

Comparing Synchronous to Non-Synchronous Converters

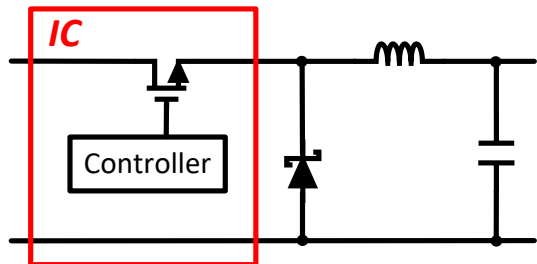
Comparing Size, Cost, Efficiency, & More

Anston Lobo

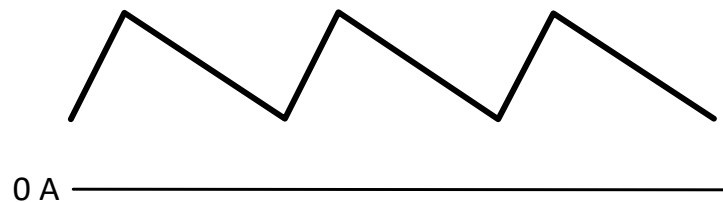
Texas Instruments

Synchronous and non-synchronous buck

Non-Synchronous Buck

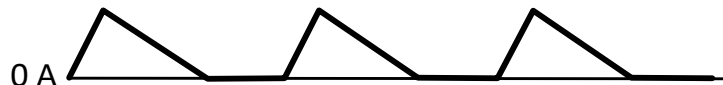


Heavy Load

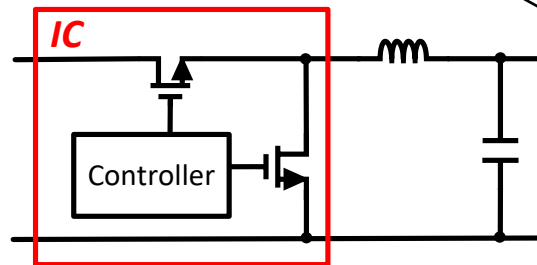


Light Load

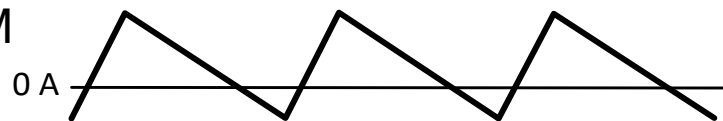
Non-sync



Synchronous Buck



Sync-FPWM

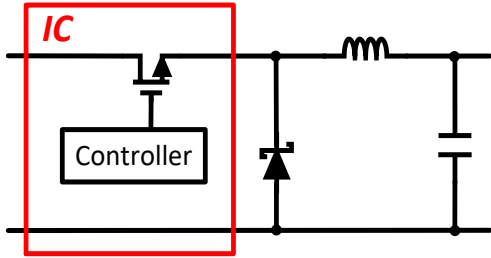


Sync-DCM
(Diode
Emulation)

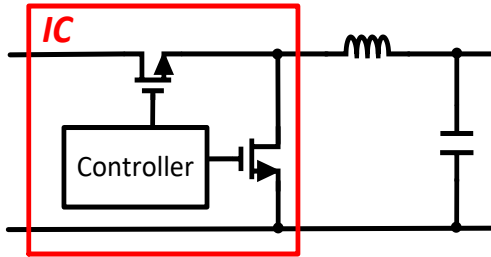


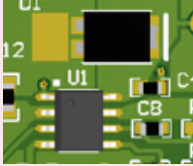
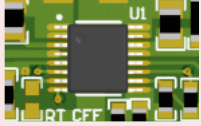
Comparison – Solution size & cost

Non-Synchronous Buck



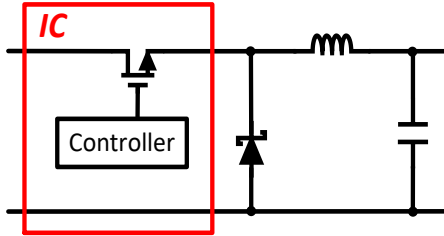
Synchronous Buck



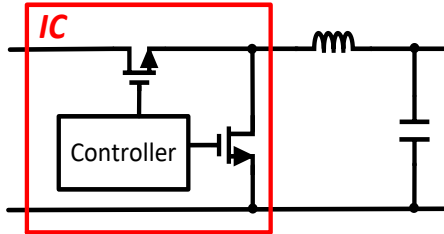
	Non-Sync	Sync
Solution Size	Larger IC + Power Diode	Smaller Both FETs Integrated
Layout		
Cost	IC costs less + Diode cost	IC costs more
Other Considerations		<ul style="list-style-type: none"> ▪ <i>Integrated sync rectifier</i> ▪ <i>More Sophisticated controller & driver</i> ▪ <i>Needs a thermally optimized package</i>

