shown in $\boxed{8}$ [10-15.](#page-31-0) For proper receiver operation, the signal should be biased to the DC bias level (common mode voltage) specified by the receiver. The typical DC bias voltage (common mode voltage) for LVPECL receivers is 2 V. Alternatively, a Thevenin equivalent circuit forms a valid termination as shown in $\&$ [10-12](#page-30-0) for Vcco = 3.3 V and 2.5 V. Note: this Thevenin circuit is different from the DC coupled example in \boxtimes [10-9](#page-28-0), since the voltage divider is setting the input common-mode voltage of the receiver.

图 **10-12. Differential LVPECL Operation, AC Coupling, Thevenin Equivalent**

10.2.2.1.3 Termination for Single-Ended Operation

A balun can be used with either LVDS or LVPECL drivers to convert the balanced, differential signal into an unbalanced, single-ended signal.

It is possible to use an LVPECL driver as one or two separate 800 mV p-p signals. When DC coupling one of the LMK00301 LVPECL driver of a CLKoutX/CLKoutX^{*} pair, be sure to properly terminate the unused driver. When DC coupling on of the LMK00301 LVPECL drivers, the termination should be 50 Ω to Vcco - 2 V as shown in \boxtimes 10-13. The Thevenin equivalent circuit is also a valid termination as shown in 图 10-14 for Vcco = 3.3 V.

图 **10-13. Single-Ended LVPECL Operation, DC Coupling**

图 **10-14. Single-Ended LVPECL Operation, DC Coupling, Thevenin Equivalent**

When AC coupling an LVPECL driver use a 160 Ω emitter resistor (or 91 Ω for Vcco = 2.5 V) to provide a DC path to ground and ensure a 50 Ω termination with the proper DC bias level for the receiver. The typical DC bias voltage for LVPECL receivers is 2 V. If the companion driver is not used, it should be terminated with either a proper AC or DC termination. This latter example of AC coupling a single-ended LVPECL signal can be used to measure single-ended LVPECL performance using a spectrum analyzer or phase noise analyzer. When using most RF test equipment no DC bias point (0 VDC) is required for safe and proper operation. The internal 50 Ω termination the test equipment correctly terminates the LVPECL driver being measured as shown in \boxtimes [10-15.](#page-31-0) When using only one LVPECL driver of a CLKoutX/CLKoutX^{*} pair, be sure to properly terminated the unused driver.

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10.2.3 Application Curves

图 **10-16. HCSL Phase Noise at 100 MHz**

11 Power Supply Recommendations

11.1 Power Supply Sequencing

For the LMK00301, when powering the V_{CC} and V_{CCO} pins from separate supply rails, it is recommended for the supplies to reach their regulation point at approximately the same time while ramping up, or reach ground potential at the same time while ramping down. Using simultaneous or ratiometric power supply sequencing prevents internal current flow from V_{CC} to V_{CCO} pins that could occur when V_{CC} is powered before V_{CCO} .

For the LMK00301A, there is no power supply sequencing requirement between V_{CC} and V_{CCO} .

11.2 Current Consumption and Power Dissipation Calculations

The current consumption values specified in *[Electrical Characteristics](#page-7-0)* can be used to calculate the total power dissipation and IC power dissipation for any device configuration. Use 方程式 6 to calculate the total V_{CC} core supply current (I_{CC_TOTAL}) :

$$
I_{CC_TOTAL} = I_{CC_CORE} + I_{CC_BANK_A} + I_{CC_BANK_B} + I_{CC_CMOS}
$$
 (6)

where

- $I_{CC\ CORE}$ is the current for core logic and input blocks and depends on selected input (CLKinX or OSCin).
- $I_{CC-BANK-A}$ is the current for Bank A and depends on output type ($I_{CC-PECL}$, $I_{CC-LVDS}$, $I_{CC-HCSL}$, or 0 mA if disabled).
- $I_{CC-BANK-B}$ is the current for Bank B and depends on output type ($I_{CC-PECL}$, $I_{CC-LVDS}$, $I_{CC-HCSL}$, or 0 mA if disabled).
- \cdot I_{CC} _{CMOS} is the current for the LVCMOS output (or 0 mA if REFout is disabled).

