

# LM2103 8V UVLO (低電圧ロックアウト) とデッドタイム制御機能と反転入力搭載、107V、0.5A/0.8A ハーフブリッジ・ドライバ

## 1 特長

- ハーフブリッジ構成の 2 つの N チャンネル MOSFET を駆動
- 8-V GVDD の低電圧誤動作防止 (代表値)
- BST での電圧 (絶対最大値) : 107V
- SH での負過渡電圧 (絶対最大値) : -19.5V
- ソース / シンク電流 (ピーク時) : 0.5A/0.8A
- 固定内部デッドタイム (代表値) : 475ns
- クロス導通防止機能を内蔵
- 伝搬遅延時間 (代表値) : 115ns
- 反転入力ピン  $\overline{\text{INL}}$

## 2 アプリケーション

- [ブラシレス DC \(BLDC\) モータ](#)
- 永久磁石同期モータ (PMSM)
- [サーボおよびステッパ・モータ駆動](#)
- [コードレス掃除機](#)
- [コードレスの園芸用器具および電動工具](#)
- [電動アシスト自転車および電動スクーター](#)
- [バッテリー試験装置](#)
- [オフライン無停電電源 \(UPS\)](#)
- 汎用 MOSFET または IGBT ドライバ

## 3 概要

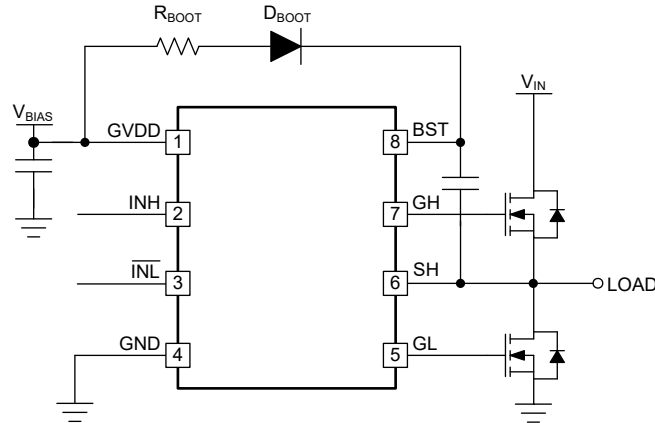
LM2103 は、同期整流式降圧型またはハーフブリッジの構成においてハイサイドとローサイド両方の N チャンネル MOSFET を駆動するよう設計された、コンパクトな高電圧ゲート・ドライバです。 $\overline{\text{INL}}$  反転入力により、このドライバはデュアルまたはシングル PWM 入力アプリケーションで使用できます。

固定のデッドタイムと、SH ピンでの DC -1V および -19.5V の過渡負電圧処理により、高ノイズ・アプリケーションにおけるシステムの堅牢性が向上します。LM2103 は、業界標準のピン配置と互換性のある 8 ピン SOIC パッケージで供給されます。ローサイドとハイサイドの両方の電源レールに低電圧誤動作防止機能 (UVLO) が搭載されており、電源投入および電源切断時の保護を実現します。

### 製品情報

部品番号	パッケージ (1)	本体サイズ (公称)
LM2103	D (SOIC, 8)	4.90mm × 3.91mm

(1) 利用可能なすべてのパッケージについては、データシートの末尾にある注文情報を参照してください。



アプリケーション概略図



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## 4 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

Changes from Revision * (April 2023) to Revision A (August 2023)	Page
• 非公開の事前情報から公開量産データに変更.....	1

## 5 Pin Configuration and Functions

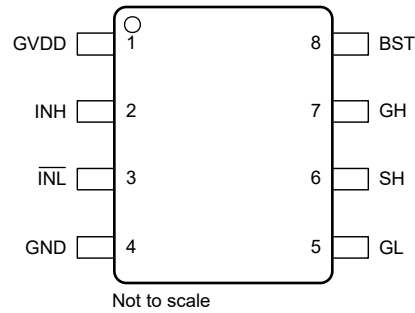


図 5-1. D Package, 8-Pin SOIC (Top View)

表 5-1. Pin Functions

PIN			DESCRIPTION
NO.	NAME	TYPE <sup>(1)</sup>	
1	GVDD	P	Gate driver positive supply rail. Locally decouple to ground using low ESR and ESL capacitor located as close to IC as possible.
2	INH	I	High-side control input. The INH input is compatible with TTL and CMOS input thresholds. Unused INH input must be tied to ground and not left open.
3	$\overline{\text{INL}}$	I	Low-side control input. The inverting $\overline{\text{INL}}$ input is compatible with TTL and CMOS input thresholds. Unused $\overline{\text{INL}}$ input must be tied to GVDD and not left open.
4	GND	G	Ground. All signals are referenced to this ground.
5	GL	O	Low-side gate driver output. Connect to the gate of the low-side MOSFET or one end of external gate resistor, when used.
6	SH	P	High-side source connection. Connect to the negative terminal of the bootstrap capacitor and to the source of the high-side MOSFET.
7	GH	O	High-side gate driver output. Connect to the gate of the high-side MOSFET or one end of external gate resistor, when used.
8	BST	P	High-side gate driver positive supply rail. Connect the positive terminal of the bootstrap capacitor to BST and the negative terminal of the bootstrap capacitor to SH. The bootstrap capacitor must be placed as close to IC as possible.

(1) G = Ground, I = Input, O = Output, and P = Power

## 6 Specifications

### 6.1 Absolute Maximum Ratings

Over operating junction temperature range and all voltages are with respect to GND (unless otherwise noted).<sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>GVDD</sub>	Low-side supply voltage	-0.3	19.5	V
V <sub>BST</sub> to V <sub>SH</sub>	High-side supply voltage	-0.3	19.5	V
V <sub>INL</sub> , V <sub>INH</sub>	Input voltages on INL and INH	-0.3	19.5	V
V <sub>GL</sub>	Output voltage on GL	-0.3	GVDD + 0.3	V
V <sub>GH</sub>	Output voltage on GH	V <sub>SH</sub> - 0.3	V <sub>BST</sub> + 0.3	V
V <sub>SH</sub>	Voltage on SH	DC	-1	95
		Repetitive pulse < 100 ns <sup>(2)</sup>	-19.5	95
V <sub>BST</sub>	Voltage on BST	V <sub>SH</sub>	107	V
T <sub>J</sub>	Junction temperature	-40	125	°C
T <sub>stg</sub>	Storage temperature	-65	150	°C

- (1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) Values are verified by characterization and are not production tested.

### 6.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±1000
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±250

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

Over operating junction temperature range and all voltages are with respect to GND (unless otherwise noted).

		MIN	NOM	MAX	UNIT
V <sub>GVDD</sub>	Supply voltage	9	12	18	V
V <sub>INL</sub> , V <sub>INH</sub>	Input Voltage Range	0	V <sub>GVDD</sub> + 0.3		V
V <sub>BST</sub>	Voltage on BST	V <sub>SH</sub> + 9		105	V
V <sub>SH</sub>	Voltage on SH (DC)	-1	V <sub>BST</sub> - V <sub>GVDD</sub>		V
V <sub>SH</sub>	Voltage on SH (repetitive pulse < 100 ns) <sup>(1)</sup>	-18	V <sub>BST</sub> - V <sub>GVDD</sub>		V
SR <sub>SH</sub>	Voltage slew rate on SH			50	V/ns
T <sub>J</sub>	Operating junction temperature	-40		125	°C

- (1) Values are verified by characterization and are not production tested.

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		LM2103	UNIT
		D (SOIC)	
		8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	133.2	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	75.2	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	76.7	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	25.5	°C/W

## 6.4 Thermal Information (continued)

THERMAL METRIC <sup>(1)</sup>		LM2103	UNIT
		D (SOIC)	
		8 PINS	
$\Psi_{JB}$	Junction-to-board characterization parameter	75.9	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report, SPRA953.