Comparison – Ease of use

Non-Synchronous Buck



Synchronous Buck



	Sync	Non-Sync
Design	Easier	Need to select Schottky diode
External Diode	No need	<p>Selection Considerations</p> <ul style="list-style-type: none"> ➤ Reverse voltage rating V_R $>V_{IN\ max}$ ➤ Forward current rating I_{FWD} $>Load\ max + I_{ripple}/2$ ➤ Forward voltage drop V_{FWD}, over current and temp Conduction loss = $V_{FWD} * I_{FWD}$ ➤ Reverse leakage current over temp Loss = $V_{IN} * I_{leak}$ ➤ Parasitic capacitance Switching loss ➤ Package for heat dissipation ➤ Size increase with V_R and I_F

Power diode example – DIODES B340, 40V 3A

B320/B330/B340

V_{RRM} (V)	I_O (A)	V_F max (V)	I_R max (mA)
20/30/40	3.0	0.5	0.5

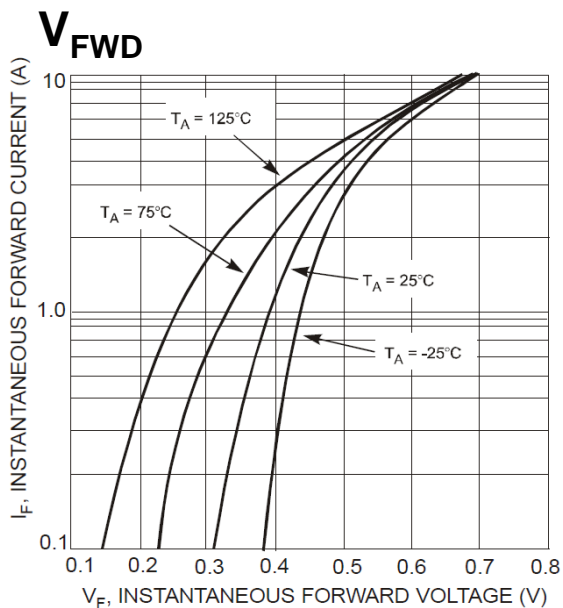


Fig. 1 Typical Forward Characteristics - B320B thru B340B

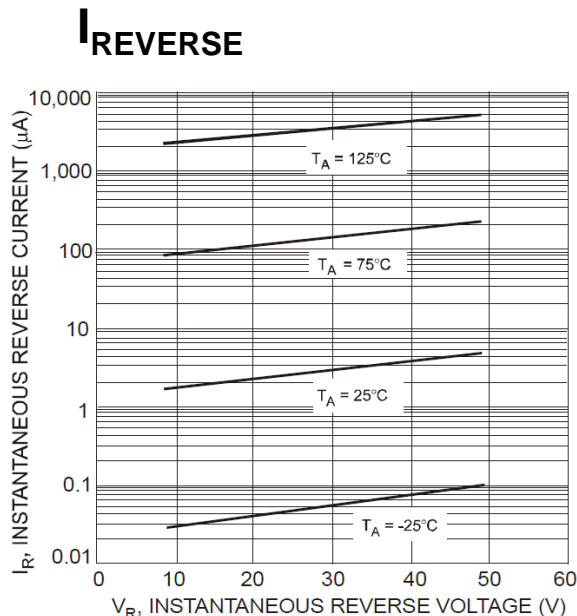
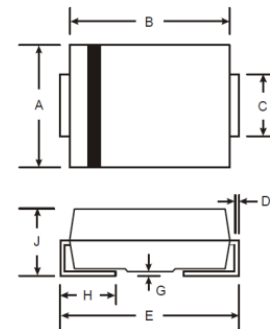


Fig. 3 Typical Reverse Characteristics, B320B thru B340B

Package



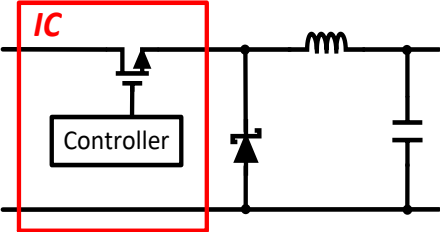
Dim	SMC	
	Min	Max
A	5.59	6.22
B	6.60	7.11
C	2.75	3.18
D	0.15	0.31
E	7.75	8.13
G	0.10	0.20
H	0.76	1.52
J	2.00	2.50

