

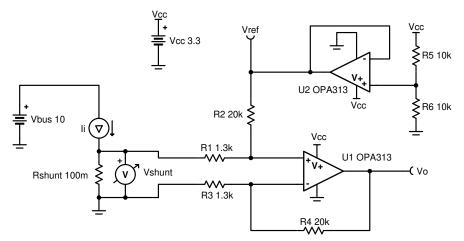
Tushar Jog

### **Design Goals**

Input		Output		Supply		
l <sub>iMin</sub>	I <sub>iMax</sub>	V <sub>oMin</sub>	V <sub>oMax</sub>	V <sub>cc</sub>	V <sub>ee</sub>	V <sub>ref</sub>
-1A	1A	110mV	3.19V	3.3V	0V	1.65V

#### **Design Description**

This single-supply low-side, bidirectional current sensing solution can accurately detect load currents from –1A to 1A. The linear range of the output is from 110mV to 3.19V. Low-side current sensing keeps the common-mode voltage near ground, and is thus most useful in applications with large bus voltages.



### **Design Notes**

- 1. To minimize errors, set  $R_3 = R_1$  and  $R_4 = R_2$ .
- 2. Use precision resistors for higher accuracy.
- 3. Set output range based on linear output swing (see Aol specification).
- 4. Do not use low-side sensing in applications where the system load cannot withstand small ground disturbances or in applications that need to detect load shorts.

#### **Design Steps**

1. Determine the transfer equation given  $R_4 = R_2$  and  $R_1 = R_3$ .

$$V_{o} = \left(I_{i} \times R_{shunt} \times \frac{R_{4}}{R_{3}}\right) + V_{ref}$$
$$V_{ref} = V_{cc} \times \left(\frac{R_{6}}{R_{5} + R_{6}}\right)$$

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2. Determine the maximum shunt resistance.

$$R_{shunt} = \frac{V_{shunt}}{I_{imax}} = \frac{100mV}{1} = 100m\Omega$$

3. Set reference voltage. Since the input current range is symmetric, set the reference to mid supply. Therefore, make  $R_5$  and  $R_6$  equal.

$$R_5 = R_6 = 10k\Omega$$

4. Set the difference amplifier gain based on the op amp output swing. The op amp output can swing from 100mV to 3.2V, given a 3.3-V supply.

$$Gain = \frac{V_{0Max} - V_{0Min}}{R_{shunt} \times (I_{iMax} - I_{iMin})} = \frac{3.2 V - 100mV}{100m\Omega \times (1 A - (-1 A))} = 15.5 \frac{V}{V}$$

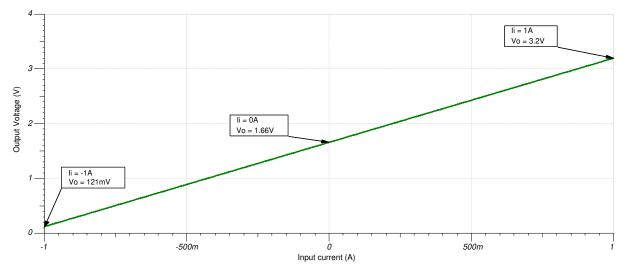
 $Gain = \frac{R_4}{R_3} = 15 .5 \frac{V}{V}$ 

Choose  $R_1 = R_3 = 1.3k\Omega$  (Standard Value)

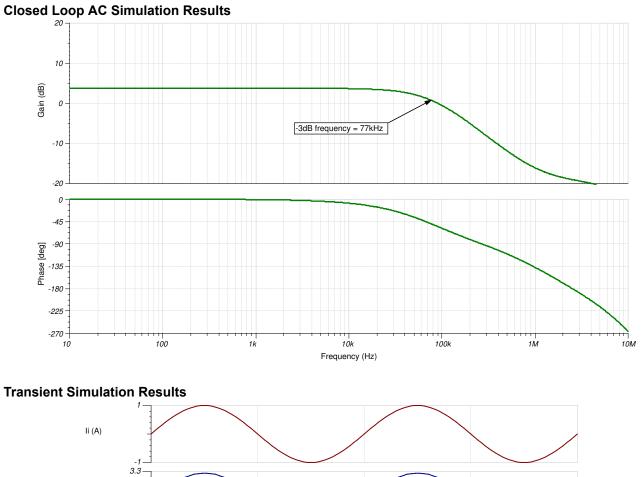
 $R_2 = R_4 = 15.5 \frac{V}{V} \times 1.3 k\Omega = 20.15 k\Omega \approx 20 k\Omega$  (Standard Value)

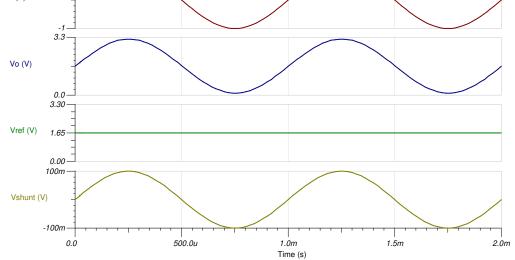
## **Design Simulations**

## **DC Simulation Results**









# **Design References**

Texas Instruments, *Simulation for Low-Side Bidirectional Current-Sensing Circuit*, circuit SPICE simulation file Texas Instruments, ±1A *Single-Supply Low-Side Current Sensing Solution*, reference design

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### **Design Featured Op Amp**

OPA313			
V <sub>cc</sub>	1.8V to 5.5V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>out</sub>	Rail-to-rail		
V <sub>os</sub>	500µV		
Ιq	50µA/Ch		
l <sub>b</sub>	0.2pA		
UGBW	1MHz		
SR	0.5V/µs		
#Channels	1, 2, 4		
OPA313			

### **Design Alternate Op Amp**

	TLV9062	OPA376
V <sub>cc</sub>	1.8V to 5.5V	2.2V to 5.5V
V <sub>inCM</sub>	Rail-to-rail	Rail-to-rail
V <sub>out</sub>	Rail-to-rail	Rail-to-rail
V <sub>os</sub>	300µV	5µV
l <sub>q</sub>	538µA/Ch	760µA/Ch
l <sub>b</sub>	0.5pA	0.2pA
UGBW	10MHz	5.5MHz
SR	6.5V/µs	2V/µs
#Channels	1, 2, 4	1, 2, 4
	TLV9062	OPA376

For battery-operated or power-conscious designs, outside of the original design goals described earlier, where lowering total system power is desired.

LPV821		
V <sub>cc</sub>	1.7V to 3.6V	
V <sub>inCM</sub>	Rail-to-rail	
V <sub>out</sub>	Rail-to-rail	
V <sub>os</sub>	1.5µV	
l <sub>q</sub>	650nA/Ch	
I <sub>b</sub>	7pA	
UGBW	8KHz	
SR	3.3V/ms	
#Channels	1	
LPV821		

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# **Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

С	hanges from Revision B (January 2019) to Revision C (October 2024)	Page
•	Updated the format for tables, figures, and cross-references throughout the document	1

CI	Changes from Revision A (May 2018) to Revision B (January 2019)		
•	Downscale the title	1	
•	Added link to circuit cookbook landing page	1	

CI	hanges from Revision * (February 2018) to Revision A (May 2018)	Page
•	Changed title role to Amplifiers	1
•	Added SPICE simulation file link	1
•	Added LPV821 as a Design Alternate Op Amp for battery-operated or power-conscious designs	1

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