

# OPAx188-Q1高精度、低ノイズ、レール・ツー・レール出力、36V、ゼロドリフト、車載用グレード・オペアンプ

## 1 特長

- 車載アプリケーションに対応
- 下記内容でAEC-Q100認定済み：
  - OPA188-Q1デバイス温度グレード1: -40°C~+125°C
  - OPA2188-Q1デバイス温度グレード2: -40°C~+105°C
  - デバイスHBM ESD分類レベル1C
  - デバイスCDM ESD分類レベルC5
- 広い電源電圧範囲:  $\pm 2V \sim \pm 18V$
- 低いオフセット電圧: 25 $\mu V$  (最大値)
- ゼロドリフト: 0.03 $\mu V/^\circ C$
- 低ノイズ: 8.8nV/ $\sqrt{Hz}$ 
  - 0.1Hz~10Hzのノイズ: 0.25 $\mu V_{pp}$
- 非常に優れたDC精度
  - PSRR: 142dB
  - CMRR: 146dB
  - オープンループ・ゲイン: 136dB
- ゲイン帯域幅: 2MHz
- 静止電流: 510 $\mu A$  (最大値)
- 広い電源電圧範囲:  $\pm 2V \sim \pm 18V$
- レール・ツー・レール出力
- 入力に負のレールも含む
- RFIフィルタ付きの入力

## 2 アプリケーション

- HEV/EVのパワートレイン
  - DC/DCコンバータ
  - トラクション・インバータ
- 高精度の安全性とセンシング: (ブレーキ、位置、乗客の在席の検出)
- 高精度の監督と監視

## 3 概要

OPAx188-Q1オペアンプ・ファミリーは、TI独自のゼロ・ドリフト技術により、低いオフセット電圧(最大値25 $\mu V$ )と、時間や温度に対してほぼゼロのドリフト係数を実現しています。この小型で高精度、低静止電流のアンプ・ファミリーは入力インピーダンスが高く、レールから15mV以内のレール・ツー・レール出力を提供します。入力同相範囲には、負のレールも含まれます。4V~36V ( $\pm 2V \sim \pm 18V$ )の単電源またはデュアル電源を使用できます。

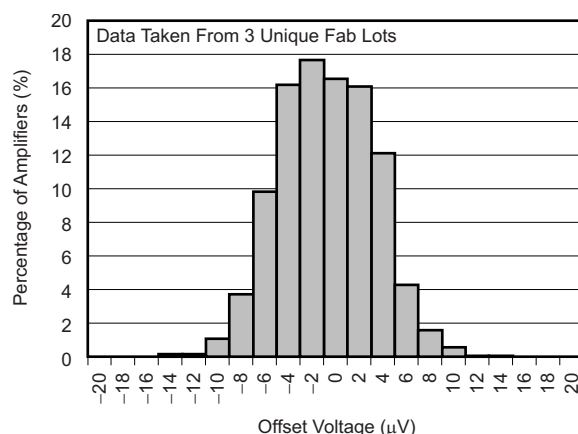
OPA188-Q1とOPA2188-Q1は、いずれもVSSOP-8で供給されます。単一チャンネル・バージョン(OPA188-Q1)は-40°C~+125°C、デュアル・チャンネル・バージョン(OPA2188-Q1)は-40°C~+105°Cで完全に動作が規定されています。

### 製品情報(1)

型番	パッケージ	本体サイズ(typ)
OPA188-Q1	VSSOP (8)	3.00mmx3.00mm
OPA2188-Q1		

(1) 利用可能なすべてのパッケージについては、このデータシートの末尾にあるパッケージ・オプションについての付録を参照してください。

### オフセット電圧の製造分布



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## 4 改訂履歴

日付	改訂内容	注
2017年4月	*	初版

## 5 Device Comparison Table

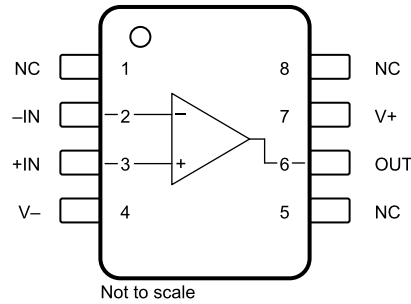
### 5.1 Portfolio Comparison

#### Zero-Drift Amplifier Portfolio

VERSION	PRODUCT	OFFSET VOLTAGE ( $\mu\text{V}$ , maximum)	OFFSET VOLTAGE DRIFT ( $\mu\text{V}/^\circ\text{C}$ , maximum)	BANDWIDTH (MHz)	INPUT VOLTAGE NOISE ( $\mu\text{V}_{\text{PP}}$ , $f = 0.1 \text{ Hz to } 10 \text{ Hz}$ )
Single	<a href="#">OPA188-Q1</a> (4 V to 36 V)	$\pm 25$	$\pm 0.085$	2	0.25
	<a href="#">OPA333</a> (5 V)	$\pm 10$	$\pm 0.05$	0.35	1.1
	<a href="#">OPA378</a> (5 V)	$\pm 50$	$\pm 0.25$	0.9	0.4
	<a href="#">OPA735</a> (12 V)	$\pm 5$	$\pm 0.05$	1.6	2.5
Dual	<a href="#">OPA2188-Q1</a> (4 V to 36 V)	$\pm 25$	$\pm 0.085$	2	0.25
	<a href="#">OPA2333</a> (5 V)	$\pm 10$	$\pm 0.05$	0.35	1.1
	<a href="#">OPA2378</a> (5 V)	$\pm 50$	$\pm 0.25$	0.9	0.4
	<a href="#">OPA2735</a> (12 V)	$\pm 5$	$\pm 0.05$	1.6	2.5
Quad	<a href="#">OPA4330</a> (5 V)	$\pm 50$	$\pm 0.25$	0.35	1.1

## 6 Pin Configuration and Functions

OPA188-Q1 DGK Package  
8-Pin VSSOP  
Top View

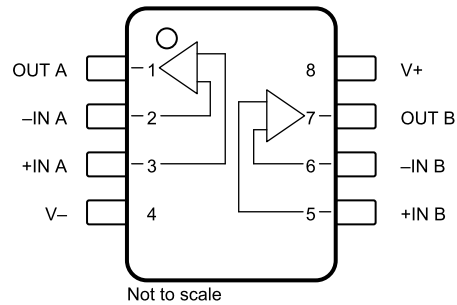


(1) NC = no connection.

### Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
+IN	3	I	Noninverting input
-IN	2	I	Inverting input
NC	1, 5, 8	—	No internal connection (can be left floating)
OUT	6	O	Output
V+	7	—	Positive (highest) power supply
V-	4	—	Negative (lowest) power supply

**OPA2188-Q1 DGK Package  
8-Pin VSSOP  
Top View**



**Pin Functions**

PIN		I/O	DESCRIPTION
NAME	NO.		
+IN A	3	I	Noninverting input, channel A
+IN B	5	I	Noninverting input, channel B
-IN A	2	I	Inverting input, channel A
-IN B	6	I	Inverting input, channel B
OUT A	1	O	Output, channel A
OUT B	7	O	Output, channel B
V+	8	—	Positive (highest) power supply
V-	4	—	Negative (lowest) power supply

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

			MIN	MAX	UNIT
Voltage	Supply	Split-supply	±20		V
		Single-supply	40		
	Signal input pins <sup>(2)</sup>		(V-) - 0.5	(V+) + 0.5	
		Differential	±0.7		
Current	Signal input pins <sup>(2)</sup>	±10		mA	
	Output short-circuit <sup>(3)</sup>	Continuous			
Temperature	OPA188-Q1, T <sub>J</sub>		150		°C
	OPA2188-Q1, T <sub>J</sub>		125		°C
	Storage, T <sub>stg</sub>		-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5 V beyond the supply rails should be current-limited to 10 mA or less.
- (3) Short-circuit to ground, V- or V+.

### 7.2 ESD Ratings

			VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±1500	V
		Charged-device model (CDM), per AEC Q100-011	±750	

- (1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted) R<sub>L</sub> = 10 kΩ connected to V<sub>S</sub> / 2<sup>(1)</sup>, and V<sub>CM</sub> = V<sub>OUT</sub> = V<sub>S</sub> / 2<sup>(1)</sup>

			MIN	NOM	MAX	UNIT
V <sub>S</sub>	Operating voltage range	Split-supply	±2		±18	V
		Single-supply	4		36	
T <sub>A</sub>	OPA188-Q1 Temperature Grade 1: Specified temperature range		-40		125	°C
	OPA2188-Q1 Temperature Grade 2: Specified temperature range		-40		105	

- (1) V<sub>S</sub> / 2 = midsupply.