All Dimensions in mm

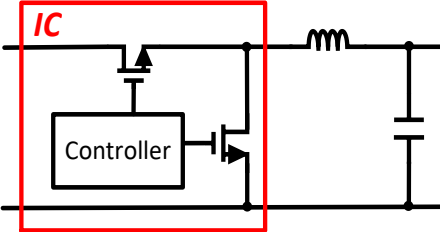
5.59mm×6.6mm

Comparison – Layout to optimize EMI

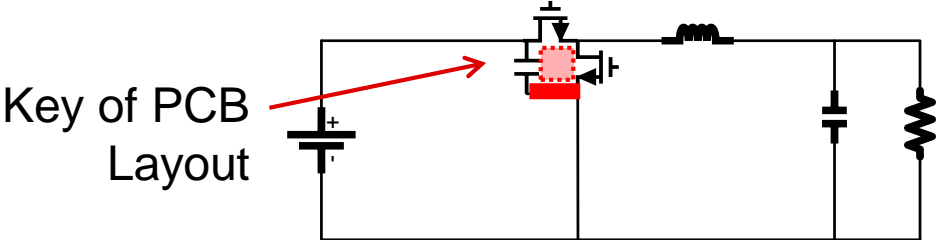
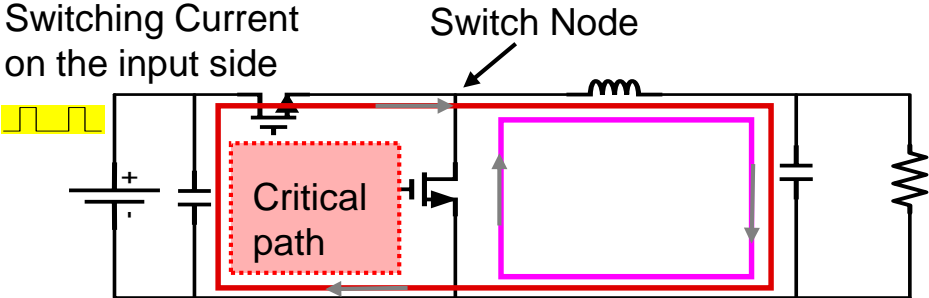
Non-Synchronous Buck



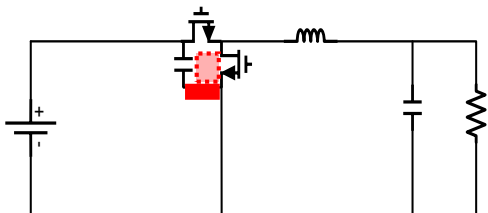
Synchronous Buck



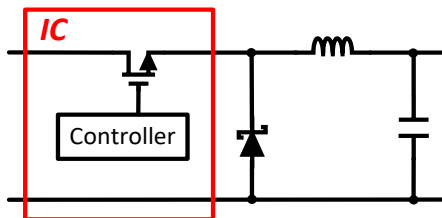
For Any Buck Converter
Reduce Critical Path Area → Reduce EMI



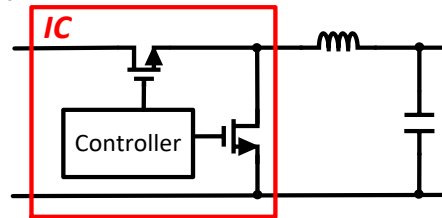
Comparison – Layout to optimize EMI



Non-Synchronous Buck



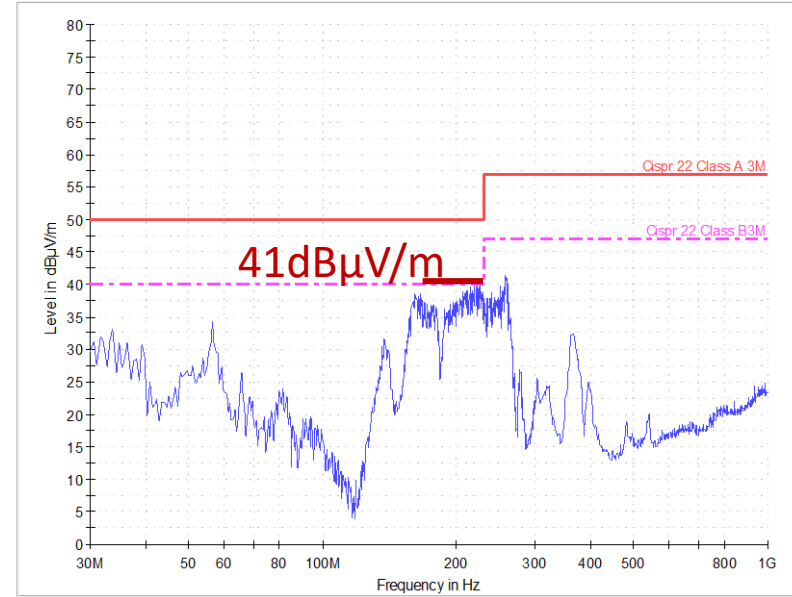
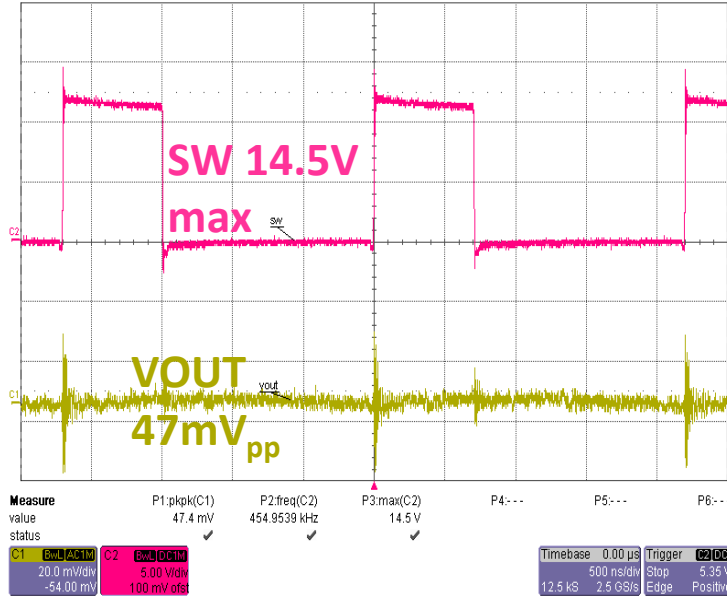
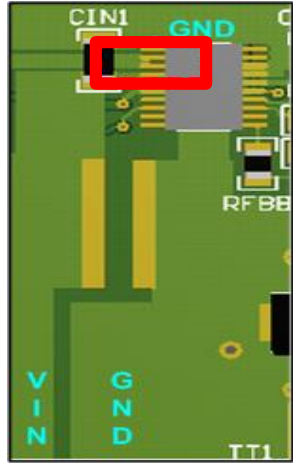
Synchronous Buck