Since the output supplies (V_{CCOA} , V_{CCOB} , V_{CCOC}) can be powered from 3 independent voltages, the respective output supply currents ($I_{CCO-BANK_A}$, $I_{CCO-BANK_B}$, $I_{CCO-CMOS}$) should be calculated separately.

I_{CCO} BANK for either Bank A or B can be directly taken from the corresponding output supply current specification (ICCO_PECL, ICCO_LVDS, or ICCO_HCSL) **provided the output loading matches the specified conditions**. Otherwise, $I_{\text{CCO-BANK}}$ should be calculated as follows:

$$
I_{CCO_BANK} = I_{BANK_BIAS} + (N \times I_{OUT_LOAD})
$$
 (7)

where

- $I_{\text{BANK BIAS}}$ is the output bank bias current (fixed value).
- $I_{OUT IOAD}$ is the DC load current per loaded output pair.
- N is the number of loaded output pairs in the bank ($N = 0$ to 5).

表 11-1 shows the typical I_{BANK_BIAS} values and I_{OUT_LOAD} expressions for the three differential output types.

For LVPECL, it is possible to use a larger termination resistor (R_T) to ground instead of terminating with 50 Ω to V_{TT} = V_{CCO} - 2 V; this technique is commonly used to eliminate the extra termination voltage supply (V_{TT}) and potentially reduce device power dissipation at the expense of lower output swing. For example, when V_{CCO} is 3.3 V, a R_T value of 160 Ω to ground will eliminate the 1.3 V termination supply without sacrificing much output swing. In this case, the typical $I_{\text{OUT}_\text{LOAD}}$ is 25 mA, so $I_{\text{CCO}_\text{PECL}}$ for a fully-loaded bank reduces to 158 mA (versus 165 mA with 50- Ω resistors to V_{CCO} - 2 V).

CURRENT PARAMETER	LVPECL	LVDS	HCSL
BANK BIAS	33 mA	34 mA	6 mA
IOUT LOAD	$(V_{OH} - V_{TT})/R_T + (V_{OL} - V_{TT})/R_T$	0 mA (No DC load current)	$\rm V_{OH}/R_{T}$

表 **11-1. Typical Output Bank Bias and Load Currents**

When the current consumption is calculated or known for each supply, the total power dissipation (P_{TOTAL}) can be calculated as:

$$
P_{\text{TOTAL}} = (V_{\text{CC}} \times I_{\text{CC_TOTAL}}) + (V_{\text{CCOA}} \times I_{\text{CCO_BANK_A}}) + (V_{\text{CCOB}} \times I_{\text{CCO_BANK_B}}) + (V_{\text{CCOC}} \times I_{\text{CCO_CMOS}})
$$
(8)

If the device configuration has LVPECL or HCSL outputs, then it is also necessary to calculate the power dissipated in any termination resistors (P_{RT} $_{PECL}$ and P_{RT} $_{HCSL}$) and in any termination voltages (P_{VTT}). The external power dissipation values can be calculated as follows:

$$
P_{RT_PECL} \text{ (per LVPECL pair)} = (V_{OH} - V_{TT})^2 / R_T + (V_{OL} - V_{TT})^2 / R_T \tag{9}
$$

 P_{VTT} pecl (per LVPECL pair) = V_{TT} * [(V_{OH} - V_{TT})/R_T + (V_{OL} - V_{TT})/R_T] (10)

$$
P_{RT_HCSL} \text{ (per HCSL pair)} = V_{OH}^2 / R_T \tag{11}
$$

Finally, the IC power dissipation (P_{DEVICE}) can be computed by subtracting the external power dissipation values from P_{TOTAL} as follows:

$$
P_{DEVICE} = P_{TOTAL} - N_1 \times (P_{RT_PECL} + P_{VTT_PECL}) - N_2 \times P_{RT_HCSL}
$$
\n
$$
(12)
$$

where

- N₁ is the number of LVPECL output pairs with termination resistors to V_{TT} (usually Vcco 2 V or GND).
- N_2 is the number of HCSL output pairs with termination resistors to GND.