### 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		OPA188-Q1	OPA2188-Q1	UNIT
		DGK (VSSOP)	DGK (VSSOP)	
		8 PINS	8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	171.7	163.2	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	62.7	57.4	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	93.0	83.4	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	9.0	6.6	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	91.4	82.0	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

## 7.5 Electrical Characteristics: High-Voltage Operation

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 4\text{ V}$  to  $\pm 18\text{ V}$  ( $V_S = 8\text{ V}$  to  $36\text{ V}$ ),  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  <sup>(1)</sup>, and  $V_{CM} = V_{OUT} = V_S / 2$  <sup>(1)</sup> (unless otherwise noted)

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{OS}$	Input offset voltage			$\pm 6$	$\pm 25$	$\mu\text{V}$
$dV_{IO}/dT$	Input offset voltage drift	OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 0.03$	$\pm 0.085$	$\mu\text{V}/^\circ\text{C}$
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$		$\pm 0.03$	$\pm 0.085$	$\mu\text{V}/^\circ\text{C}$
PSRR	Power-supply rejection ratio	OPA188-Q1 $V_S = 4\text{ V}$ to $36\text{ V}$ $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 0.075$	$\pm 0.3$	$\mu\text{V}/\text{V}$
		OPA2188-Q1 $V_S = 4\text{ V}$ to $36\text{ V}$ $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$		$\pm 0.075$	$\pm 0.3$	$\mu\text{V}/\text{V}$
	Long-term stability <sup>(2)</sup>			4		$\mu\text{V}$
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current	$V_{CM} = V_S / 2$		$\pm 160$	$\pm 1400$	pA
		OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 18$	nA
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$			$\pm 18$	nA
$I_{OS}$	Input offset current	$V_{CM} = V_S / 2$		$\pm 320$	$\pm 2800$	pA
		OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 6$	nA
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$			$\pm 6$	nA
<b>NOISE</b>						
$e_n$	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		250		nV <sub>PP</sub>
		$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		40		nV <sub>rms</sub>
	Input voltage noise density	$f = 1\text{ kHz}$		8.8		nV/ $\sqrt{\text{Hz}}$
$i_n$	Input current noise density	$f = 1\text{ kHz}$		7		fA/ $\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>						
$V_{CM}$	Common-mode voltage range	OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	$V^-$		$(V^+) - 1.5$	V
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$	$V^-$		$(V^+) - 1.5$	V
CMRR	Common-mode rejection ratio	$(V^-) < V_{CM} < (V^+) - 1.5\text{ V}$	120	134		dB
		$(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 18\text{ V}$	130	146		dB
		OPA188-Q1 $(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 18\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	120	126		dB
		OPA2188-Q1 $(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 18\text{ V}$ , $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$	120	126		dB
<b>INPUT IMPEDANCE</b>						
$Z_{ID}$	Differential			100    6		M $\Omega$    pF
$Z_{IC}$	Common-mode			6    9.5		$10^{12}\ \Omega$    pF
<b>OPEN-LOOP GAIN</b>						
$A_{OL}$	Open-loop voltage gain	$(V^-) + 0.5\text{ V} < V_O < (V^+) - 0.5\text{ V}$	130	136		dB
		OPA188-Q1 $(V^-) + 0.5\text{ V} < V_O < (V^+) - 0.5\text{ V}$ $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	120	126		dB
		OPA2188-Q1 $(V^-) + 0.5\text{ V} < V_O < (V^+) - 0.5\text{ V}$ $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$	120	126		dB
<b>FREQUENCY RESPONSE</b>						

(1)  $V_S / 2 = \text{midsupply}$ .

(2) 1000-hour life test at  $125^\circ\text{C}$  demonstrated randomly distributed variation in the range of measurement limits at approximately  $4\ \mu\text{V}$ .

**Electrical Characteristics: High-Voltage Operation (continued)**

 at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 4\text{ V}$  to  $\pm 18\text{ V}$  ( $V_S = 8\text{ V}$  to  $36\text{ V}$ ),  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  <sup>(1)</sup>, and  $V_{CM} = V_{OUT} = V_S / 2$  <sup>(1)</sup>  
 (unless otherwise noted)

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
GBW	Gain-bandwidth product			2		MHz
SR	Slew rate	$G = 1$		0.8		V/ $\mu\text{s}$
$t_s$	Settling time	0.1%	$V_S = \pm 18\text{ V}$ , $G = 1$ , 10-V step	20		$\mu\text{s}$
		0.01%	$V_S = \pm 18\text{ V}$ , $G = 1$ , 10-V step	27		$\mu\text{s}$
$t_{OR}$	Overload recovery time	$V_{IN} \times G = V_S$		1		$\mu\text{s}$
THD+N	Total harmonic distortion + noise	1 kHz, $G = 1$ , $V_{OUT} = 1\text{ V}_{RMS}$		0.0001%		
<b>OUTPUT</b>						
	Voltage output swing from rail	No load		6	15	mV
		$R_L = 10\text{ k}\Omega$		220	250	mV
		OPA188-Q1 $R_L = 10\text{ k}\Omega$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		310	350	mV
		OPA2188-Q1 $R_L = 10\text{ k}\Omega$ , $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$		310	350	mV
$I_{SC}$	Short-circuit current	Sinking		-18		mA
		Sourcing		16		mA
$R_O$	Open-loop output resistance	$f = 1\text{ MHz}$ , $I_O = 0\text{ mA}$		120		$\Omega$
$C_{LOAD}$	Capacitive load drive			1		nF
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current (per amplifier)	$V_S = \pm 4\text{ V}$ to $V_S = \pm 18\text{ V}$		450	510	$\mu\text{A}$
		OPA188-Q1 $I_O = 0\text{ mA}$ $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			600	$\mu\text{A}$
		OPA2188-Q1 $I_O = 0\text{ mA}$ $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$			600	$\mu\text{A}$



## 7.6 Electrical Characteristics: Low-Voltage Operation

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2\text{ V}$  to  $< \pm 4\text{ V}$  ( $V_S = 4\text{ V}$  to  $< 8\text{ V}$ ),  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2^{(1)}$ , and  $V_{CM} = V_{OUT} = V_S / 2^{(1)}$  (unless otherwise noted)

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>						
$V_{OS}$	Input offset voltage			$\pm 6$	$\pm 25$	$\mu\text{V}$
$dV_{IO}/dT$	Input offset voltage drift	OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		$\pm 0.03$	$\pm 0.085$	$\mu\text{V}/^\circ\text{C}$
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$		$\pm 0.03$	$\pm 0.085$	$\mu\text{V}/^\circ\text{C}$
PSRR	Power-supply rejection ratio	OPA188-Q1 $V_S = 4\text{ V}$ to $36\text{ V}$ $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		0.075	0.3	$\mu\text{V}/\text{V}$
		OPA2188-Q1 $V_S = 4\text{ V}$ to $36\text{ V}$ $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$		0.075	0.3	$\mu\text{V}/\text{V}$
Long-term stability <sup>(2)</sup>				4		$\mu\text{V}$
<b>INPUT BIAS CURRENT</b>						
$I_B$	Input bias current			$\pm 160$	$\pm 1400$	$\text{pA}$
		OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 18$	$\text{nA}$
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$			$\pm 18$	$\text{nA}$
$I_{OS}$	Input offset current			$\pm 320$	$\pm 2800$	$\text{pA}$
		OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			$\pm 6$	$\text{nA}$
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$			$\pm 6$	$\text{nA}$
<b>NOISE</b>						
$e_n$	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		250		$\text{nV}_{PP}$
		$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		40		$\text{nV}_{rms}$
	Input voltage noise density	$f = 1\text{ kHz}$		8.8		$\text{nV}/\sqrt{\text{Hz}}$
$i_n$	Input current noise density	$f = 1\text{ kHz}$		7		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>						
$V_{CM}$	Common-mode voltage range	OPA188-Q1 $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	$V^-$		$(V^+) - 1.5$	$\text{V}$
		OPA2188-Q1 $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$	$V^-$		$(V^+) - 1.5$	$\text{V}$
CMRR	Common-mode rejection ratio	$(V^-) < V_{CM} < (V^+) - 1.5\text{ V}$	106	114		$\text{dB}$
		$(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 2\text{ V}$	114	120		$\text{dB}$
		OPA188-Q1 $(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 2\text{ V}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	110	120		$\text{dB}$
		OPA2188-Q1 $(V^-) + 0.5\text{ V} < V_{CM} < (V^+) - 1.5\text{ V}$ $V_S = \pm 2\text{ V}$ , $T_A = -40^\circ\text{C}$ to $105^\circ\text{C}$	110	120		$\text{dB}$
<b>INPUT IMPEDANCE</b>						
$Z_{ID}$	Differential			$100 \parallel 6$		$\text{M}\Omega \parallel \text{pF}$
$Z_{IC}$	Common-mode			$6 \parallel 9.5$		$10^{12}\ \Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>						

(1)  $V_S / 2 = \text{midsupply}$ .