	Non-Sync	Sync
	<p>Harder to optimize EMI by layout (Depends on pin out of IC)</p>	<p>Easier (Depends on pin out of IC)</p>
Layout for EMI		

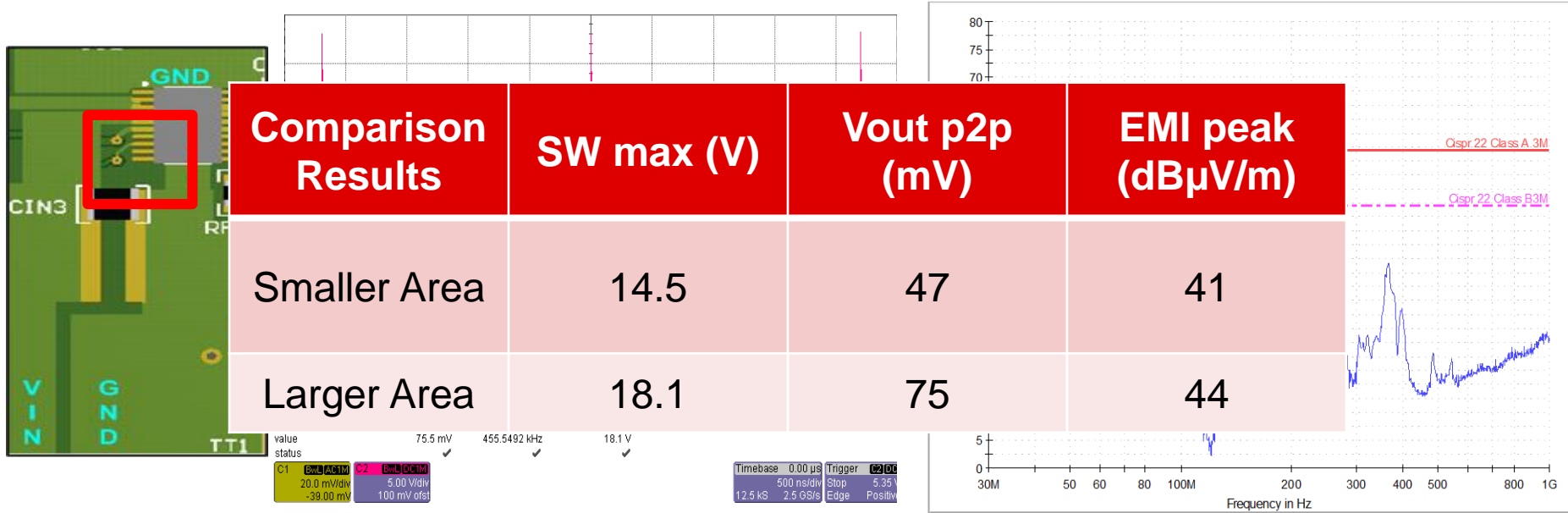
EMI mitigation by PCB layout

Critical Path Area Reduction



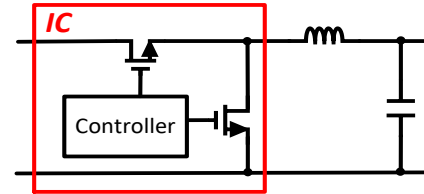
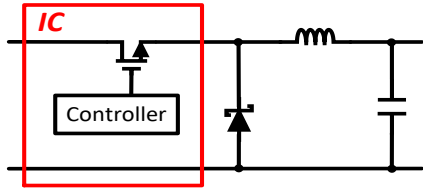
EMI mitigation by PCB layout