## 6.5 Electrical Characteristics

$V_{GVDD} = V_{BST} = 12\text{ V}$ ,  $GND = V_{SH} = 0\text{ V}$ , No Load on GL or GH,  $T_J = 25^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>SUPPLY CURRENTS</b>						
$I_{GVDD}$	GVDD quiescent current	$V_{INL} = 3\text{ V}$ , $V_{INH} = 0\text{ V}$		430		$\mu\text{A}$
$I_{DDO}$	GVDD operating current	$f = 50\text{ kHz}$ , $C_{LOAD} = 0$		0.56		mA
$I_{BST}$	Total BST quiescent current	$V_{INL} = 3\text{ V}$ , $V_{INH} = 0\text{ V}$ , $V_{DD} = 12\text{ V}$		150		$\mu\text{A}$
$I_{BSTO}$	Total BST operating current	$f = 50\text{ kHz}$ , $C_{LOAD} = 0$		0.16		mA
$I_{BSTS}$	BST to GND quiescent current	$V_{SH} = V_{BST} = 95\text{ V}$ , $GVDD = 12\text{ V}$		33.3		$\mu\text{A}$
$I_{BSTO}$	BST to GND operating current	$f = 50\text{ kHz}$ , $C_{LOAD} = 0$		0.07		mA
<b>INPUT</b>						
$V_{HIT}$	Input voltage high threshold	$-40^\circ\text{C}$ to $125^\circ\text{C}$		1.45	2	V
$V_{LIT}$	Input voltage low threshold	$-40^\circ\text{C}$ to $125^\circ\text{C}$	0.8	1.35		V
$V_{IHYS}$	Input voltage hysteresis			0.15		V
$R_{INH}$	INH input pulldown resistance	$V_{INH} = 3\text{ V}$		200		k $\Omega$
$R_{INL}$	INL input pullup resistance	$V_{INL} = 0\text{ V}$		200		k $\Omega$
<b>UNDERVOLTAGE PROTECTION (UVLO)</b>						
$V_{GVDDR}$	GVDD rising threshold	$V_{GVDDR} = V_{GVDD} - GND$ , $-40^\circ\text{C}$ to $125^\circ\text{C}$		8.15	8.75	V
$V_{GVDDF}$	GVDD falling threshold	$V_{GVDDF} = V_{GVDD} - GND$ , $-40^\circ\text{C}$ to $125^\circ\text{C}$	6.75	7.7		V
$V_{GVDDHYS}$	GVDD threshold hysteresis			0.45		V
$V_{BSTR}$	VBST rising threshold	$V_{BSTR} = V_{BST} - V_{SH}$ , $-40^\circ\text{C}$ to $125^\circ\text{C}$		7.6	8.5	V
$V_{BSTF}$	VBST falling threshold	$V_{BSTF} = V_{BST} - V_{SH}$ , $-40^\circ\text{C}$ to $125^\circ\text{C}$	6.25	7.15		V
$V_{BSTHYS}$	VBST threshold hysteresis			0.45		V
<b>LO GATE DRIVER</b>						
$V_{GL\_L}$	Low level output voltage	$I_{GL} = 100\text{ mA}$ , $V_{GL\_L} = V_{GL} - GND$		0.25		V
$V_{GL\_H}$	High level output voltage	$I_{GL} = -100\text{ mA}$ , $V_{GL\_H} = V_{GVDD} - V_{GL}$		0.8		V
	Peak pullup current <sup>(1)</sup>	$V_{GL} = 0\text{ V}$		0.5		A
	Peak pulldown current <sup>(1)</sup>	$V_{GL} = 12\text{ V}$		0.8		A
<b>HO GATE DRIVER</b>						
$V_{GH\_L}$	Low level output voltage	$I_{GH} = 100\text{ mA}$ , $V_{GH\_L} = V_{GH} - V_{SH}$		0.25		V
$V_{GH\_H}$	High level output voltage	$I_{GH} = -100\text{ mA}$ , $V_{GH\_H} = V_{BST} - V_{GH}$		0.8		V
	Peak pullup current <sup>(1)</sup>	$V_{GH} = 0\text{ V}$		0.5		A
	Peak pulldown current <sup>(1)</sup>	$V_{GH} = 12\text{ V}$		0.8		A

(1) Parameter not tested in production.

## 6.6 Switching Characteristics

$V_{GVDD} = V_{BST} = 12\text{ V}$ ,  $GND = V_{SH} = 0\text{ V}$ , No Load on GL or GH,  $T_J = 25^\circ\text{C}$  (unless otherwise noted).

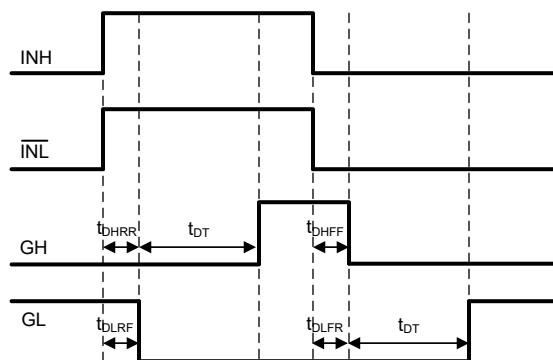
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>PROPAGATION DELAYS</b>						
$t_{DLRF}$	$V_{INL}$ rising to $V_{GL}$ falling	$V_{INL} = 0\text{ V}$ to $3\text{ V}$ , $C_{LOAD} = 0\text{ pF}$ . Time from 50% of the input to 90% of the output.		115		ns

## 6.6 Switching Characteristics (continued)

$V_{GVDD} = V_{BST} = 12\text{ V}$ ,  $GND = V_{SH} = 0\text{ V}$ , No Load on GL or GH,  $T_J = 25^\circ\text{C}$  (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{DHFF}$	$V_{INH}$ falling to $V_{GH}$ falling	$V_{INH} = 3\text{ V}$ to $0\text{ V}$ , $C_{LOAD} = 0\text{ pF}$ . Time from 50% of the input to 90% of the output.		115		ns
$t_{DLFR}$	$V_{INL}$ falling to $V_{GL}$ rising	$V_{INL} = 3\text{ V}$ to $0\text{ V}$ , $C_{LOAD} = 0\text{ pF}$ . Time from 50% of the input to 10% of the output.		115		ns
$t_{DHRR}$	$V_{INH}$ rising to $V_{GH}$ rising	$V_{INH} = 0\text{ V}$ to $3\text{ V}$ , $C_{LOAD} = 0\text{ pF}$ . Time from 50% of the input to 10% of the output.		115		ns
<b>DEADTIME</b>						
$t_{DT}$	Internal Deadtime			475		ns
<b>OUTPUT RISE AND FALL TIME</b>						
$t_{R\_GL}$	GL	$C_{LOAD} = 1000\text{ pF}$		28		ns
$t_{R\_GH}$	GH	$C_{LOAD} = 1000\text{ pF}$		28		ns
$t_{F\_GL}$	GL	$C_{LOAD} = 1000\text{ pF}$		18		ns
$t_{F\_GH}$	GH	$C_{LOAD} = 1000\text{ pF}$		18		ns

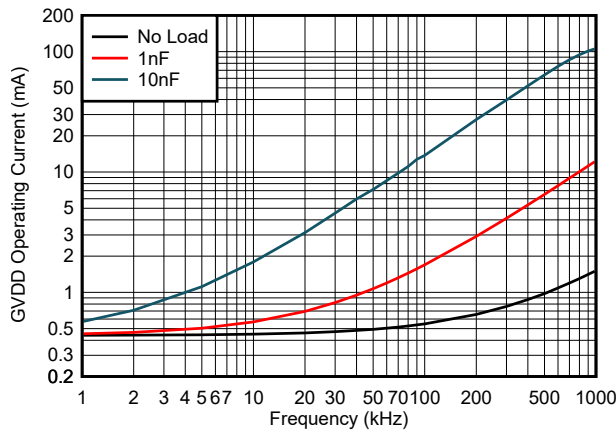
## 6.7 Timing Diagrams



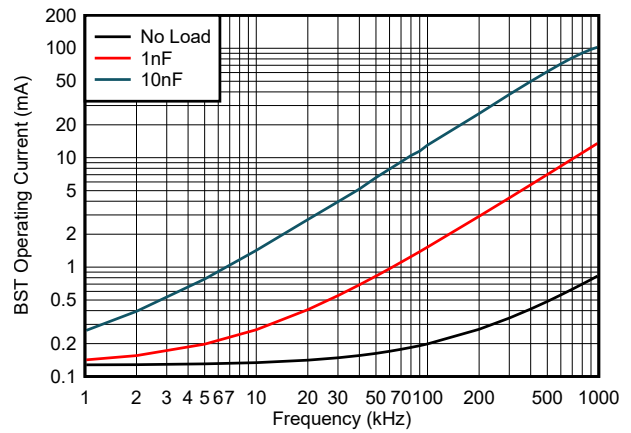
⊗ 6-1. Timing Definition Diagram

## 6.8 Typical Characteristics

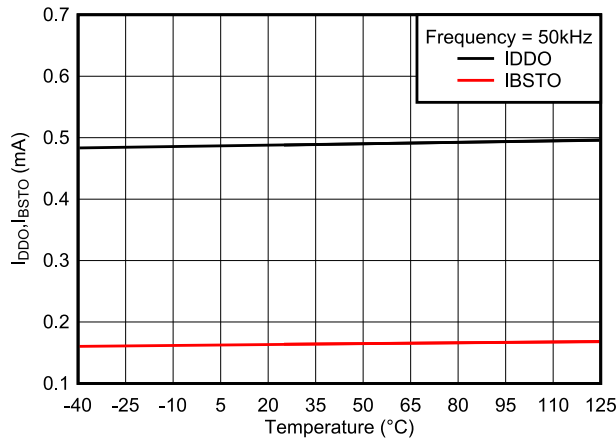
Unless otherwise specified,  $V_{GVDD} = V_{BST} = 12\text{ V}$ ,  $GND = V_{SH} = 0\text{ V}$ , No Load on GL or GH,  $T_J = 25^\circ\text{C}$ .