11.2.1 Power Dissipation Example #1: Separate V_{CC} and V_{CCO} Supplies with Unused Outputs

This example shows how to calculate IC power dissipation for a configuration with separate V_{CC} and V_{CCO} supplies and unused outputs. Because some outputs are not used, the I_{CCO PECL} value specified in *[Electrical](#page-7-0) [Characteristics](#page-7-0)* cannot be used directly, and output bank current (I_{CCO_BANK}) should be calculated to accurately estimate the IC power dissipation.

- V_{CC} = 3.3 V, V_{CCOA} = 3.3 V, V_{CCOB} = 2.5 V. Typical I_{CC} and I_{CCO} values.
- CLKin0/CLKin0* input is selected.
- Bank A is configured for LVPECL: 4 pairs used with $R_T = 50 \Omega$ to V_T = V_{CCO} 2 V (1 pair unused).
- Bank B is configured for LVDS: 3 pairs used with $R_L = 100 \Omega$ differential (2 pairs unused).
- REFout is disabled.
- T_A = 85°C

Using the current and power calculations from the previous section, we can compute P_{TOTAL} and P_{DEVICE} .

- From [方程式](#page-32-0) 6: I_{CC_TOTAL} = 8.5 mA + 20 mA + 26 mA + 0 mA = 54.5 mA
- From 表 [11-1](#page-32-0): I_{OUT_LOAD} (LVPECL) = (1.6 V 0.5 V) 50 Ω + (0.75 V 0.5 V)/50 Ω = 27 mA
- From [方程式](#page-32-0) 7: I_{CCO_BANK_A} = 33 mA + (4 × 27 mA) = 141 mA
- From 方程式 8: P_{TOTAL} = (3.3 V × 54.5 mA) + (3.3 V × 141 mA) + (2.5 V × 34 mA)] = 730 mW
- From 方程式 9: P_{RT_PECL} = ((2.4 V 1.3 V)²/50 Ω) + ((1.55 V 1.3 V)²/50 Ω) = 25.5 mW (per output pair)
- From 方程式 10: P_{VTT} $_{\text{PFCL}}$ = 0.5 V × [((2.4 V 1.3 V) / 50 Ω) + ((1.55 V 1.3 V) / 50 Ω)] = 13.5 mW (per output pair)
- From 方程式 11: P_{RT_HCSL} = 0 mW (no HCSL outputs)
- From 方程式 12: P_{DEVICE} = 730 mW (4 × (25.5 mW + 13.5 mW)) 0 mW = 574 mW

In this example, the IC device will dissipate about 574 mW or 79% of the total power (730 mW), while the remaining 21% will be dissipated in the emitter resistors (102 mW for 4 pairs) and termination voltage (54 mW into V_{CCO} – 2 V).

Based on the thermal resistance junction-to-case (R $_{\theta$ JA) of 28.5°C/W, the estimated die junction temperature would be about 16.4°C above ambient, or 101.4°C when $T_A = 85$ °C.

11.2.2 Power Dissipation Example #2: Worst-Case Dissipation

This example shows how to calculate IC power dissipation for a configuration to estimate **worst-case power dissipation**. In this case, the maximum supply voltage and supply current values specified in *[Electrical](#page-7-0) [Characteristics](#page-7-0)* are used.

- Maximum V_{CC} = V_{CCO} = 3.465 V. Maximum I_{CC} and I_{CCO} values
- CLKin0/CLKin0* input is selected
- Banks A and B are configured for LVPECL: all outputs terminated with 50 Ω to V_T = V_{CCO} 2 V
- REFout is enabled with 5-pF load
- $T_A = 85^{\circ}C$

Using the *maximum* supply current and power calculations from the previous section, we can compute P_{TOTAL} and P_{DFVICE} .