(2) 1000-hour life test at  $125^\circ\text{C}$  demonstrated randomly distributed variation in the range of measurement limits at approximately  $4\ \mu\text{V}$ .

**Electrical Characteristics: Low-Voltage Operation (continued)**

 at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2\text{ V}$  to  $< \pm 4\text{ V}$  ( $V_S = 4\text{ V}$  to  $< 8\text{ V}$ ),  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2^{(1)}$ , and  $V_{CM} = V_{OUT} = V_S / 2^{(1)}$   
 (unless otherwise noted)

PARAMETER		CONDITIONS	MIN	TYP	MAX	UNIT
A <sub>OL</sub>	Open-loop voltage gain	(V <sup>-</sup> ) + 0.5 V < V <sub>O</sub> < (V <sup>+</sup> ) - 0.5 V R <sub>L</sub> = 5 kΩ	110	120		dB
		(V <sup>-</sup> ) + 0.5 V < V <sub>O</sub> < (V <sup>+</sup> ) - 0.5 V	120	130		dB
		OPA188-Q1 (V <sup>-</sup> ) + 0.5 V < V <sub>O</sub> < (V <sup>+</sup> ) - 0.5 V T <sub>A</sub> = -40°C to 125°C	110	120		dB
		OPA2188-Q1 (V <sup>-</sup> ) + 0.5 V < V <sub>O</sub> < (V <sup>+</sup> ) - 0.5 V T <sub>A</sub> = -40°C to 105°C	110	120		dB
<b>FREQUENCY RESPONSE</b>						
GBW	Gain-bandwidth product			2		MHz
SR	Slew rate	G = 1		0.8		V/μs
t <sub>OR</sub>	Overload recovery time	V <sub>IN</sub> × G = V <sub>S</sub>		1		μs
THD+N	Total harmonic distortion + noise	1 kHz, G = 1, V <sub>OUT</sub> = 1 V <sub>RMS</sub>		0.0001%		
<b>OUTPUT</b>						
	Voltage output swing from rail	No load		6	15	mV
		R <sub>L</sub> = 10 kΩ		220	250	mV
		OPA188-Q1 R <sub>L</sub> = 10 kΩ, T <sub>A</sub> = -40°C to 125°C		310	350	mV
		OPA2188-Q1 R <sub>L</sub> = 10 kΩ, T <sub>A</sub> = -40°C to 105°C		310	350	mV
I <sub>SC</sub>	Short-circuit current	Sinking		-18		mA
		Sourcing		16		mA
R <sub>O</sub>	Open-loop output resistance	f = 1 MHz, I <sub>O</sub> = 0 mA		120		Ω
C <sub>LOAD</sub>	Capacitive load drive			1		nF
<b>POWER SUPPLY</b>						
I <sub>Q</sub>	Quiescent current (per amplifier)	V <sub>S</sub> = ±2 V to V <sub>S</sub> = ±4 V		425	485	μA
		OPA188-Q1 I <sub>O</sub> = 0 mA T <sub>A</sub> = -40°C to 125°C			575	μA
		OPA2188-Q1 I <sub>O</sub> = 0 mA T <sub>A</sub> = -40°C to 105°C			575	μA

## 7.7 Typical Characteristics: Table of Graphs

### 7.7.1 Table of Graphs

**表 1. Typical Characteristic Graphs**

DESCRIPTION	FIGURE
Offset Voltage Production Distribution	<a href="#">Figure 1</a>
Offset Voltage Drift Distribution	<a href="#">Figure 2</a>
Offset Voltage vs Temperature	<a href="#">Figure 3</a>
Offset Voltage vs Common-Mode Voltage	<a href="#">Figure 4</a> , <a href="#">Figure 5</a>
Offset Voltage vs Power Supply	<a href="#">Figure 6</a>
Open-Loop Gain and Phase vs Frequency	<a href="#">Figure 7</a>
Closed-Loop Gain vs Frequency	<a href="#">Figure 8</a>
$I_B$ and $I_{OS}$ vs Common-Mode Voltage	<a href="#">Figure 9</a>
Input Bias Current vs Temperature	<a href="#">Figure 10</a>
Output Voltage Swing vs Output Current (Maximum Supply)	<a href="#">Figure 11</a>
CMRR and PSRR vs Frequency (Referred-to-Input)	<a href="#">Figure 12</a>
CMRR vs Temperature	<a href="#">Figure 13</a> , <a href="#">Figure 14</a>
PSRR vs Temperature	<a href="#">Figure 15</a>
0.1-Hz to 10-Hz Noise	<a href="#">Figure 16</a>
Input Voltage Noise Spectral Density vs Frequency	<a href="#">Figure 17</a>
THD+N Ratio vs Frequency	<a href="#">Figure 18</a>
THD+N vs Output Amplitude	<a href="#">Figure 19</a>
Quiescent Current vs Supply Voltage	<a href="#">Figure 20</a>
Quiescent Current vs Temperature	<a href="#">Figure 21</a>
Open-Loop Gain vs Temperature	<a href="#">Figure 22</a>
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Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)	<a href="#">Figure 24</a> , <a href="#">Figure 25</a>
No Phase Reversal	<a href="#">Figure 26</a>
Positive Overload Recovery	<a href="#">Figure 27</a>
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Small-Signal Step Response (100 mV)	<a href="#">Figure 29</a> , <a href="#">Figure 30</a>
Large-Signal Step Response	<a href="#">Figure 31</a> , <a href="#">Figure 32</a>
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Short-Circuit Current vs Temperature	
Maximum Output Voltage vs Frequency	<a href="#">Figure 35</a>
EMIRR IN+ vs Frequency	<a href="#">Figure 36</a>

### 7.8 Typical Characteristics

at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)

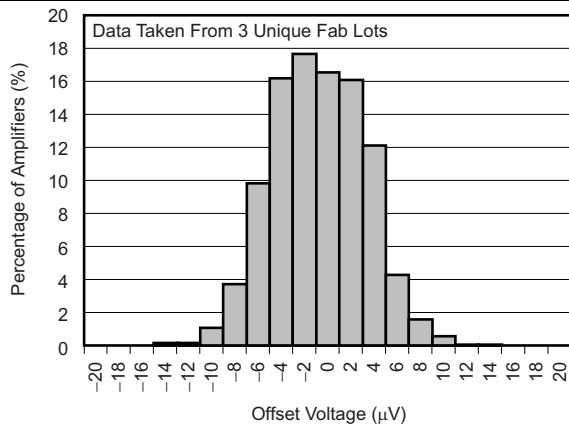


图 1. Offset Voltage Production Distribution

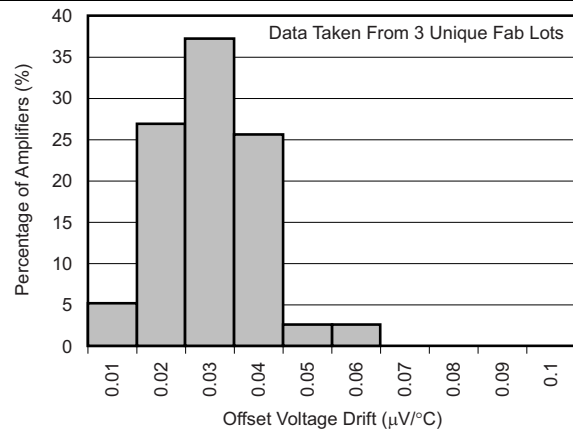
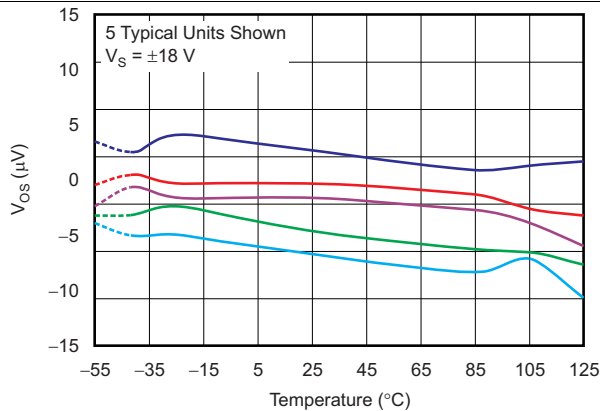