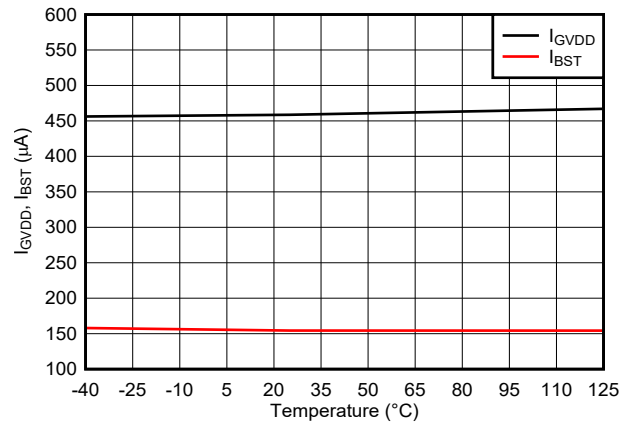
**6-2. GVDD Operating Current vs Frequency**



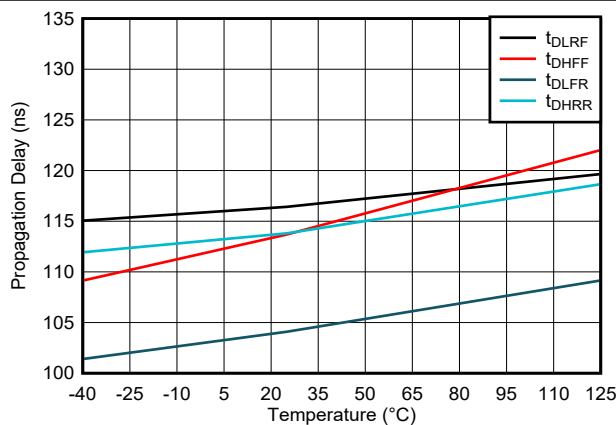
**6-3. BST Operating Current vs Frequency**



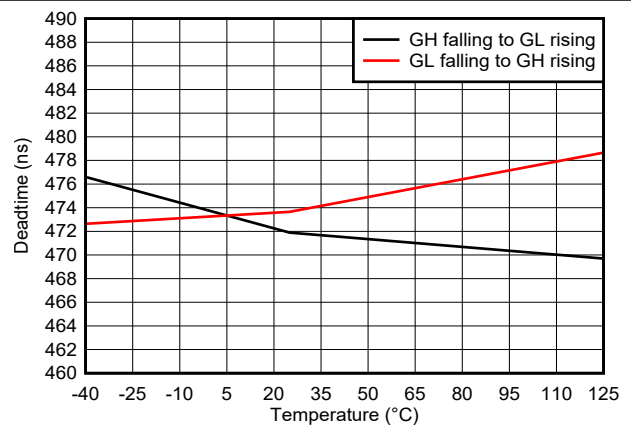
**6-4. Operating Currents vs Temperature**



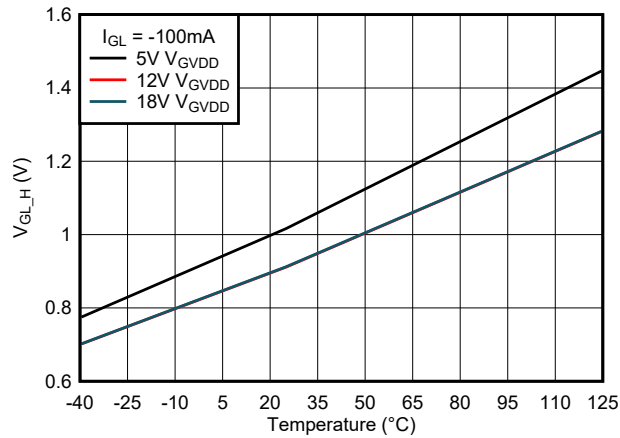
**6-5. Quiescent Currents vs Temperature**



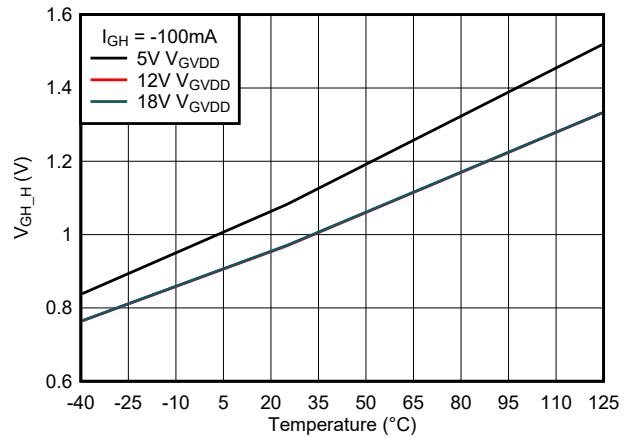
**6-6. Propagation Delays vs Temperature**



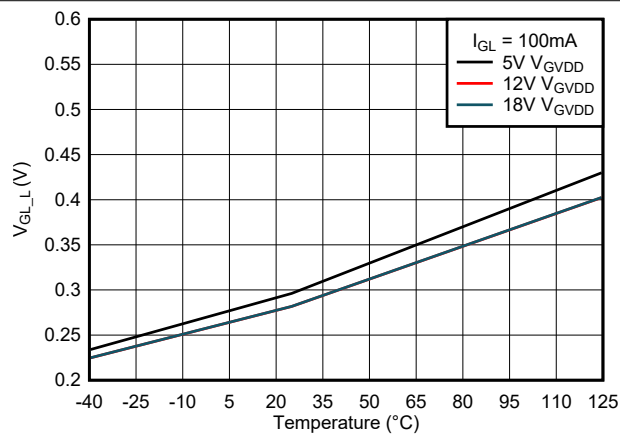
**6-7. Deadtime vs Temperature**



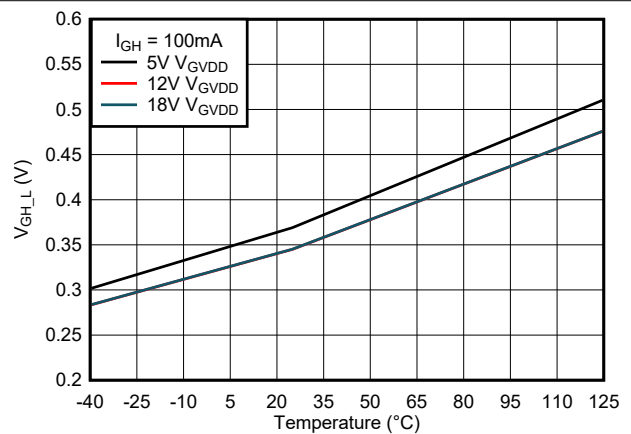
**6-8. GL Output High Voltage vs Temperature**



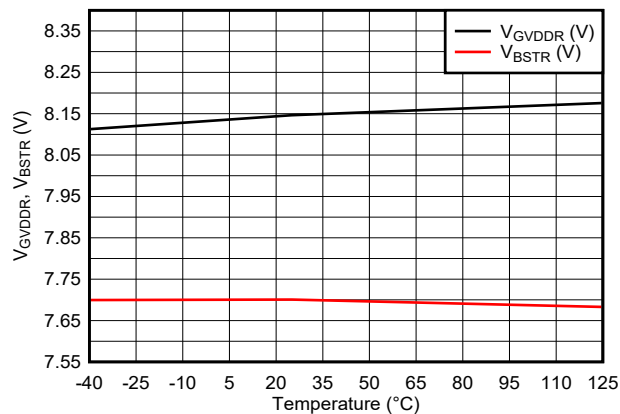
**6-9. GH Output High Voltage vs Temperature**



