

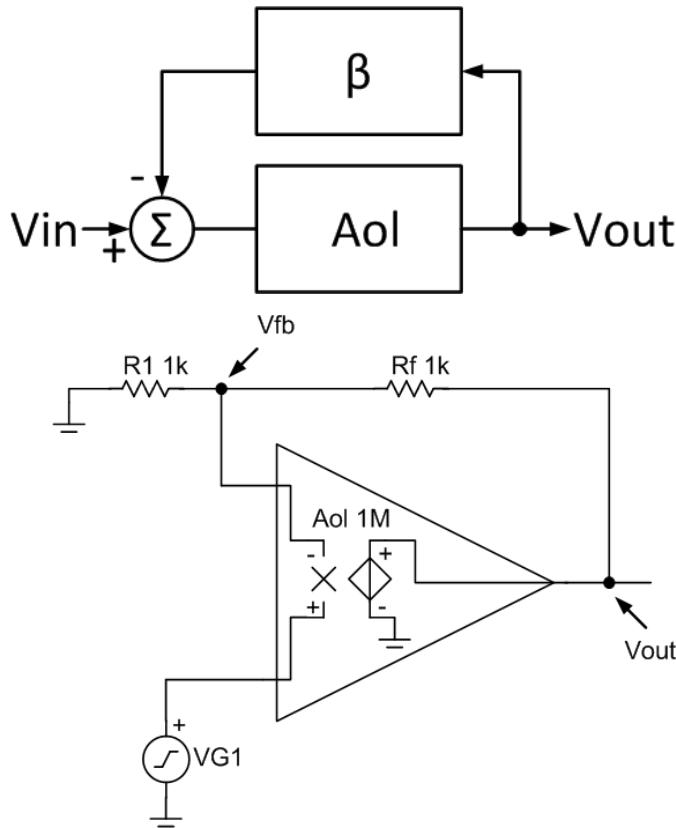
帯域幅 2 TI プレシジョン・ラボーオペアンプ

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TEXAS INSTRUMENTS

オペアンプ帯域幅



A_{ol} = Open loop Gain

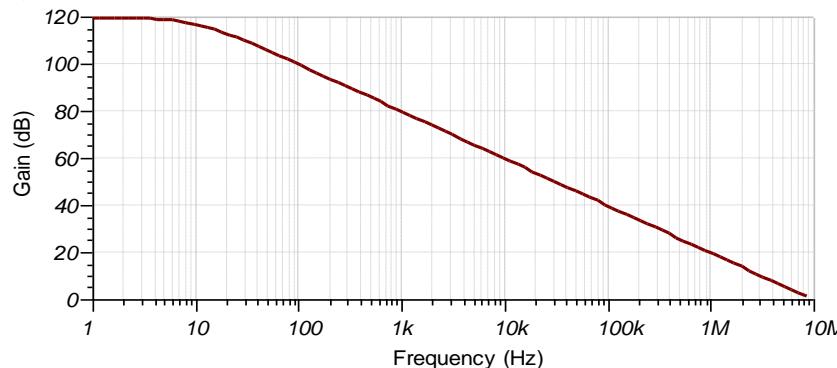
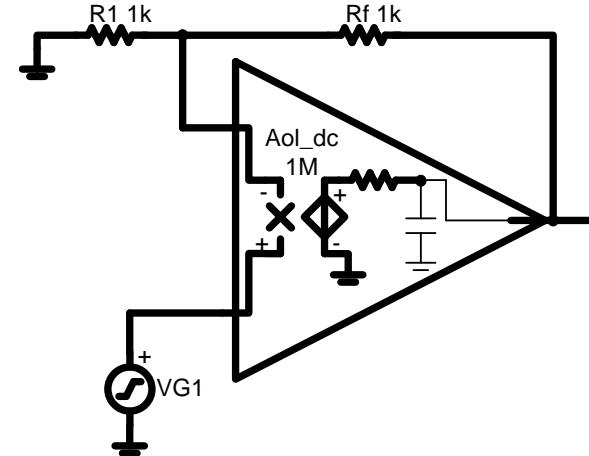
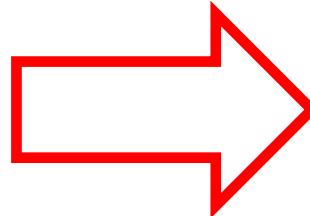
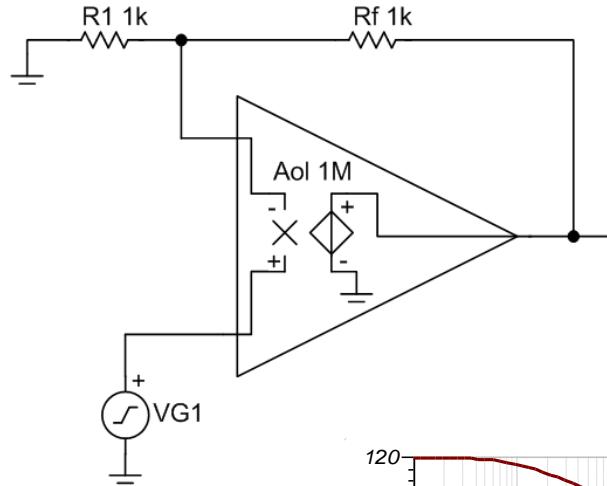
$$\beta = \text{Feedback Factor} = \frac{V_{fb}}{V_{out}} = \frac{R_1}{R_1 + R_f}$$