图 2. Offset Voltage Drift Distribution



OPA188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$   
OPA2188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$

图 3. Offset Voltage vs Temperature

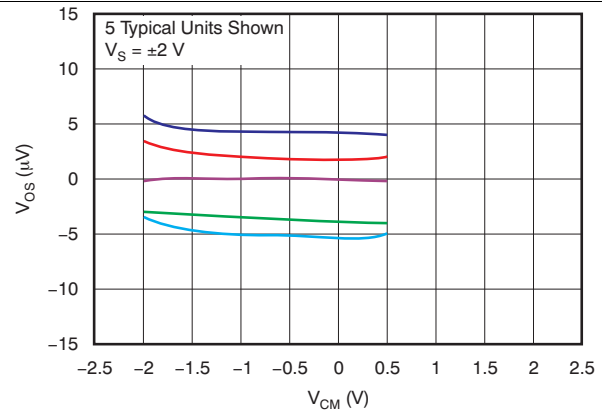


图 4. Offset Voltage vs Common-Mode Voltage

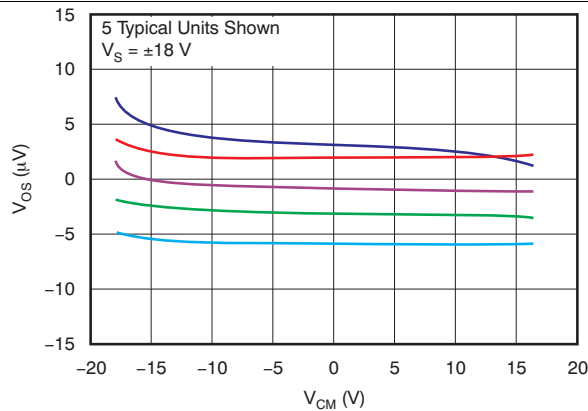


图 5. Offset Voltage vs Common-Mode Voltage

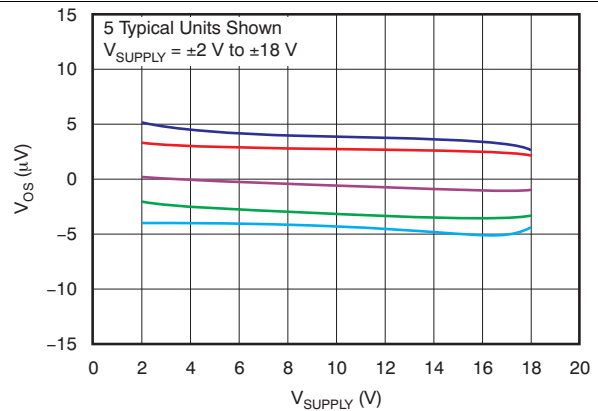
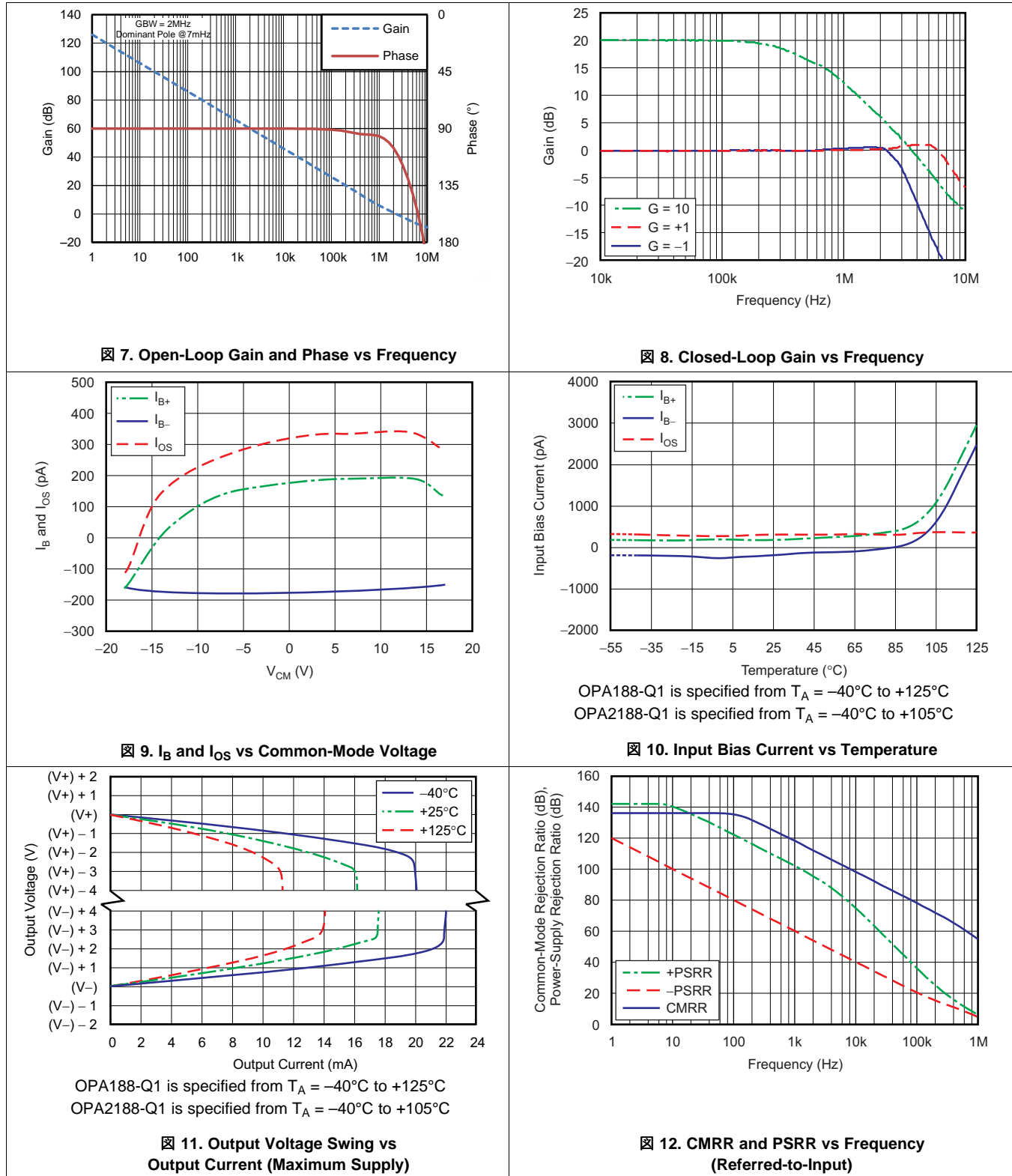


图 6. Offset Voltage vs Power Supply

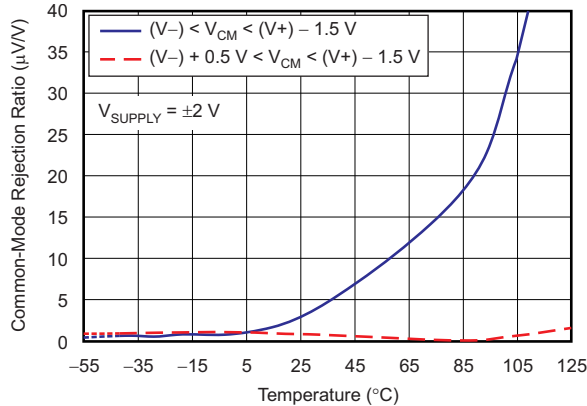
Typical Characteristics (continued)

at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)



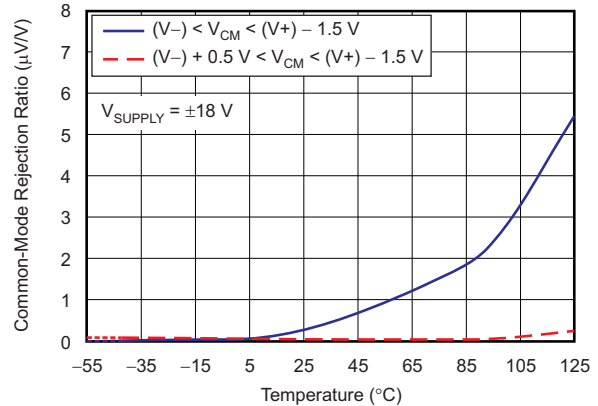
Typical Characteristics (continued)

at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)