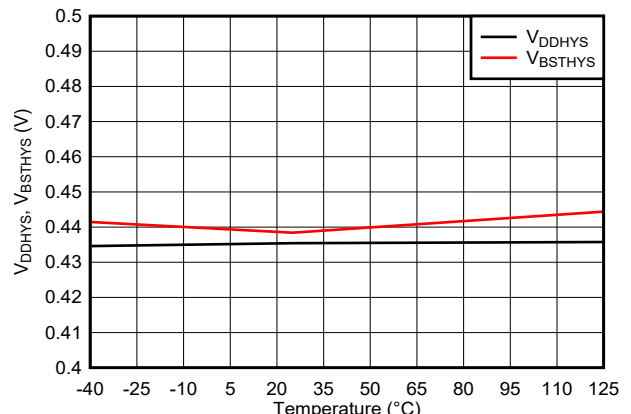
**6-10. GL Output Low Voltage vs Temperature**



**6-11. GH Output Low Voltage vs Temperature**

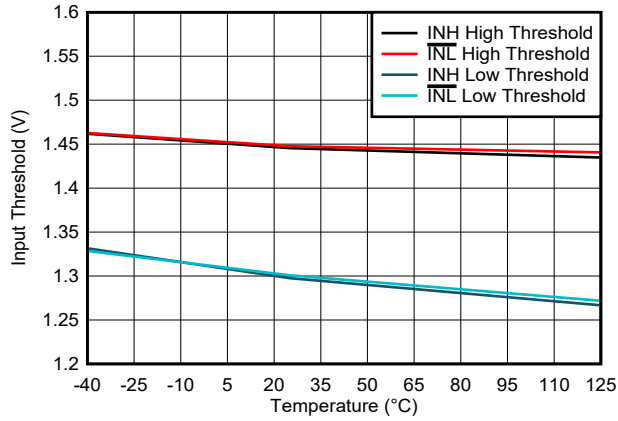


**6-12. GVDD and BST UVLO Thresholds vs Temperature**

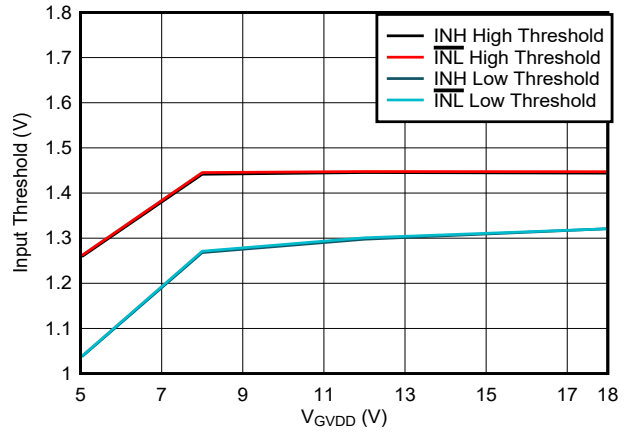


**6-13. GVDD and BST UVLO Hysteresis vs Temperature**






**6-14. Input Voltage Thresholds vs Temperature**



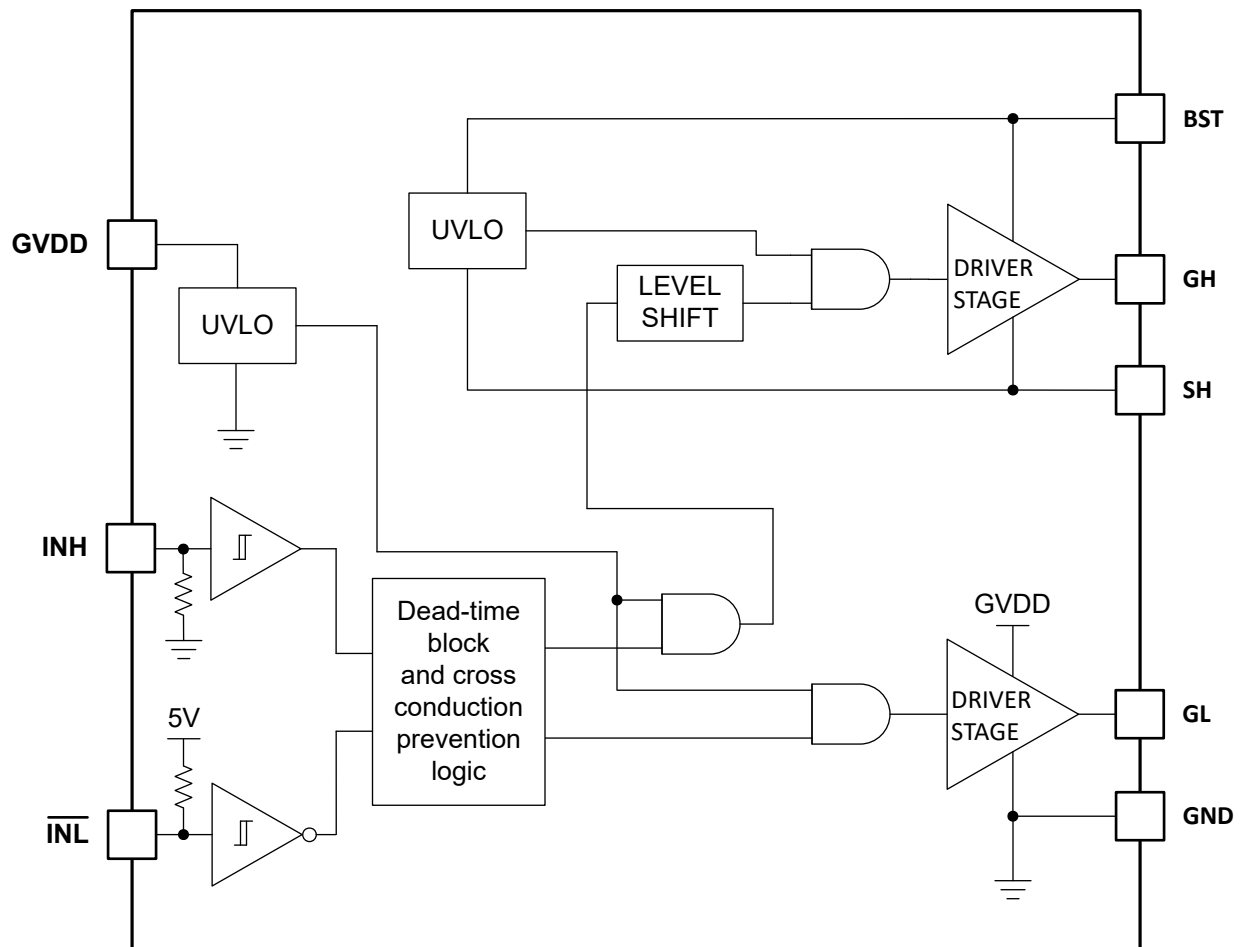

**6-15. Input Voltage Thresholds vs Supply Voltage**

## 7 Detailed Description

### 7.1 Overview

The LM2103 is a high-voltage gate driver designed to drive both the high-side and the low-side N-channel FETs in a synchronous buck or a half-bridge configuration. The two outputs are independently controlled with two TTL-compatible input signals, with an exception to prevent cross conduction when  $INH$  is high and  $\overline{INL}$  is low at the same time. The device can also work with CMOS type control signals at its inputs as long as the signals meet the turn-on and turn-off threshold specifications of the LM2103. The floating high-side driver is capable of working with a recommended BST voltage up to 105 V. A robust level shifter operates at high speed while consuming low power and providing clean level transitions from the control logic to the high-side gate driver. Undervoltage lockout (UVLO) is provided on both the low-side and the high-side power rails.

### 7.2 Functional Block Diagram



### 7.3 Feature Description

#### 7.3.1 Start-Up and UVLO

Both the high-side and the low-side driver stages include UVLO protection circuitry which monitors the supply voltage ( $V_{GVDD}$ ) and the bootstrap capacitor voltage ( $V_{BST-SH}$ ). The UVLO circuit inhibits each output until sufficient supply voltage is available to turn on the external MOSFETs, and the built-in UVLO hysteresis prevents chattering during supply voltage variations. When the supply voltage is applied to the  $GVDD$  pin of the device, both outputs are held low until  $V_{GVDD}$  exceeds the UVLO threshold, typically 8 V. Any UVLO condition on the bootstrap capacitor ( $V_{BST-SH}$ ) disables only the high-side output (GH).