- From [方程式](#page-32-0) 6: $I_{\text{CC TOTAL}}$ = 10.5 mA + 27 mA + 27 mA + 5.5 mA = 70 mA
- From $I_{CCO~PECL}$ max spec: $I_{CCO~BANK~A} = I_{CCO~BANK~B} = 197 \text{ mA}$
- From [方程式](#page-33-0) 8: P_{TOTAL} = 3.465 V × (70 mA + 197 mA + 197 mA + 10 mA) = 1642.4 mW
- From [方程式](#page-33-0) 9: P_{RT_PECL} = ((2.57 V 1.47 V)²/50 Ω) + ((1.72 V 1.47 V)²/50 Ω) = 25.5 mW (per output pair)
- From [方程式](#page-33-0) 10: $P_{\text{VTT_PECL}}$ = 1.47 V × [((2.57 V 1.47 V) / 50 Ω) + ((1.72 V 1.47 V) / 50 Ω)] = 39.5 mW (per output pair)
- From [方程式](#page-33-0) 11: $P_{RT HCSL}$ = 0 mW (no HCSL outputs)
- From [方程式](#page-33-0) 12: P_{DEVICE} = 1642.4 mW (10 × (25.5 mW + 39.5 mW)) 0 mW = 992.4 mW

In this worst-case example, the IC device will dissipate about 992.4 mW or 60% of the total power (1642.4 mW), while the remaining 40% will be dissipated in the LVPECL emitter resistors (255 mW for 10 pairs) and termination voltage (395 mW into V_{CCO} - 2 V).

Based on θ_{JA} of 28.5°C/W, the estimated die junction temperature would be about 28.3°C above ambient, or 113.3 °C when $T_A = 85$ °C.

11.3 Power Supply Bypassing

The V_{CC} and V_{CCO} power supplies should have a high-frequency bypass capacitor, such as 0.1 µF or 0.01 µF, placed very close to each supply pin. Place 1-µF to 10-µF decoupling capacitors nearby the device between the supply and ground planes. All bypass and decoupling capacitors should have short connections to the supply and ground plane through a short trace or via to minimize series inductance.

11.3.1 Power Supply Ripple Rejection

In practical system applications, power supply noise (ripple) can be generated from switching power supplies, digital ASICs or FPGAs, and so forth. While power supply bypassing can help filter out some of this noise, it is important to understand the effect of power supply ripple on the device performance. When a single-tone sinusoidal signal is applied to the power supply of a clock distribution device, such as LMK00301, the signal can produce narrow-band phase modulation as well as amplitude modulation on the clock output (carrier). In the single-side band phase noise spectrum, the ripple-induced phase modulation appears as a phase spur level relative to the carrier (measured in dBc).

For the LMK00301, power supply ripple rejection, or PSRR, was measured as the single-sideband phase spur level (in dBc) modulated onto the clock output when a ripple signal was injected onto the V_{CCO} supply. \boxtimes 11-1 shows the PSRR test setup.

图 **11-1. PSRR Test Setup**

A signal generator was used to inject a sinusoidal signal onto the V_{CCO} supply of the DUT board, and the peakto-peak ripple amplitude was measured at the V_{CCO} pins of the device. A limiting amplifier was used to remove amplitude modulation on the differential output clock and convert it to a single-ended signal for the phase noise analyzer. The phase spur level measurements were taken for clock frequencies of 156.25 MHz and 312.5 MHz under the following power supply ripple conditions:

- Ripple amplitude: 100 mVpp on V_{CCO} = 2.5 V
- Ripple frequencies: 100 kHz, 1 MHz, and 10 MHz

Assuming no amplitude modulation effects and small index modulation, the peak-to-peak deterministic jitter (DJ) can be calculated using the measured single-sideband phase spur level (PSRR) as follows:

$$
DJ (ps pk-pk) = [(2*10(PSRR/20)) / (\pi *fCLK)] * 1012
$$
 (13)