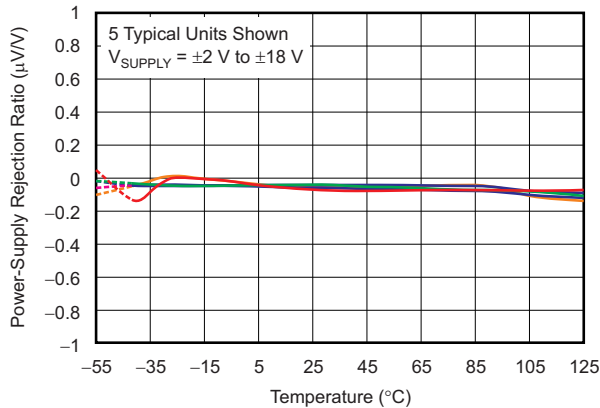
OPA188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$   
 OPA2188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$

FIG 13. CMRR vs Temperature



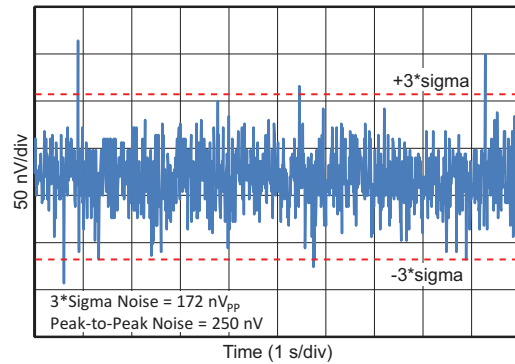
OPA188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$   
 OPA2188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$

FIG 14. CMRR vs Temperature



OPA188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$   
 OPA2188-Q1 is specified from  $T_A = -40^\circ\text{C}$  to  $+105^\circ\text{C}$

FIG 15. PSRR vs Temperature



C016

FIG 16. 0.1-Hz to 10-Hz Noise

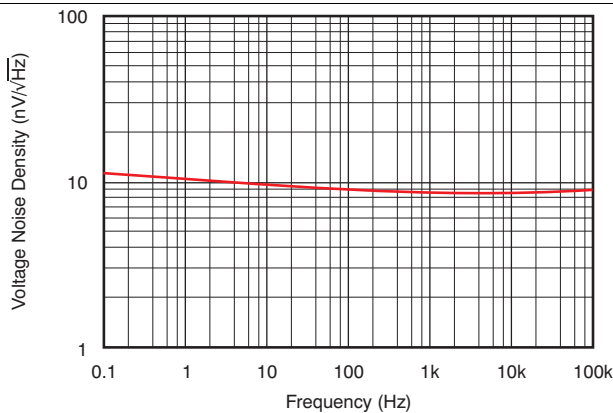


FIG 17. Input Voltage Noise Spectral Density vs Frequency

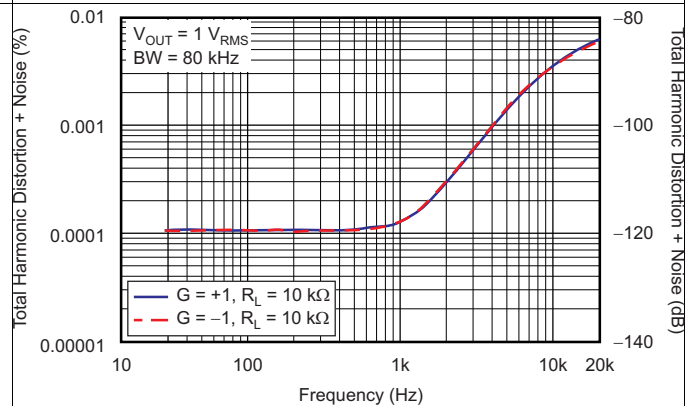


FIG 18. THD+N Ratio vs Frequency

Typical Characteristics (continued)

at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)