表 7-1. GVDD UVLO Logic Operation

CONDITION ( $V_{BST-SH} > V_{BSTR}$ )	INH	$\overline{INL}$	GH	GL
$V_{GVDD} - GND < V_{GVDDR}$ during device start-up	H	L	L	L
	L	H	L	L
	H	H	L	L
	L	L	L	L
$V_{GVDD} - GND < V_{GVDDR} - V_{DDHYS}$ after device start-up	H	L	L	L
	L	H	L	L
	H	H	L	L
	L	L	L	L

表 7-2. BST UVLO Logic Operation

CONDITION ( $V_{GVDD} > V_{GVDDR}$ )	INH	$\overline{INL}$	GH	GL
$V_{BST-SH} < V_{BSTR}$ during device start-up	H	L	L	H
	L	H	L	L
	H	H	L	L
	L	L	L	H
$V_{BST-SH} < V_{BSTR} - V_{BSTHYS}$ after device start-up	H	L	L	H
	L	H	L	L
	H	H	L	L
	L	L	L	H

### 7.3.2 Input Stages

The  $\overline{INL}$  and INH inputs operate independent of each other, with an exception to prevent cross conduction when INH is high and  $\overline{INL}$  is low at the same time. Under such condition, the device turns OFF both the high-side and the low-side outputs to prevent shoot-through. The device has built-in fixed dead time with a typical value of 475 ns. A small filter at each of the inputs of the driver further improves system robustness in noise-prone applications. The INH input has an internal pulldown resistor and the  $\overline{INL}$  input has an internal pullup resistor both with typical value of 200 k $\Omega$ . Thus, when the inputs are floating, the outputs are held low.

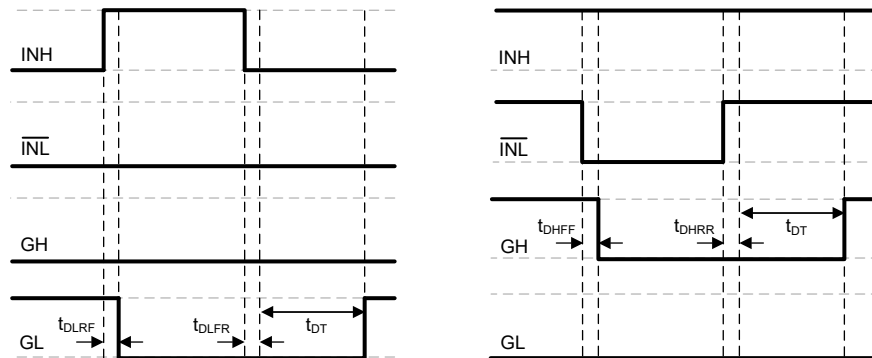


图 7-1. Cross Conduction Prevention and Deadtime Insertion

### 7.3.3 Level Shift

The level shift circuit is the interface from the high-side input, which is a GND referenced signal, to the high-side driver stage, which is referenced to the switch node (SH). The level shift allows control of the GH output which is referenced to the SH pin and provides excellent delay matching with the low-side driver.

### 7.3.4 Output Stages

The output stages are the interface to the power MOSFETs in the power train. High slew rate, low resistance, and high peak current capability of both outputs allow for efficient switching of the power MOSFETs. The low-side output stage is referenced to GND and the high-side is referenced to SH.

### 7.3.5 SH Transient Voltages Below Ground

In most applications, the body diode of the external low-side power MOSFET clamps the SH node to ground. In some situations, board capacitance and inductance can cause the SH node to transiently swing several volts below ground, before the body diode of the external low-side MOSFET clamps this swing. The SH pin in the LM2103 is allowed to swing below ground as long as specifications are not violated and conditions mentioned in this section are followed.

SH must always be at a lower potential than GH. Pulling GH more negative than specified conditions can activate parasitic transistors which may result in excessive current flow from the BST supply. This may result in damage to the device. The same relationship is true with GL and GND. If necessary, a Schottky diode can be placed externally between GH and SH or GL and GND to protect the device from this type of transient. The diode must be placed as close to the device pins as possible in order to be effective.

Low ESR bypass capacitors from BST to SH and from GVDD to GND are essential for proper operation of the gate driver device. The capacitor should be located at the leads of the device to minimize series inductance. The peak currents from GL and GH can be quite large. Any series inductance with the bypass capacitor causes voltage ringing at the leads of the device which must be avoided for reliable operation.

## 7.4 Device Functional Modes

The device operates in normal mode and UVLO mode. See [セクション 7.3.1](#) for more information on UVLO operation mode. In normal mode, when the  $V_{GVDD}$  and  $V_{BST-SH}$  are above UVLO threshold, the output stage is dependent on the states of the INH and INL pins. The outputs GH and GL will be low if input state is floating.

**表 7-3. Input/Output Logic in Normal Mode of Operation**

INH	INL	GH <sup>(1)</sup>	GL <sup>(2)</sup>
L	L	L	H
L	H	L	L
H	L	L	L
H	H	H	L
Floating	Floating	L	L

(1) GH is measured with respect to SH.

(2) GL is measured with respect to GND.

## 8 Application and Implementation

### 注

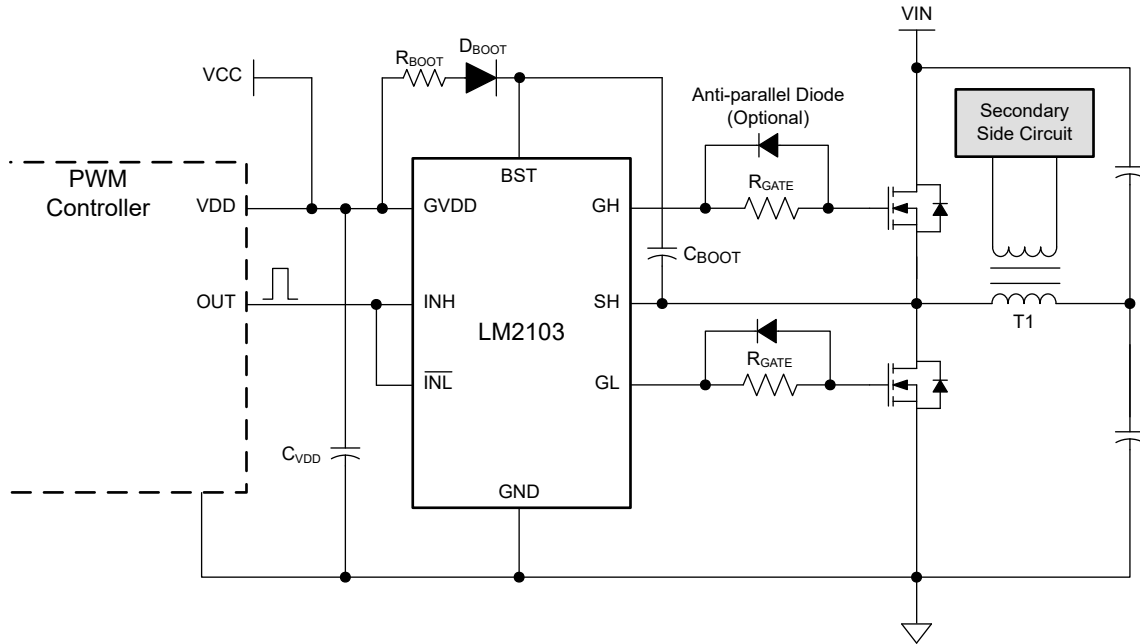
Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 8.1 Application Information

To operate power MOSFETs at high switching frequencies and to reduce associated switching losses, a powerful gate driver is employed between the PWM output of controller and the gates of the power semiconductor devices. Also, gate drivers are indispensable when it is impossible for the PWM controller to directly drive the gates of the switching devices. With the advent of digital power, this situation is often encountered because the PWM signal from the digital controller is often a 3.3-V logic signal which cannot effectively turn on a power switch. Level-shift circuitry is needed to boost the 3.3-V signal to the gate-drive voltage (such as 12 V) to

fully turn on the power device and minimize conduction losses. Traditional buffer drive circuits based on NPN and PNP bipolar transistors in totem-pole arrangement prove inadequate with digital power because they lack level-shifting capability. Gate drivers effectively combine both the level-shifting and buffer-drive functions. Gate drivers can also minimize the effect of high-frequency switching noise by being placed physically close to the power switch. Additionally, gate drivers can drive gate-drive transformers and control floating power-device gates, reducing the controller's power dissipation and thermal stress by moving the gate-charge power losses into the driver.

## 8.2 Typical Application



8-1. LM2103 Driving MOSFETs in a Half-Bridge Converter

## 8.2.1 Design Requirements

表 8-1 lists the design parameters of the LM2103.