Critical Path Area Reduction



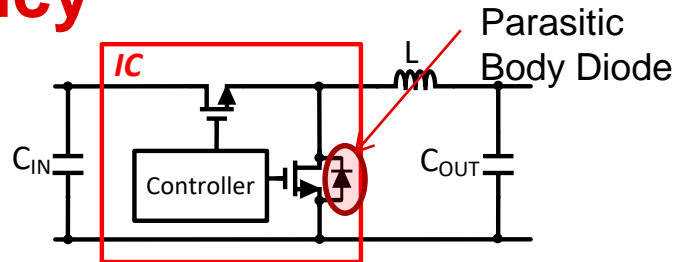
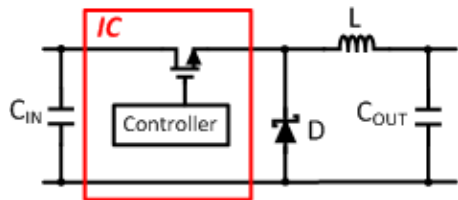
Now shown with single C_{IN} with 2.5 times larger area

Comparison – Light load efficiency



	Non-Sync	Sync - FPWM	Sync - DCM
Light Load Current Waveform			
Negative Current?	No	Yes	No
HS Conduction Losses	Lower I_{RMS} HS: $(I_{RMS-HS}^2) * R_{ON-HS} * D$	Higher I_{RMS} HS: $(I_{RMS-HS}^2) * R_{ON-HS} * D$	Lower I_{RMS} HS: $(I_{RMS-HS}^2) * R_{ON-HS} * D$
LS Conduction Loss	Diode: $I_{Diode} * V_F * t_{Diode} * f_S$	LS: $(I_{RMS-LS}^2) * R_{ON-LS} * (1-D)$	LS: $(I_{RMS-LS}^2) * R_{ON-LS} * t_{LS} * f_S$
Switching Frequency	Reduced at very light load	Constant over load	Reduced at very light load
Switching Losses	Less	More	Less

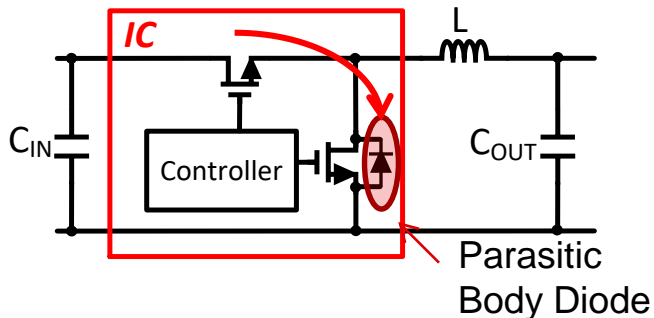
Comparison – Heavy load efficiency



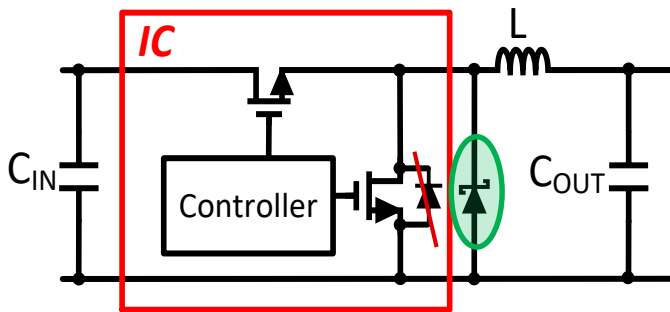
	Non-Sync	Sync – FPWM and DCM
Heavy Load Current Waveform		
Low Side Conduction Losses	Diode: $I_{\text{Diode}} * V_F * (1-D)$	LS: $(I_{\text{RMS-LS}}^2) * R_{\text{ON-LS}} * (1-D)$
HS FET Switching Losses	Less $\frac{1}{2} * (V_{\text{IN}} * I_{\text{OUT}}) * (t_{\text{rise}} + t_{\text{fall}}) * f_s$	More $\frac{1}{2} * (V_{\text{IN}} * I_{\text{OUT}}) * (t_{\text{rise}} + t_{\text{fall}}) * f_s + Q_{\text{rr}} * f_s * V_{\text{IN}}$ Q _{rr} : LS Body diode Reverse recovery charge

Comparison – Efficiency

Synchronous Buck

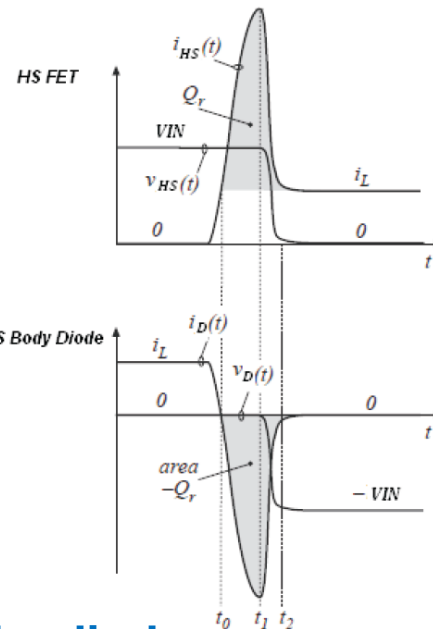


To have the best of both worlds



Parasitic Body Diode

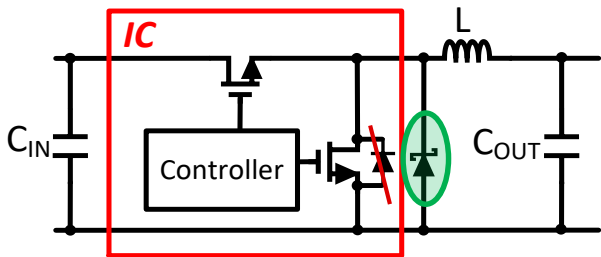
- Conduct during dead-time
- Reverse Recover Charge increases switching loss
- Increase ringing in SW node