$$A_{cl} = \text{Closed Loop Gain} = \frac{A_{ol}}{1 + A_{ol}\beta}$$

$A_{ol}\beta$ = Loop Gain

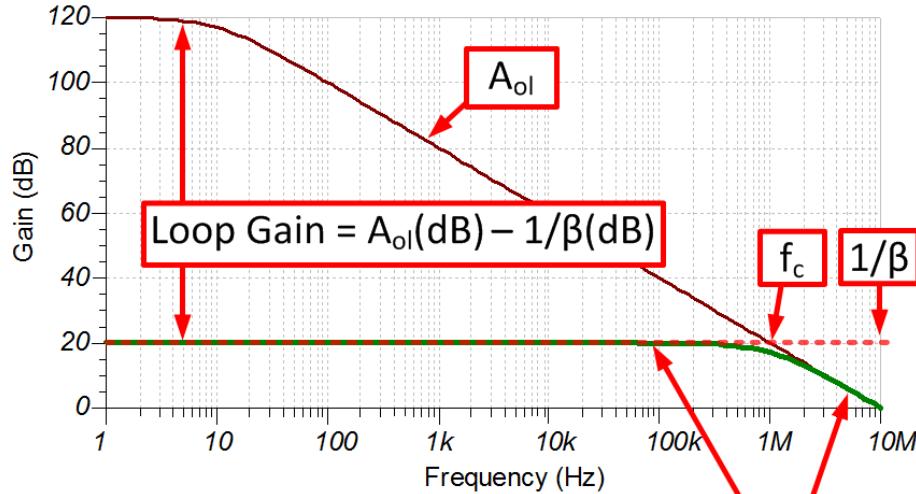
$$A_{cl} = \lim_{A_{ol}\beta \rightarrow \infty} \left(\frac{A_{ol}}{1 + A_{ol}\beta} \right) = \frac{1}{\beta} = 1 + \frac{R_f}{R_1}$$

オペアンプ帯域幅



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ループ・ゲイン、閉ループ・ゲイン& A_{ol}



$$\log(A_{ol}\beta) = \log(A_{ol}) + \log(\beta)$$

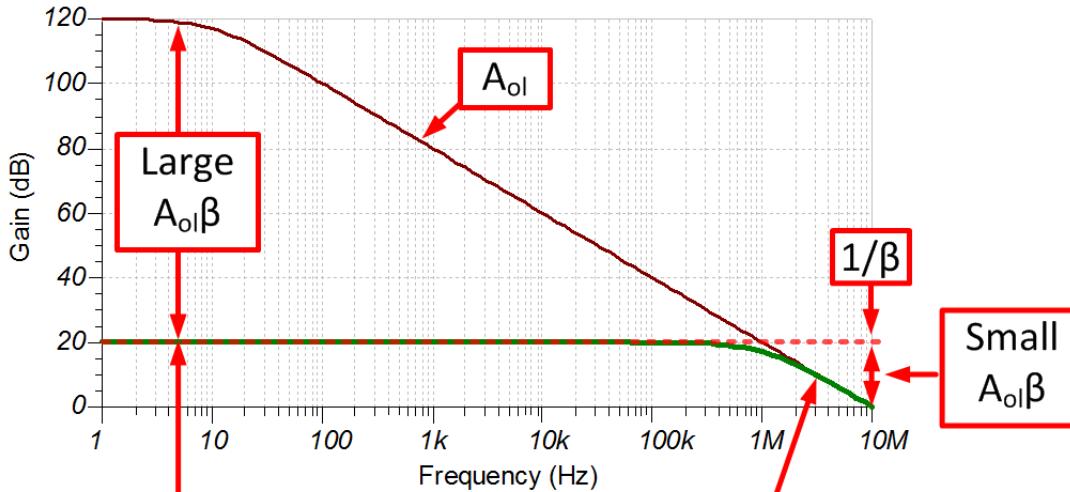
$$\log(A_{ol}\beta) = \log(A_{ol}) - \log\left(\frac{1}{\beta}\right)$$