表 8-1. Design Example

PARAMETER	VALUE
Gate Driver	LM2103
MOSFET	CSD19534KCS
$V_{DD}$	12 V
$Q_G$	17 nC
$f_{sw}$	50 kHz

## 8.2.2 Detailed Design Procedure

### 8.2.2.1 Select External Bootstrap Diode and Its Series Resistor

An external bootstrap diode between GVDD pin and BST pin is required to allow the bootstrap capacitor to be charged from GVDD pin every cycle when the low-side MOSFET turns on. The charging of the capacitor involves high-peak currents, and therefore, transient power dissipation in the bootstrap diode may be significant. The reverse recovery time of the bootstrap diode must be very small to achieve a reduction in reverse recovery losses. Both the diode conduction losses and reverse recovery losses contribute to the total losses in the gate driver and must be considered in calculation the gate driver's power dissipation.

In order to minimize losses associated with the reverse recovery properties of the diode and ground noise bouncing, a fast recovery diode or Schottky diode with low forward voltage drop and low junction capacitance is recommended. Using Schottky diodes reduce the risk associated with charge supplied back to the gate driver supply from the bootstrap capacitor and minimize leakage current. When the SH pin (switch node) is pulled to a higher voltage, the diode must be able reverse bias fast enough to block any charges from the bootstrap capacitor to the GVDD supply. This bootstrap diode should be carefully chosen such that it is capable of handling the peak transient currents during start-up, and such that its voltage rating is higher than the system DC-link voltage with enough margins.

A bootstrap resistor  $R_{BOOT}$  in series with the bootstrap diode is recommended to reduce the inrush current in  $D_{BOOT}$  and limit the ramp up slew rate of voltage of  $V_{BST-SH}$  during each switching cycle, especially when the SH pin has excessive negative transient voltage.  $R_{BOOT}$  recommended value is between 2  $\Omega$  and 10  $\Omega$  depending on diode selection. A current limiting resistor of 2.2  $\Omega$  is selected to limit inrush current of bootstrap diode, and the estimated peak current on the  $D_{BOOT}$  is shown in 式 1.

$$I_{Dboot(pk)} = \frac{V_{GVDD} - V_{DH}}{R_{BOOT}} = \frac{12V - 1V}{2.2\Omega} = 5A \quad (1)$$

where

- $V_{DH}$  is the bootstrap diode forward voltage drop

### 8.2.2.2 Select Bootstrap and GVDD Capacitor

The bootstrap capacitor must maintain the  $V_{BST-SH}$  voltage above the UVLO threshold for normal operation. Calculate the maximum allowable drop across the bootstrap capacitor with 式 2.

$$\Delta V_{BST} = V_{GVDD} - V_{DH} - V_{BSTL} = 12V - 1V - 7.75V = 3.25V \quad (2)$$

where

- $V_{GVDD}$  = Supply voltage of the gate drive IC
- $V_{DH}$  = Bootstrap diode forward voltage drop
- $V_{BSTL}$  = BST falling threshold ( $V_{BSTR(max)} - V_{BSTHYS}$ )

Then, the total charge needed per switching cycle is estimated by 式 3.

$$Q_{TOTAL} = Q_G + I_{BSTS} \times \frac{D_{MAX}}{f_{SW}} + \frac{I_{BST}}{f_{SW}} = 17\text{nC} + 33.3\mu\text{A} \times \frac{0.95}{50\text{kHz}} + \frac{150\mu\text{A}}{50\text{kHz}} = 20\text{nC} \quad (3)$$

where

- $Q_G$  = Total MOSFET gate charge
- $I_{BSTS}$  = BST to VSS leakage current
- $D_{Max}$  = Converter maximum duty cycle
- $I_{BST}$  = BST quiescent current

Next, use 式 4 to estimate the minimum bootstrap capacitor value.

$$C_{BOOT}(\text{MIN}) = \frac{Q_{TOTAL}}{\Delta V_{BST}} = \frac{20\text{nC}}{3.25\text{V}} = 6.2\text{nF} \quad (4)$$

In practice, the value of the  $C_{BOOT}$  capacitor must be greater than calculated to allow for situations where the power stage may skip pulse due to load transients. 式 5 can be used to estimate the recommended bootstrap capacitance based on the maximum bootstrap voltage ripple desired for a specific application.

$$C_{BOOT} > \frac{Q_{TOTAL}}{\Delta V_{BST\_RIPPLE}} \quad (5)$$

where

- $\Delta V_{BST\_RIPPLE}$  = Maximum allowable voltage drop across the bypass capacitor based on system requirements
- TI recommends having enough margins and to place the bootstrap capacitor as close to the BST and SH pins as possible.

$$C_{BOOT} = 100\text{ nF} \quad (6)$$

As a general rule, the local  $V_{GVDD}$  bypass capacitor must be 10 times greater than the value of  $C_{BOOT}$ , as shown in 式 7.

$$C_{GVDD} = 1\ \mu\text{F} \quad (7)$$

The bootstrap and bias capacitors must be ceramic types with X7R dielectric. The voltage rating must be twice that of the maximum  $V_{GVDD}$  considering capacitance tolerances once the devices have a DC bias voltage across them and to ensure long-term reliability.

### 8.2.2.3 Select External Gate Driver Resistor

The external gate driver resistor,  $R_{GATE}$ , is sized to reduce ringing caused by parasitic inductances and capacitances and also to limit the current coming out of the gate driver.

The peak GH pullup current is calculated in 式 8.

$$I_{GHH} = \frac{V_{GVDD} - V_{DH}}{R_{GHH} + R_{GATE} + R_{GFET\_INT}} \quad (8)$$

where

- $I_{GHH}$  = GH Peak pullup current
- $V_{DH}$  = Bootstrap diode forward voltage drop
- $R_{GHH}$  = Gate driver internal GH pullup resistance, estimated from the testing conditions, that is  $R_{GHH} = \frac{V_{GH\_H}}{I_{GH}}$
- $R_{GATE}$  = External gate drive resistance
- $R_{GFET\_INT}$  = MOSFET internal gate resistance, provided by transistor data sheet

Similarly, the peak GH pulldown current is shown in 式 9.

$$I_{GHL} = \frac{V_{GVDD} - V_{DH}}{R_{GHL} + R_{GATE} + R_{GFET\_INT}} \quad (9)$$

where

- $R_{GHL}$  is the GH pulldown resistance

The peak GL pullup current is shown in 式 10.

$$I_{GLH} = \frac{V_{GVDD}}{R_{GLH} + R_{GATE} + R_{GFET\_INT}} \quad (10)$$

where

- $R_{GLH}$  is the GL pullup resistance

The peak GL pulldown current is shown in 式 11.

$$I_{GLL} = \frac{V_{GVDD}}{R_{GLL} + R_{GATE} + R_{GFET\_INT}} \quad (11)$$

where

- $R_{GLL}$  is the GL pulldown resistance

For some scenarios, if the applications require fast turnoff, an anti-paralleled diode on  $R_{Gate}$  could be used to bypass the external gate drive resistor and speed up turnoff transition.

#### 8.2.2.4 Estimate the Driver Power Loss

The total driver IC power dissipation can be estimated through the following components.

1. Static power losses,  $P_{QC}$ , due to quiescent currents  $I_{GVDD}$  and  $I_{BST}$  is shown in 式 12.

$$P_{QC} = V_{GVDD} \times I_{GVDD} + (V_{GVDD} - V_F) \times I_{BST} = 12V \times 0.43mA + (12V - 1V) \times 0.15mA = 6.8mW \quad (12)$$

2. Level-shifter losses,  $P_{IBSTS}$ , due high-side leakage current  $I_{BSTS}$  is shown in 式 13.

$$P_{IBSTS} = V_{BST} \times I_{BSTS} \times D = 72V \times 0.033mA \times 0.95 = 2.26mW \quad (13)$$

where

- $D$  is the high-side switch duty cycle

3. Dynamic losses,  $P_{QG1\&2}$ , due to the FETs gate charge  $Q_G$  as shown in 式 14.

$$P_{QG1\&2} = 2 \times V_{GVDD} \times Q_G \times f_{SW} \times \frac{R_{GD\_R}}{R_{GD\_R} + R_{GATE} + R_{GFET\_INT}} = 2 \times 12V \times 17nC \times 50kHz \times \frac{5.25\Omega}{5.25\Omega + 4.7\Omega + 2.2\Omega} = 8.8mW \quad (14)$$

where

- $Q_G$  = Total FETs gate charge
- $f_{SW}$  = Switching frequency
- $R_{GD\_R}$  = Average value of pullup and pulldown resistor
- $R_{GATE}$  = External gate drive resistor
- $R_{GFET\_INT}$  = Internal FETs gate resistor

4. Level-shifter dynamic losses,  $P_{LS}$ , during high-side switching due to required level-shifter charge on each switching cycle. For this example it is assumed that value of parasitic charge  $Q_P$  is 2.5 nC, as shown in 式 15.

$$P_{LS} = V_{BST} \times Q_P \times f_{SW} = 72V \times 2.5nC \times 50kHz = 9mW \quad (15)$$



In this example, the sum of all the losses is 27 mW as a total gate driver loss. For gate drivers that include bootstrap diode, one should also estimate losses in the bootstrap diode. Diode forward conduction loss is computed as product of average forward voltage drop and average forward current.