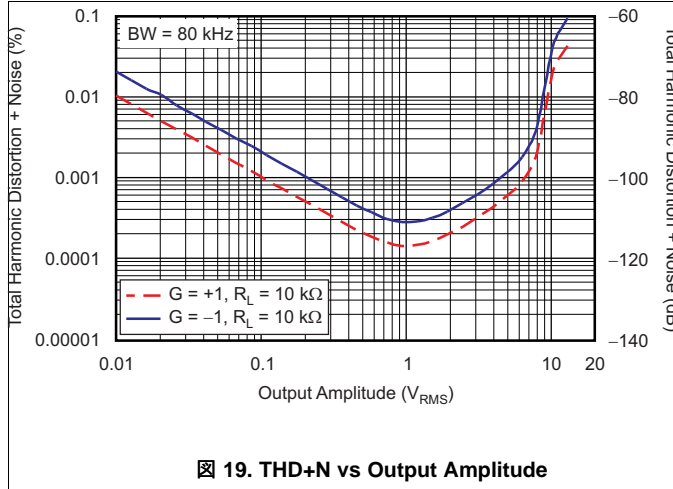


Figure 19. THD+N vs Output Amplitude

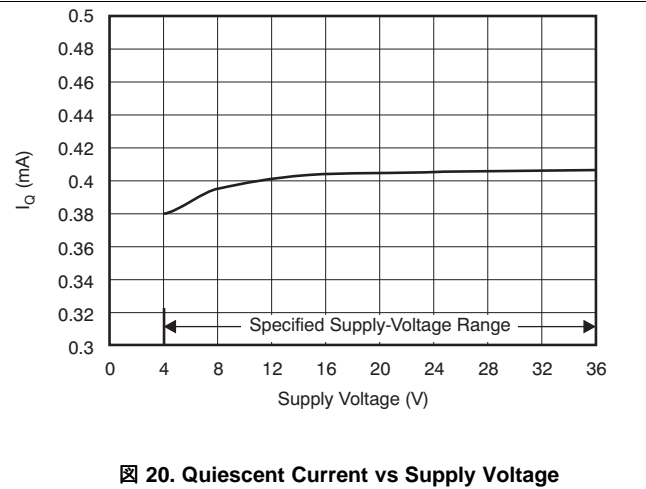


Figure 20. Quiescent Current vs Supply Voltage

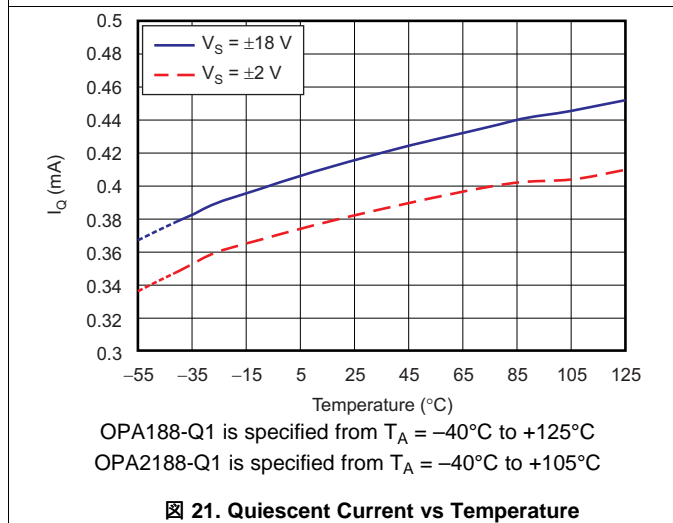


Figure 21. Quiescent Current vs Temperature

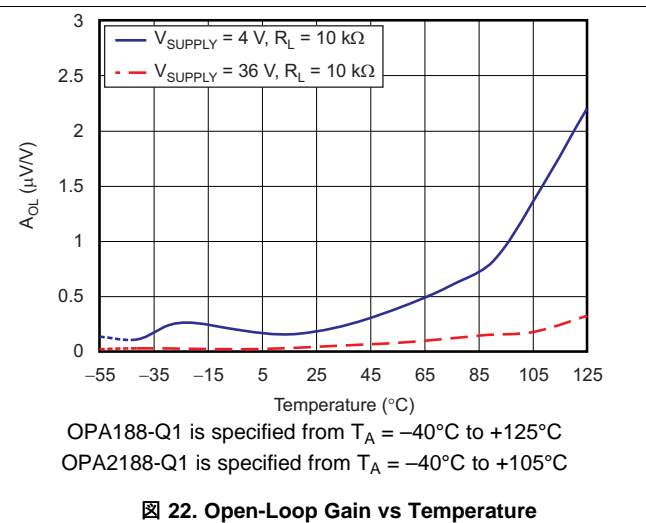


Figure 22. Open-Loop Gain vs Temperature

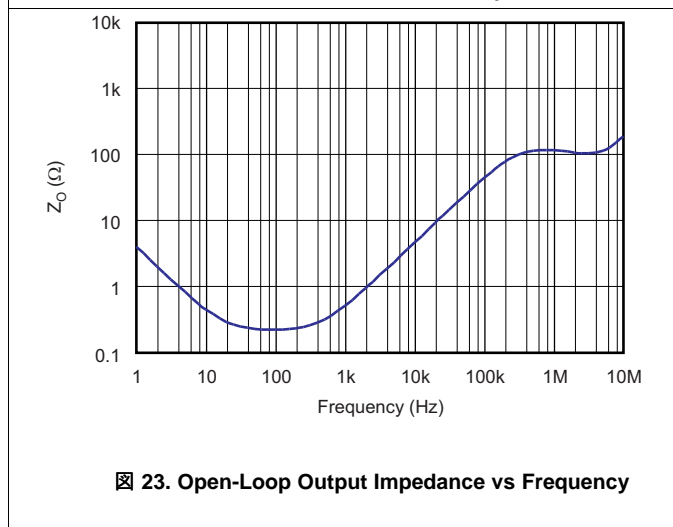


Figure 23. Open-Loop Output Impedance vs Frequency

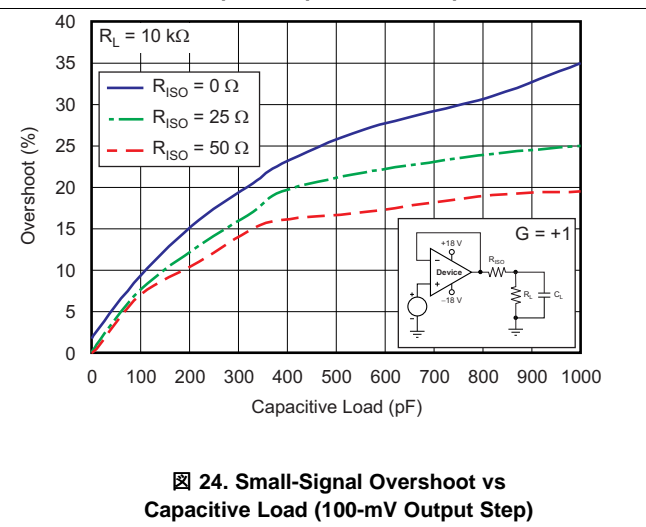
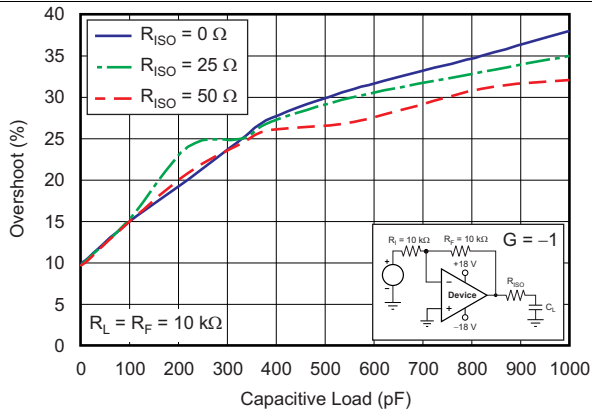


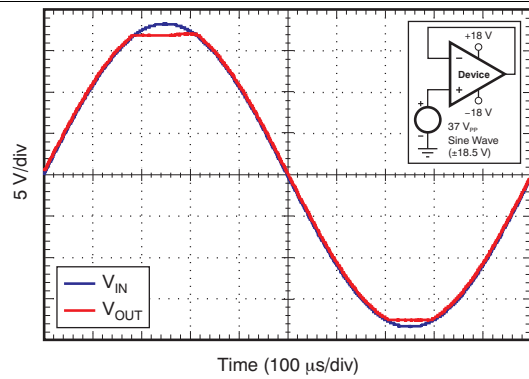
Figure 24. Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)

**Typical Characteristics (continued)**

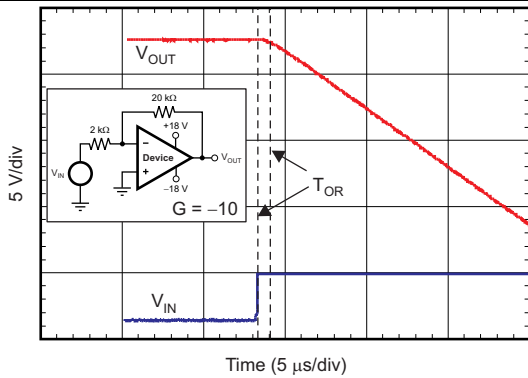
at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)



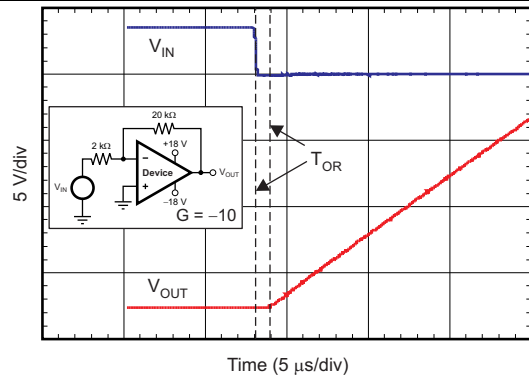
**25. Small-Signal Overshoot vs Capacitive Load (100-mV Output Step)**



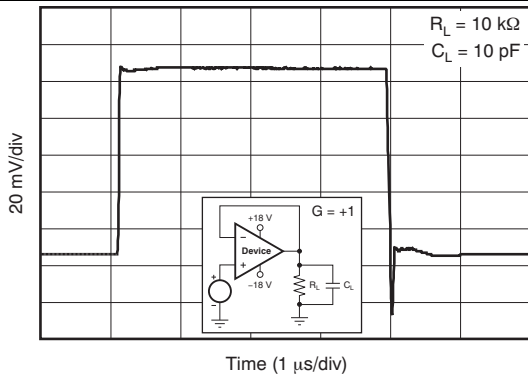
**26. No Phase Reversal**



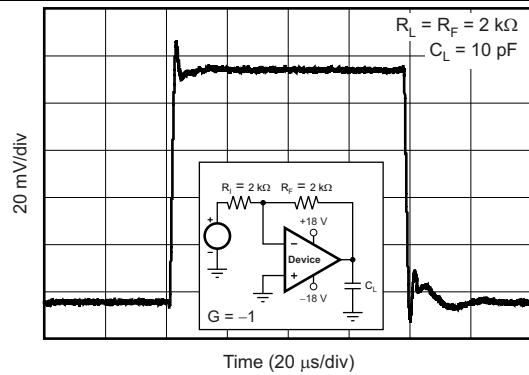
**27. Positive Overload Recovery**



**28. Negative Overload Recovery**



**29. Small-Signal Step Response (100 mV)**



**30. Small-Signal Step Response (100 mV)**



Typical Characteristics (continued)

at  $V_S = \pm 18\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 100\text{ pF}$  (unless otherwise noted)