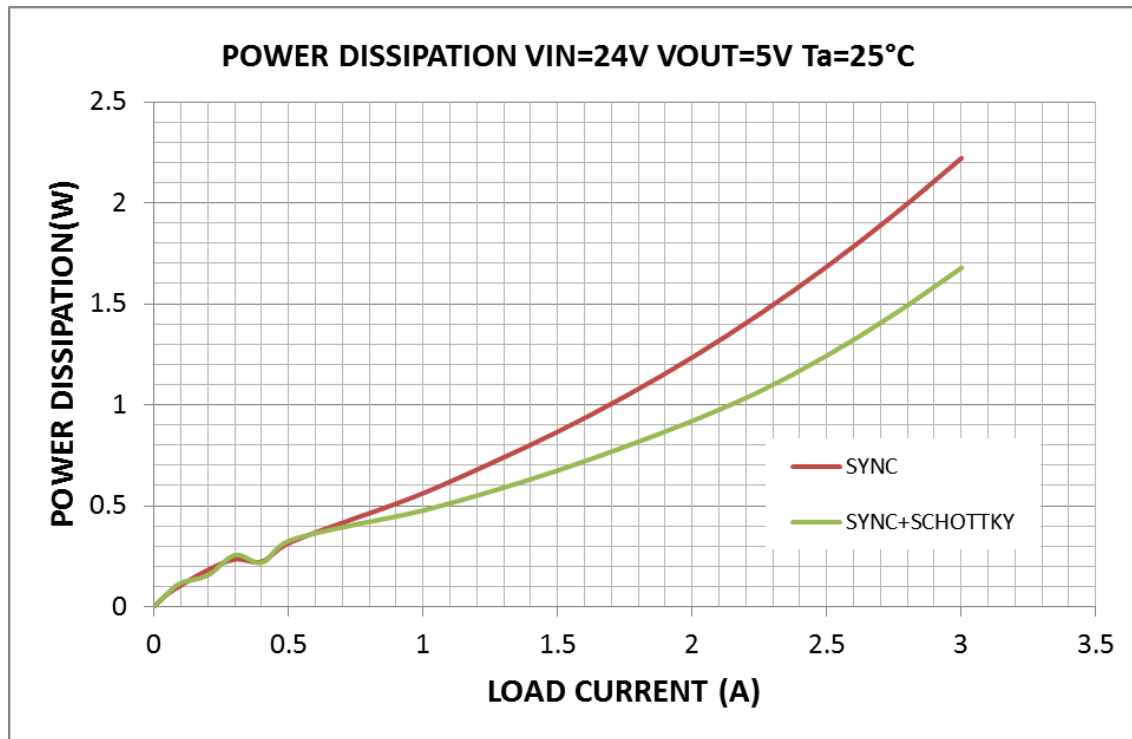
Parallel a SMALL Schottky diode

- Bypass body diode during dead-time
- No reverse recover charge
- Current rating can be a fraction of the power diode for a non-sync buck – only conducts during deadtime

Efficiency improvement with small Schottky



Improvement depends on switching loss from Q_{rr}

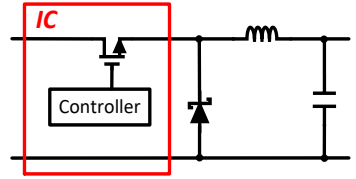


Comparison – Efficiency summary

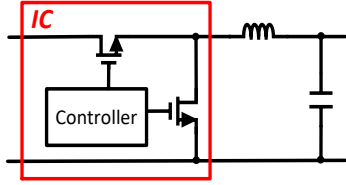
	Non-Sync	Sync-FPWM	Sync-DCM	Sync + Small Schottky
Light Load Efficiency	Better	Worse	Better	Better
Heavy Load Conduction Losses	More	Less	Less	Less
Heavy Load Switching Losses	Less	More	More	Less
Fixed Switching Frequency	No	Yes	No	No
Lower V_{OUT}	Worse (V_F)	Better	Better	Better