式 16 estimates the maximum allowable power loss of the device for a given ambient temperature.

$$P_{\text{MAX}} = \frac{T_J - T_A}{R_{\theta JA}} \quad (16)$$

where

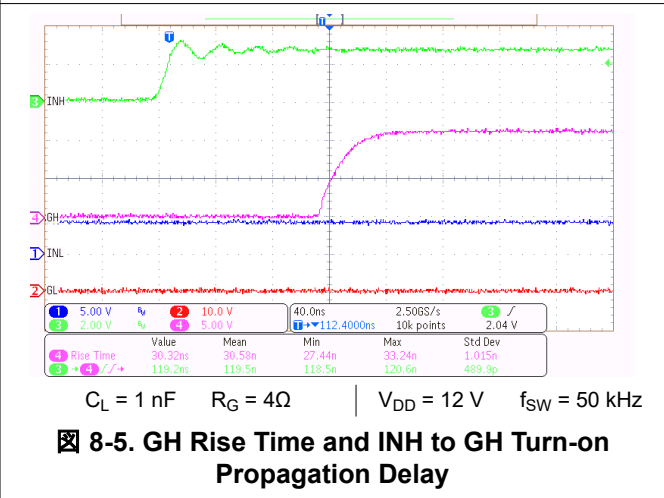
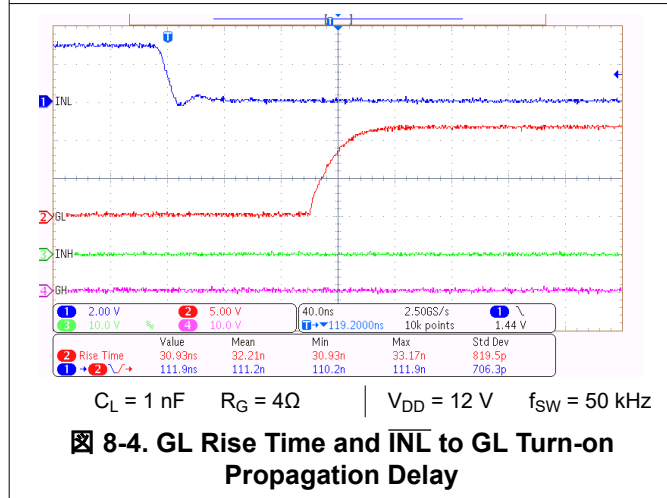
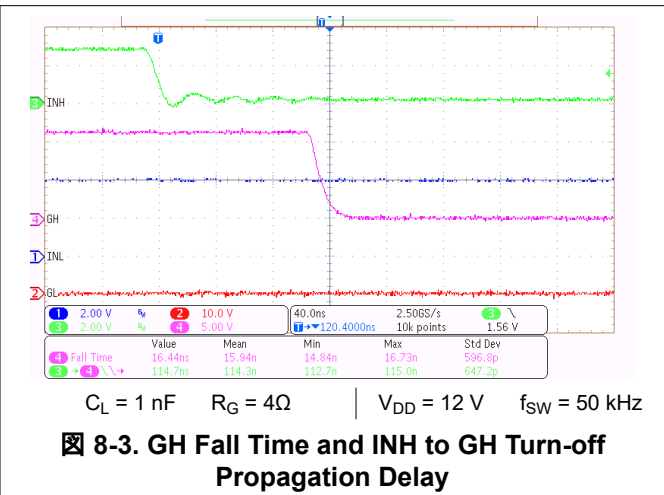
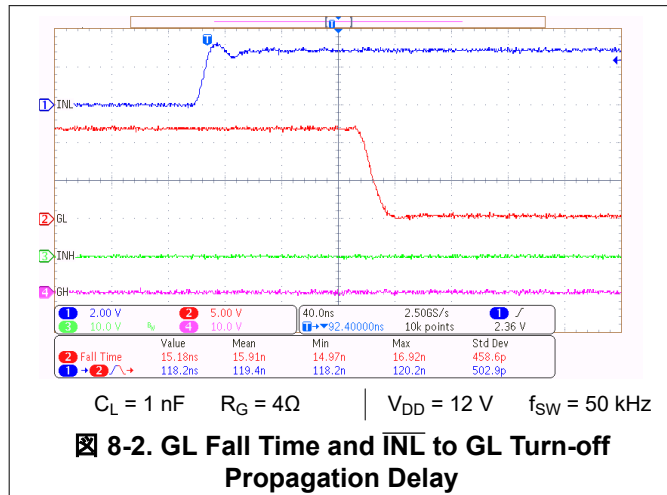
- $P_{\text{MAX}}$  = Maximum allowed power dissipation in the gate driver device
- $T_J$  = Junction temperature
- $T_A$  = Ambient temperature
- $R_{\theta JA}$  = Junction-to-ambient thermal resistance

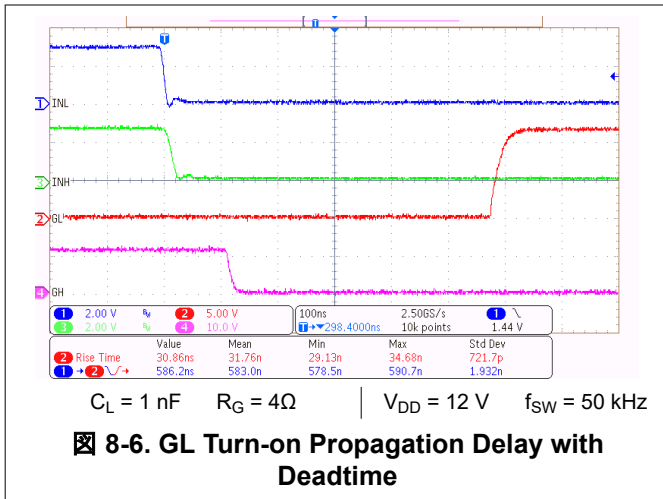
The thermal metrics for the driver package is summarized in the *Thermal Information* table of the data sheet. For detailed information regarding the thermal information table, refer to the Texas Instruments application note entitled [Semiconductor and IC Package Thermal Metrics](#).

### 8.2.3 Application Curves

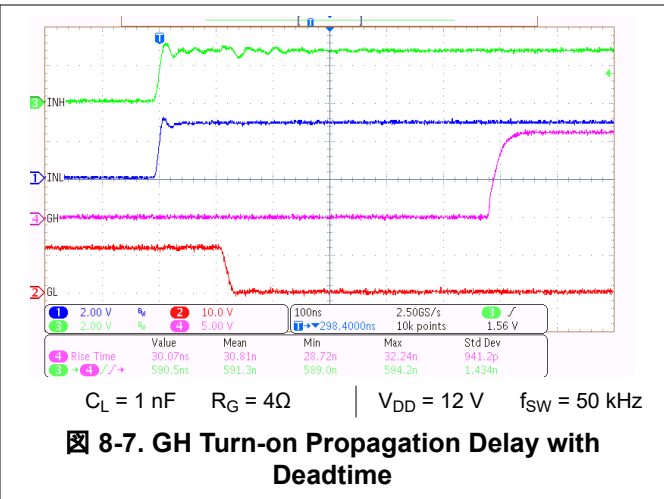
Figure 8-2 and Figure 8-3 show the fall times and turn-off propagation delays for the low side driver and the high side driver respectively. Likewise, Figure 8-4 and Figure 8-5 show the fall times and turn-off propagation delays, and Figure 8-6 and Figure 8-7 show the propagation delays with deadtime. Each channel (INH, INL, GH, and GL) is labeled and displayed on the left hand of the waveforms.

The testing condition: load capacitance is 1 nF, gate resistor is 4Ω,  $V_{DD} = 12\text{ V}$ ,  $f_{SW} = 50\text{ kHz}$ .





8-6. GL Turn-on Propagation Delay with Deadtime



8-7. GH Turn-on Propagation Delay with Deadtime

## 9 Power Supply Recommendations

The recommended bias supply voltage range for LM2103 is from 9 V to 18 V. The lower end of this range is governed by the internal undervoltage lockout (UVLO) protection feature of the  $V_{GVDD}$  supply circuit blocks. The upper end of this range is driven by the 18-V recommended maximum voltage rating of the GVDD pin. It is recommended that the voltage on GVDD pin is lower than the maximum recommended voltage to account for transient voltage spikes.