The *PSRR vs. Ripple Frequency* plots in *[Typical Characteristics](#page-14-0)* show the ripple-induced phase spur levels for the differential output types at 156.25 MHz and 312.5 MHz . The LMK00301 exhibits very good and wellbehaved PSRR characteristics across the ripple frequency range for all differential output types. The phase spur levels for LVPECL are below -64 dBc at 156.25 MHz and below -62 dBc at 312.5 MHz. Using 方程式 13, these phase spur levels translate to Deterministic Jitter values of 2.57 ps pk-pk at 156.25 MHz and 1.62 ps pk-pk

at 312.5 MHz. Testing has shown that the PSRR performance of the device improves for V_{CCO} = 3.3 V under the same ripple amplitude and frequency conditions.

11.4 Thermal Management

Power dissipation in the LMK00301 device can be high enough to require attention to thermal management. For reliability and performance reasons the die temperature should be limited to a maximum of 125°C. That is, as an estimate, T_A (ambient temperature) plus device power dissipation times R $_{\theta}$ J_A should not exceed 125°C.

The package of the device has an exposed pad that provides the primary heat removal path as well as excellent electrical grounding to the printed circuit board. To maximize the removal of heat from the package a thermal land pattern including multiple vias to a ground plane must be incorporated on the PCB within the footprint of the package. The exposed pad must be soldered down to ensure adequate heat conduction out of the package.

A recommended land and via pattern is shown in \boxtimes 11-2. More information on soldering WQFN packages can be obtained at: [http://www.ti.com/packaging.](http://www.ti.com/packaging)

图 **11-2. Recommended Land and Via Pattern**

To minimize junction temperature it is recommended that a simple heat sink be built into the PCB (if the ground plane layer is not exposed). This is done by including a copper area of about 2 square inches on the opposite side of the PCB from the device. This copper area may be plated or solder coated to prevent corrosion but should not have conformal coating (if possible), which could provide thermal insulation. The vias shown in 图 11-2 should connect these top and bottom copper layers and to the ground layer. These vias act as "heat pipes" to carry the thermal energy away from the device side of the board to where it can be more effectively dissipated.

12 Layout

12.1 Layout Guidelines

Consider the following guidelines for this device:

- Keep the connections between the bypass capacitors and the power supply on the device as short as possible.
- Ground the other side of the capacitor using a low impedance connection to the ground plane.
- If the capacitors are mounted on the back side, 0402 components can be employed. However, soldering to the Thermal Dissipation Pad can be difficult
- For component side mounting, use 0201 body size capacitors to facilitate signal routing.

12.2 Layout Example

13 Device and Documentation Support

13.1 Documentation Support

13.1.1 Related Documentation

Application Note AN-912 *[Common Data Transmission Parameters and their Definitions](https://www.ti.com/lit/pdf/SNLA036)* (SNLA036)

13.2 接收文档更新通知

要接收文档更新通知,请导航至 [ti.com](https://www.ti.com) 上的器件产品文件夹。点击*订阅更新* 进行注册,即可每周接收产品信息更 改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

13.3 支持资源

TI E2E™ [支持论坛](https://e2e.ti.com)是工程师的重要参考资料,可直接从专家获得快速、经过验证的解答和设计帮助。搜索现有解 答或提出自己的问题可获得所需的快速设计帮助。

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13.4 Trademarks

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13.5 静电放电警告

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ESD 的损坏小至导致微小的性能降级,大至整个器件故障。精密的集成电路可能更容易受到损坏,这是因为非常细微的参 数更改都可能会导致器件与其发布的规格不相符。

13.6 术语表

TI [术语表](https://www.ti.com/lit/pdf/SLYZ022) 本术语表列出并解释了术语、首字母缩略词和定义。

14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

PACKAGE OPTION ADDENDUM

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TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal

PACKAGE MATERIALS INFORMATION

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PACKAGE OUTLINE

RHS0048A WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

EXAMPLE BOARD LAYOUT

RHS0048A WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RHS0048A WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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