Comparison – Thermal performance

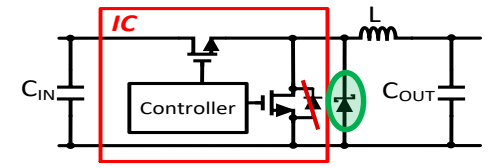
Non-Synchronous Buck

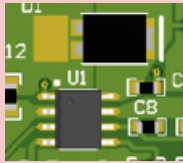
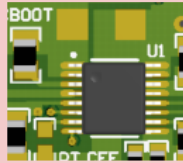
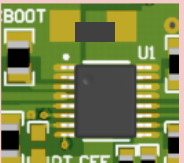
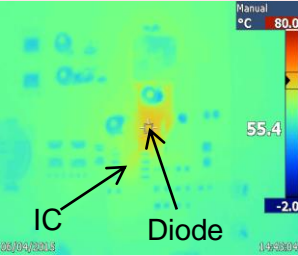
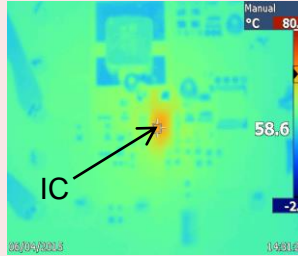



Synchronous Buck

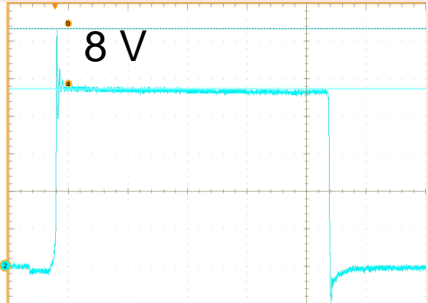
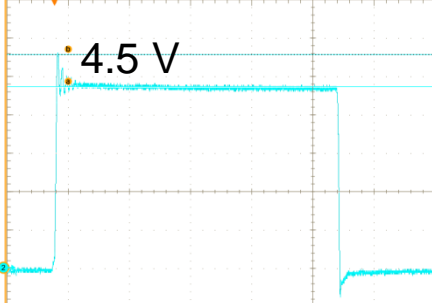
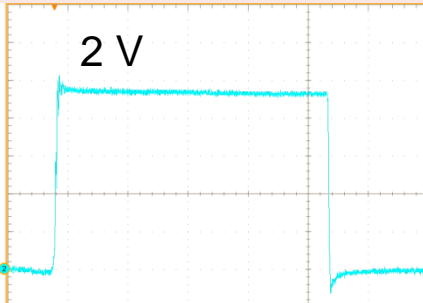
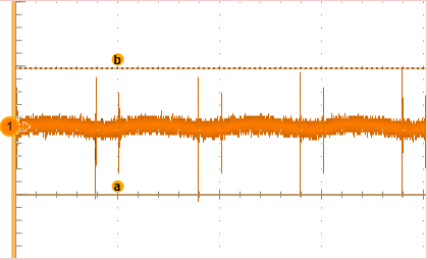
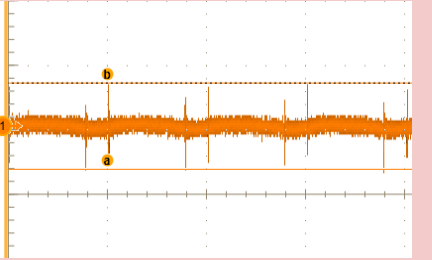
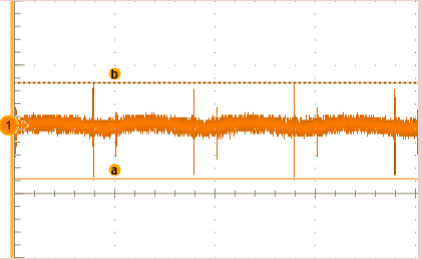


Synchronous + small Schottky

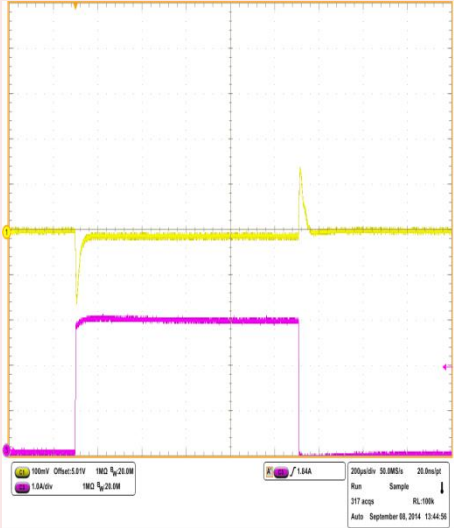
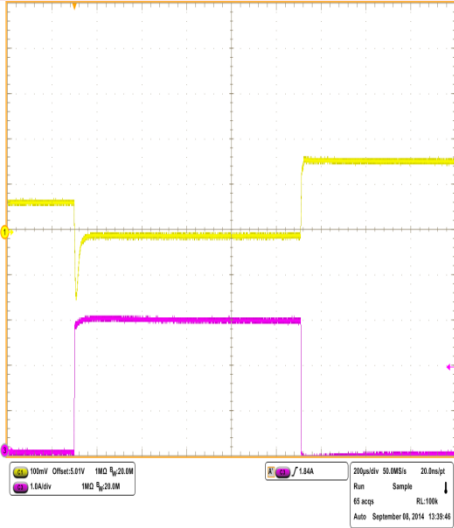