The UVLO protection feature also involves a hysteresis function. This means that once the device is operating in normal mode, if the  $V_{GVDD}$  voltage drops, the device continues to operate in normal mode as long as the voltage drop does not exceed the hysteresis specification,  $V_{DDHYS}$ . If the voltage drop is more than hysteresis specification, the device shuts down. Therefore, while operating at or near the 8-V range, the voltage ripple on the auxiliary power supply output must be smaller than the hysteresis specification of LM2103 to avoid triggering device-shutdown.

A local bypass capacitor must be placed between the GVDD and GND pins and this capacitor must be located as close to the device as possible. A low-ESR, ceramic surface mount capacitor is recommended. TI recommends using 2 capacitors across GVDD and GND: a low capacitance ceramic surface-mount capacitor for high-frequency filtering placed very close to GVDD and GND pins, and another high capacitance value surface-mount capacitor for IC bias requirements. In a similar manner, the current pulses delivered by the GH pin are sourced from the BST pin. Therefore, a local decoupling capacitor is recommended between the BST and SH pins.

## 10 Layout

### 10.1 Layout Guidelines

Optimum performance of half-bridge gate drivers cannot be achieved without taking due considerations during circuit board layout. The following points are emphasized:

1. Low-ESR and low-ESL capacitors must be connected close to the IC between GVDD and GND pins and between BST and SH pins to support high peak currents being drawn from GVDD and BST during the turn-on of the external MOSFETs.
2. To prevent large voltage transients at the drain of the top MOSFET, a low-ESR electrolytic capacitor and a good-quality ceramic capacitor must be connected between the MOSFET drain and ground (GND).
3. To avoid large negative transients on the switch node (SH) pin, the parasitic inductances between the source of the top MOSFET and the drain of the bottom MOSFET (synchronous rectifier) must be minimized.
4. Grounding considerations:
  - The first priority in designing grounding connections is to confine the high peak currents that charge and discharge the MOSFET gates to a minimal physical area. This will decrease the loop inductance and minimize noise issues on the gate terminals of the MOSFETs. The gate driver must be placed as close as possible to the MOSFETs.
  - The second consideration is the high current path that includes the bootstrap capacitor, the bootstrap diode, the local ground referenced bypass capacitor, and the low-side MOSFET body diode. The bootstrap capacitor is recharged on a cycle-by-cycle basis through the bootstrap diode from the ground referenced GVDD bypass capacitor. The recharging occurs in a short time interval and involves high peak current. Minimizing this loop length and area on the circuit board is important to ensure reliable operation.

## 10.2 Layout Example

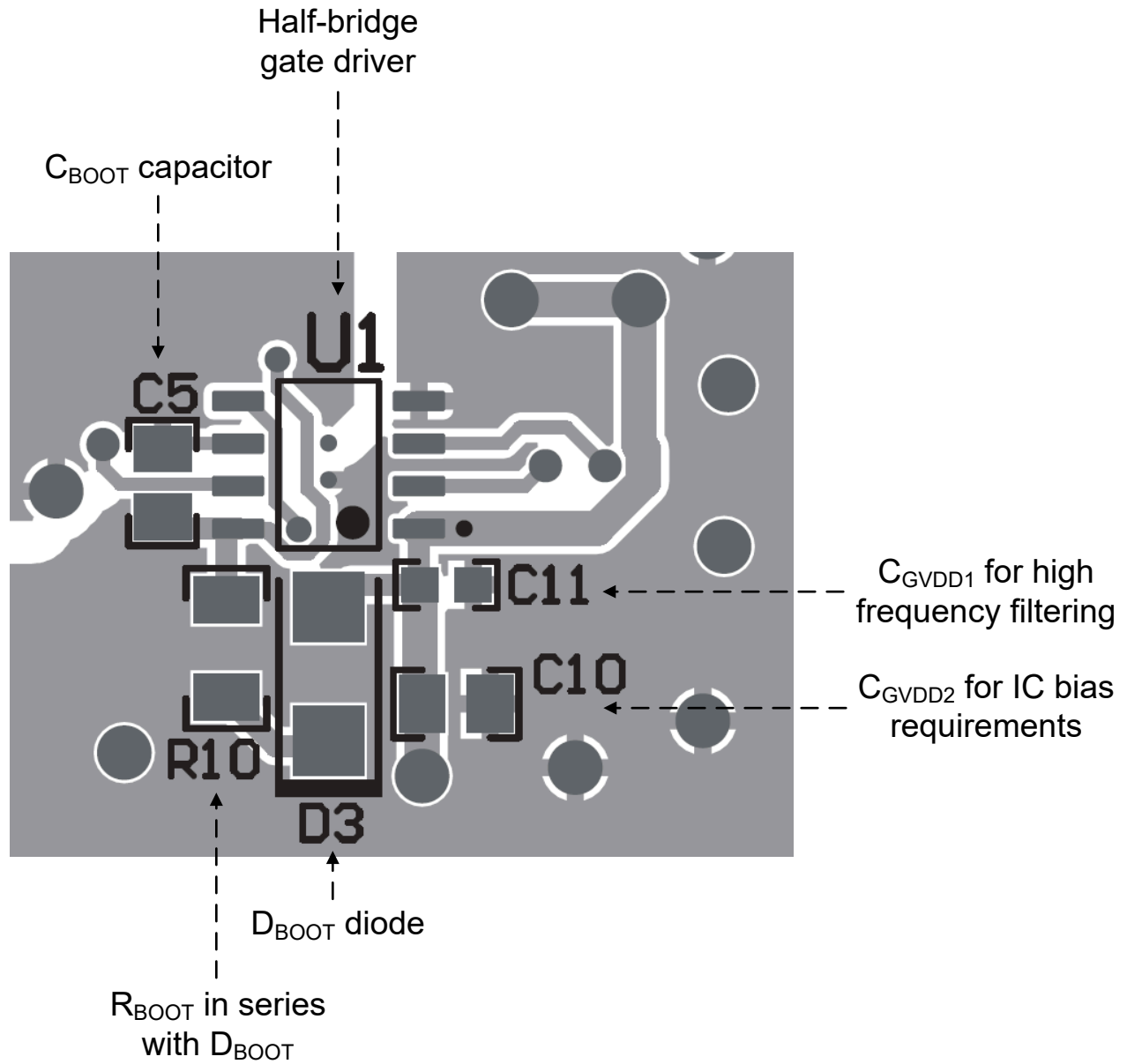


图 10-1. Layout Example

## 11 Device and Documentation Support

### 11.1 Device Support

#### 11.1.1 サード・パーティ製品に関する免責事項

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### 11.2 Documentation Support

#### 11.2.1 Related Documentation

For related documentation see the following:

- *Semiconductor and IC Packaging Thermal Metrics*, [SPRA953](#)

### 11.3 ドキュメントの更新通知を受け取る方法

ドキュメントの更新についての通知を受け取るには、[ti.com](#) のデバイス製品フォルダを開いてください。「更新の通知を受け取る」をクリックして登録すると、変更されたすべての製品情報に関するダイジェストを毎週受け取れます。変更の詳細については、修正されたドキュメントに含まれている改訂履歴をご覧ください。

### 11.4 サポート・リソース

[TI E2E™ サポート・フォーラム](#) は、エンジニアが検証済みの回答と設計に関するヒントをエキスパートから迅速かつ直接得ることができる場所です。既存の回答を検索したり、独自の質問をしたりすることで、設計に必要な支援を迅速に得ることができます。

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ESD による破損は、わずかな性能低下からデバイスの完全な故障まで多岐にわたります。精密な IC の場合、パラメータがわずかに変化するだけで公表されている仕様から外れる可能性があるため、破損が発生しやすくなっています。

### 11.7 用語集

[テキサス・インスツルメンツ用語集](#) この用語集には、用語や略語の一覧および定義が記載されています。

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LM2103DR	ACTIVE	SOIC	D	8	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	L2103D	Samples

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM2103DR	SOIC	D	8	3000	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1



**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM2103DR	SOIC	D	8	3000	356.0	356.0	35.0



D0008A

# PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



4214825/C 02/2019

NOTES:

- Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- This drawing is subject to change without notice.
- This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed  $.006$  [0.15] per side.
- This dimension does not include interlead flash.
- Reference JEDEC registration MS-012, variation AA.

# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
 EXPOSED METAL SHOWN  
 SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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