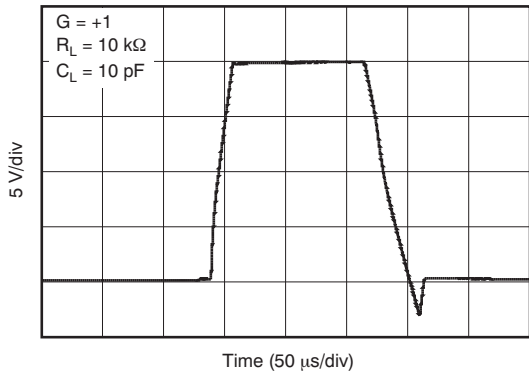


Figure 31. Large-Signal Step Response

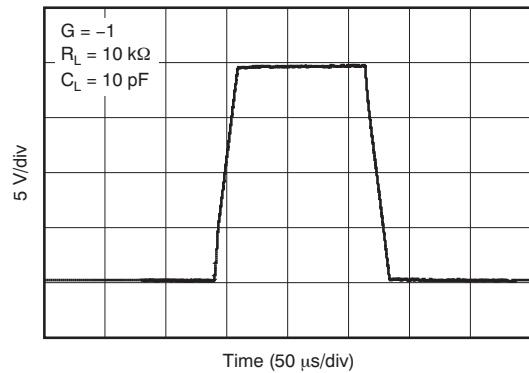


Figure 32. Large-Signal Step Response

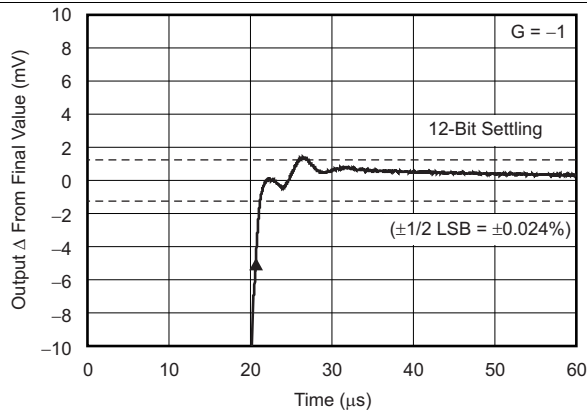


Figure 33. Large-Signal Settling Time (10-V Positive Step)

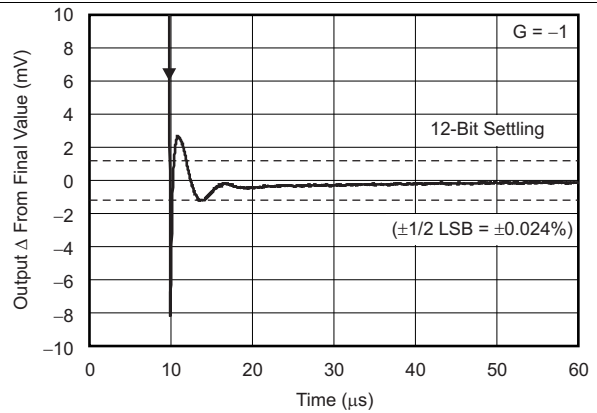


Figure 34. Large-Signal Settling Time (10-V Negative Step)

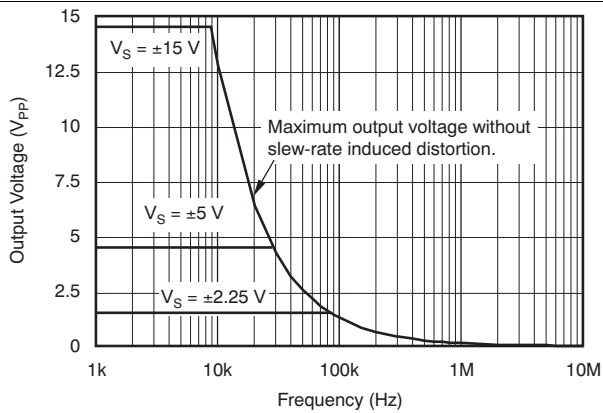


Figure 35. Maximum Output Voltage vs Frequency

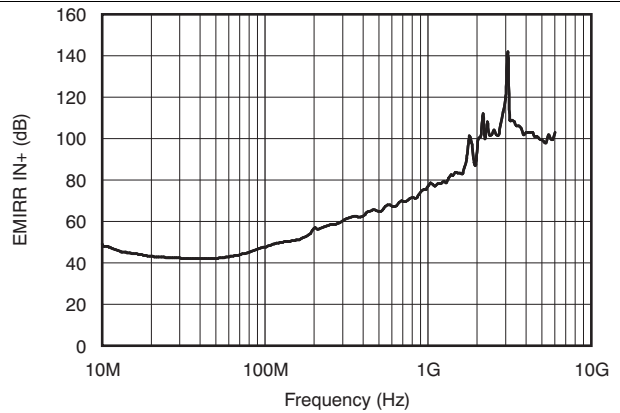


Figure 36. EMIRR IN+ vs Frequency

## 8 Detailed Description

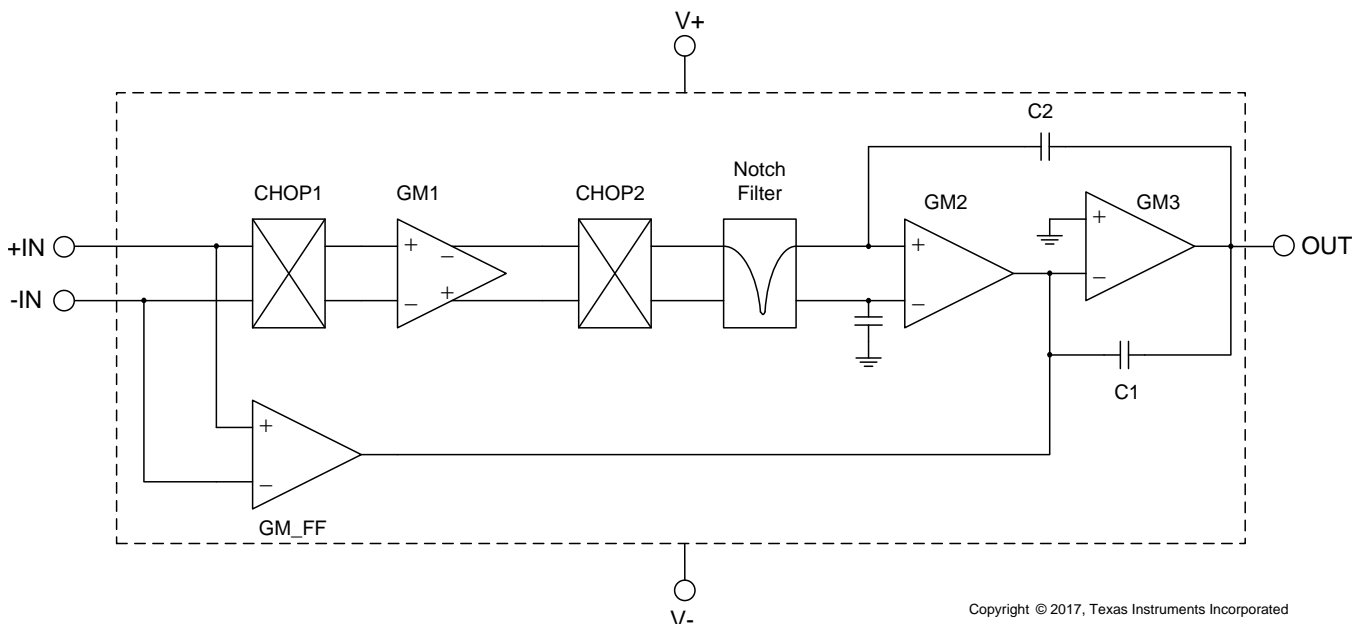
### 8.1 Overview

The OPAx188-Q1 operational amplifier series combines precision offset and drift with excellent overall performance, making the device ideal for many precision applications. The precision offset drift of only 0.085  $\mu\text{V}/^\circ\text{C}$  provides stability over the entire temperature range. In addition, this device offers excellent overall performance with high CMRR, PSRR, and  $A_{\text{OL}}$ . As with all amplifiers, applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1- $\mu\text{F}$  capacitors are adequate.

The OPAx188-Q1 device is part of a family of zero-drift, low-power, rail-to-rail output operational amplifiers. These devices operate from 4 V to 36 V, are unity-gain stable, and are suitable for a wide range of general-purpose applications. The zero-drift architecture provides ultra-low input offset voltage and near-zero input offset voltage drift over temperature and time. This choice of architecture also offers outstanding ac performance, such as ultra-low broadband noise and zero flicker noise.

### 8.2 Functional Block Diagram

Figure 37 shows a representation of the proprietary OPAx188-Q1 architecture. Table 2 lists the active and passive component counts for this device. The component count allows for accurate reliability calculations.



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Figure 37. Functional Block Diagram

Table 2. Component Count

COMPONENT	COUNT
Transistors	636
Diodes	5
Resistors	41
Capacitors	72

### 8.3 Feature Description

The OPAx188-Q1 series is unity-gain stable and free from unexpected output phase reversal. This device series uses a proprietary, periodic zero-drift technique to provide low input offset voltage and very low input offset voltage drift over temperature. For lowest offset voltage and precision performance, optimize circuit layout and mechanical conditions. Avoid temperature gradients that create thermoelectric (Seebeck) effects in the thermocouple junctions formed from connecting dissimilar conductors. Cancel these thermally-generated potentials by ensuring the potentials are equal on both input pins. Other layout and design considerations include:

- Use low thermoelectric-coefficient conditions (avoid dissimilar metals).
- Thermally isolate components from power supplies or other heat sources.
- Shield the operational amplifier and input circuitry from air currents, such as cooling fans.