Closed
Loop Gain



TEXAS INSTRUMENTS

ループ・ゲイン、閉ループ・ゲイン& A_{ol}



$$A_{cl} = 1/\beta \text{ for Large } A_{ol}\beta$$

$$A_{cl} = \lim_{A_{ol}\beta \rightarrow \infty} \left(\frac{A_{ol}}{1 + A_{ol}\beta} \right) = \frac{1}{\beta} = 1 + \frac{R_f}{R_1}$$

$$A_{cl} = A_{ol} \text{ for Small } A_{ol}\beta$$

$$A_{cl} = \lim_{A_{ol}\beta \rightarrow 0} \left(\frac{A_{ol}}{1 + A_{ol}\beta} \right) = A_{ol}$$



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帯域幅 製品仕様例

PARAMETER	CONDITIONS	STANDARD GRADE OPA827AI			HIGH GRADE OPA827I ⁽¹⁾⁽²⁾			UNIT
		MIN	TYP	MAX	MIN	TYP	MAX	
FREQUENCY RESPONSE								
Gain-Bandwidth Product	GBW	G = +1		22		22		MHz

$$\text{GBW} = \text{Gain} \cdot \text{BW}$$

In this example, for any gain from 0dB to Avol.

where

GBW -- Gain Bandwidth in Hz

Gain -- closed loop voltage gain

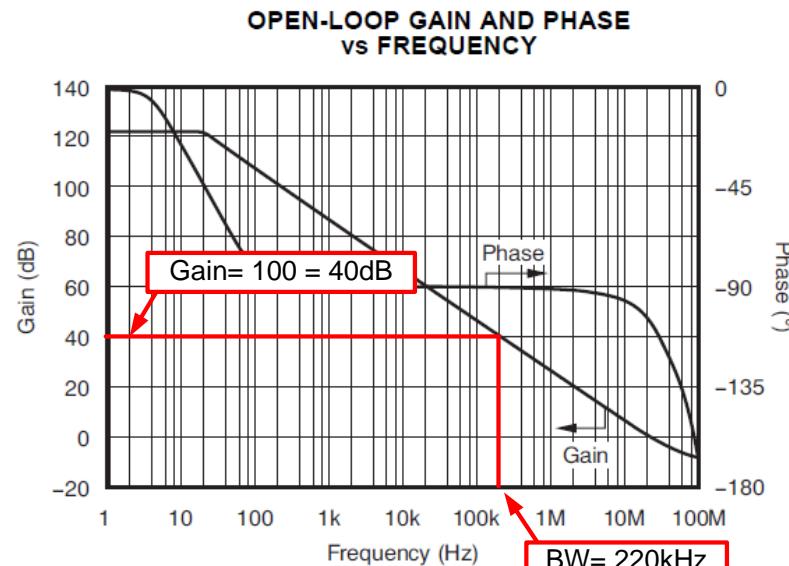
BW -- Bandwidth in Hz

For example

$$\text{Gain} = 100$$

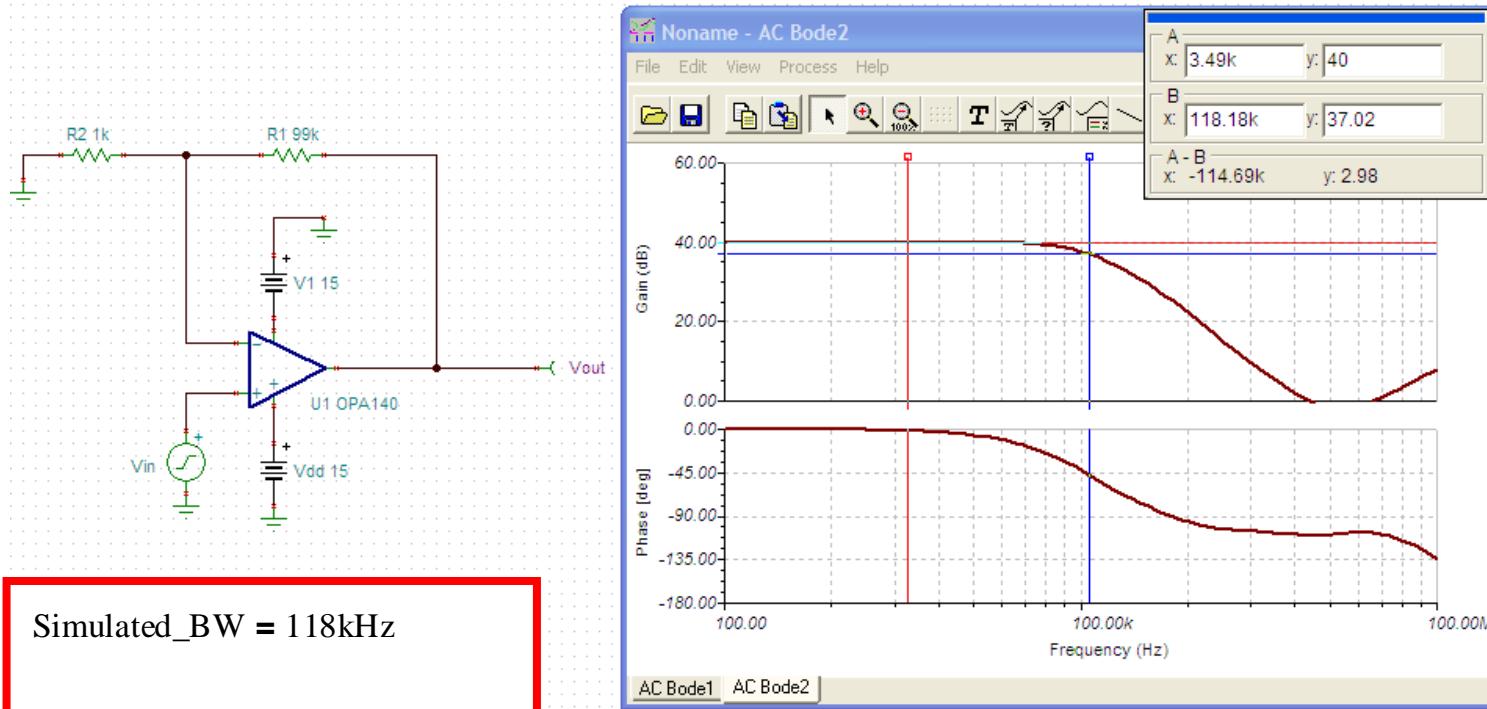
Closed Loop Bandwidth is calculated:

$$\text{BW} = \frac{\text{GBW}}{\text{Gain}} = \frac{22\text{MHz}}{100} = 220\text{kHz}$$



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シミュレーション : Non-inverting Gain of 100V/V



Simulated_BW = 118kHz

$$BW = \frac{GBW}{Gain} = \frac{11MHz}{100} = 110kHz$$

带域幅 vs. I_q

Op Amp	Typical GBW	Typical I _q
OPA369	12kHz	0.8uA
OPA333	350kHz	17uA
OPA277	1MHz	790uA
OPA129	1MHz	1.2mA
OPA827	22MHz	4.8mA
OPA350	38MHz	5.2mA
OPA211	45MHz (Gain=1)	3.6mA
OPA835	51MHz (Gain=1)	250uA
OPA847	600MHz (Gain=12)	18.1mA



带域幅 vs. I_q

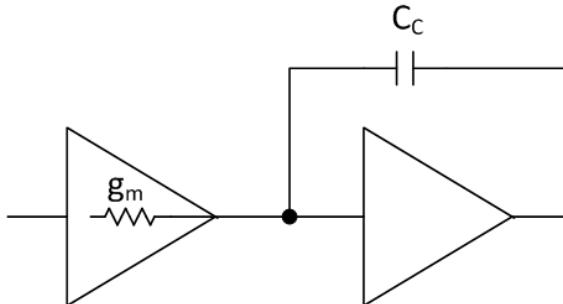
BIPOLAR

$$g_m = \frac{q \cdot I_c}{k \cdot T}$$

$$r_{gm} = \frac{1}{g_m}$$

$$BW = \frac{g_m}{2 \cdot \pi C_c} = \frac{1}{2 \cdot \pi C_c \cdot r_{gm}}$$

$$BW = \frac{q \cdot I_c}{2 \cdot \pi C_c \cdot k \cdot T}$$



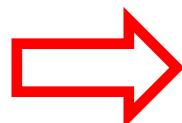
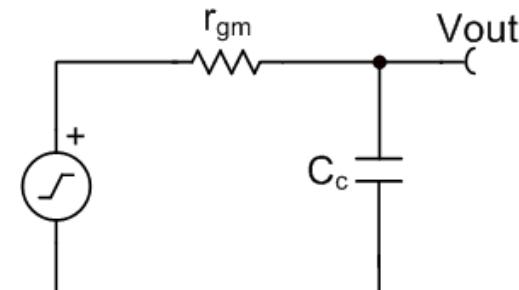
MOSFET

$$g_m = \sqrt{2 \cdot I_D \cdot \mu \cdot C_{ox} \cdot \frac{W}{L}}$$

$$r_{gm} = \frac{1}{g_m}$$

$$BW = \frac{g_m}{2 \cdot \pi C_c} = \frac{1}{2 \cdot \pi C_c \cdot r_{gm}}$$

$$BW = \frac{\sqrt{2 \cdot I_D \cdot \mu \cdot C_{ox} \cdot \frac{W}{L}}}{2 \cdot \pi C_c}$$



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ありがとうございました