	Non-Sync	Sync	Sync + Small Schottky
Thermal	<p>Better</p> <p>Two packages</p> <p>LMR14030</p> 	<p>Harder</p> <p>One package</p> <p>LM43603</p> 	<p>Loss and heat reduced by Schottky diode</p> <p>LM43603</p> 
<p>Example</p> <p>$V_{IN} = 24V$</p> <p>$V_{OUT} = 5V$</p> <p>Load = 3A</p> <p>500kHz</p>			

Comparison – Noise

	Sync	Non-Sync	Sync + Small Schottky
V_{OUT} Spike	More - Body diode reverse recovery	Less - Schottky diode	Less – small Schottky diode
SW Ringing Peak V_{IN} = 24V V_{OUT} = 5V Load = 3A 500kHz			
V_{OUT} Spikes V_{IN} = 24V V_{OUT} = 5V Load = 3A 500kHz			

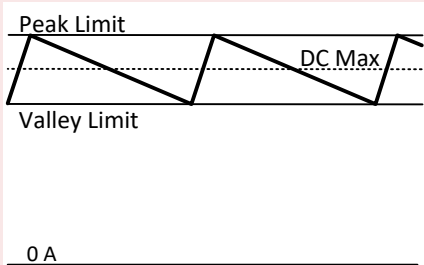
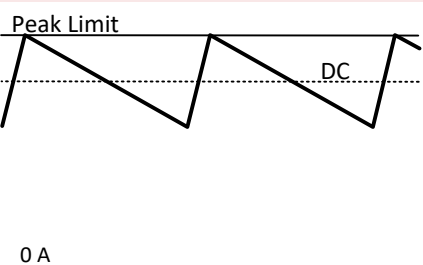
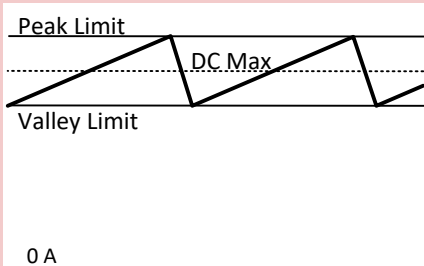
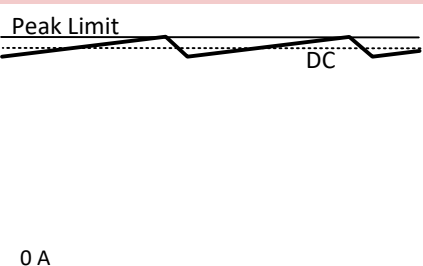
Comparison – Unloading transient

	Sync-FPWM	Sync-DCM	Non-Sync
Unloading Transient Overshoot	Good Allow neg current to discharge C_{OUT}	Worse Depend on load to discharge C_{OUT}	Worse Depend on load to discharge C_{OUT}
Example $V_{IN} = 8V$ $V_{OUT} = 5V$ Load = 3A $F_S = 2.2MHz$ LM53603 set at FPWM and DCM modes	 <p>The waveform shows a steady-state output voltage (yellow) at 5V and a load current (purple) at 3A. When the load is removed, the output voltage remains stable with a very small negative transient spike. The load current drops to zero.</p>	 <p>The waveform shows a steady-state output voltage (yellow) at 5V and a load current (purple) at 3A. When the load is removed, the output voltage exhibits a significant negative transient spike, and the load current (purple) shows a large negative spike, indicating the capacitor is being discharged by the inductor current.</p>	Same as Sync-DCM

Comparison – Controllability

	Non-Sync	Sync
Controllability	Limited Only controls one FET	Better Controls both FETs Info from both FETs
Current Limit	Peak current only	Peak current Valley current Average current (depends on controller)
OVP	Cannot actively pull down V_{OUT}	Can actively pull down V_{OUT} (depends on controller)
Control architecture		More options

Comparison – Current limit

	Sync	Non-Sync
DC current limiting	Control of Peak current and Valley current → more accurate DC current limiting	Only has control of Peak current DC current limit depends on ripple
Fast slew rate		
Slow slew rate		

Comparison – Summary

	Non-Synchronous	Synchronous
Size / Ease of use	Larger size	Smaller size, Easier to Use
Light Load Efficiency	Better	Worse with FPWM, better with DCM
Heavy Load Efficiency	More conduction loss Less switching loss	Less conduction loss More switching loss due to reverse recovery Adding small Schottky gives highest efficiency
Lower V_{OUT}	Lower Efficiency (V_F/V_{OUT})	Higher Efficiency
Thermal	Better with two packages	Harder with one package Adding small Schottky reduces power loss a lot
Fixed F_{SW}	No	Yes with FPWM, No with DCM
Noise	less	More, due to body diode reverse recover charge Adding small Schottky diode reduces noise a lot
Unloading Transient	Worse	Good with FPWM, worse with DCM
Controllability	No LS control	More control flexibility



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