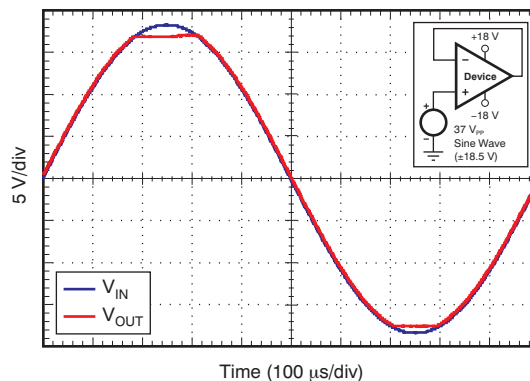
Follow these guidelines to reduce the likelihood of junctions being at different temperatures, which may cause thermoelectric voltages of 0.1  $\mu\text{V}/^\circ\text{C}$  or higher, depending on the materials used.

#### 8.3.1 Operating Characteristics

The OPAx188-Q1 is specified for operation from 4 V to 36 V ( $\pm 2$  V to  $\pm 18$  V). Many specifications apply from  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ . Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in [Typical Characteristics](#).

#### 8.3.2 Phase-Reversal Protection

The OPAx188-Q1 series has an internal phase-reversal protection. Many op amps exhibit a phase reversal when the input is driven beyond the linear common-mode range. This condition is most often encountered in noninverting circuits when the input is driven beyond the specified common-mode voltage range, causing the output to reverse into the opposite rail. The OPAx188-Q1 series input prevents phase reversal with excessive common-mode voltage. Instead, the output limits into the appropriate rail; [Figure 38](#) shows this performance.



**Figure 38. No Phase Reversal**

#### 8.3.3 Input Bias Current Clock Feedthrough

Zero-drift amplifiers (such as the OPAx188-Q1 series) use switching on the inputs to correct for the intrinsic offset and drift of the amplifier. Charge injection from the integrated switches on the inputs can introduce very short transients in the input bias current of the amplifier. The extremely short duration of these pulses prevents the devices from being amplified. However, the devices may be coupled to the output of the amplifier through the feedback network. The most effective method to prevent transients in the input bias current from producing additional noise at the amplifier output is to use a low-pass filter such as an RC network.

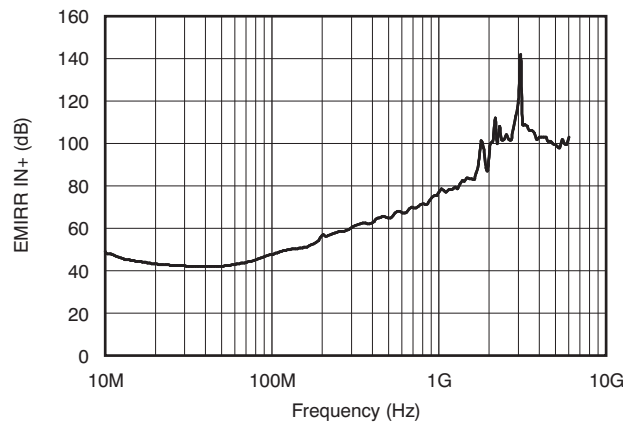
#### 8.3.4 Internal Offset Correction

The OPAx188-Q1 op amp series uses an auto-calibration technique with a time-continuous 750-kHz op amp in the signal path. This amplifier is zero-corrected every 3  $\mu\text{s}$  using a proprietary technique. Upon power up, the amplifier requires approximately 100  $\mu\text{s}$  to achieve the specified  $V_{\text{OS}}$  accuracy. This design has no aliasing or flicker noise.

## Feature Description (continued)

### 8.3.5 EMI Rejection

The OPAx188-Q1 series uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI interference from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the OPAx188-Q1 series benefits from these design improvements. Texas Instruments™ has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. [Figure 39](#) shows the results of this testing on the OPAx188-Q1. [Table 3](#) lists the EMIRR IN+ values for the OPAx188-Q1 devices at particular frequencies commonly encountered in real-world applications. Applications listed in [Table 3](#) may be centered on or operated near the particular frequency shown. Detailed information can also be found in [EMI Rejection Ratio of Operational Amplifiers](#), available for download from [www.ti.com](http://www.ti.com).



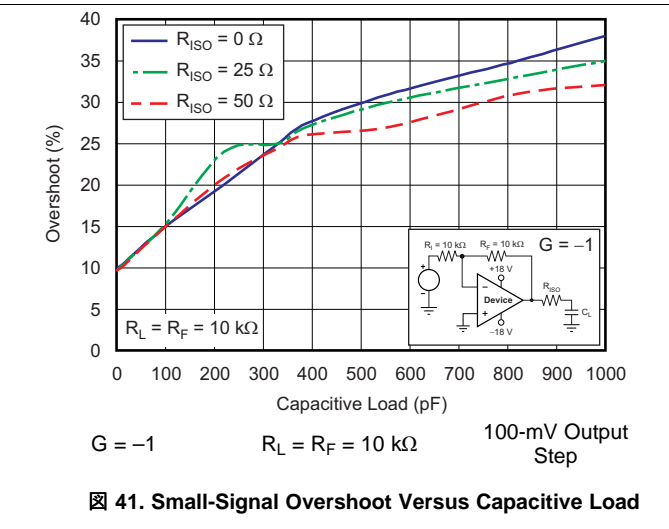
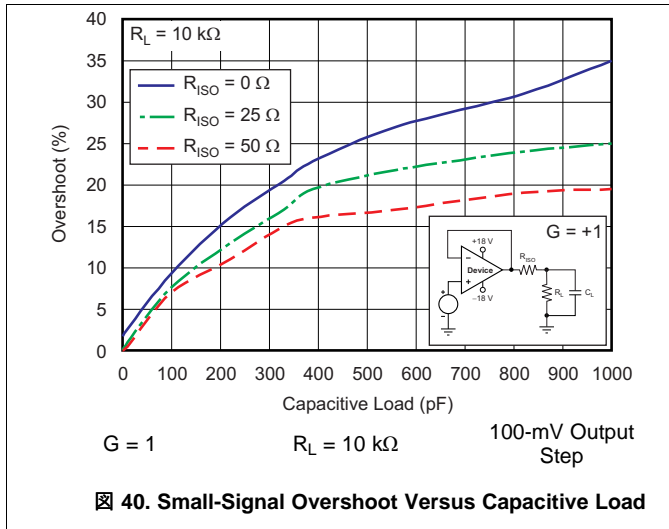
**Figure 39. EMIRR Testing**

**Table 3. OPAx188-Q1 EMIRR IN+ for Frequencies of Interest**

FREQUENCY	APPLICATION OR ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	62.2 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	74.7 dB
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	100.7 dB
2.4 GHz	802.11b, 802.11g, 802.11n, <i>Bluetooth</i> ®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	102.4 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	104.8 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	100.3 dB

### 8.3.6 Capacitive Load and Stability

The device dynamic characteristics are optimized for a range of common operating conditions. The combination of low closed-loop gain and high capacitive loads decreases the amplifier phase margin and can lead to gain peaking or oscillations. As a result, larger capacitive loads must be isolated from the output. The simplest way to achieve this isolation is to add a small resistor (for example,  $R_{OUT}$  equal to 50  $\Omega$ ) in series with the output. [Figure 40](#) and [Figure 41](#) show graphs of small-signal overshoot versus capacitive load for several values of  $R_{OUT}$ . For details of analysis techniques and application circuits, see [Feedback Plots Define Op Amp AC Performance](#), available for download from [www.ti.com](http://www.ti.com).



### 8.3.7 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

Having a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event is helpful. See Fig 42 for an illustration of the ESD circuits contained in the OPAx188-Q1 (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where the diodes meet at an internal absorption device of the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

An ESD event produces a short-duration, high-voltage pulse that is transformed into a short-duration, high-current pulse while discharging through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent damage. The energy absorbed by the protection circuitry is dissipated as heat.

When an ESD voltage develops across two or more amplifier device pins, current flows through one or more steering diodes. Depending on the path that the current takes, the absorption device may activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the OPAx188-Q1 but below the device breakdown voltage level. When this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

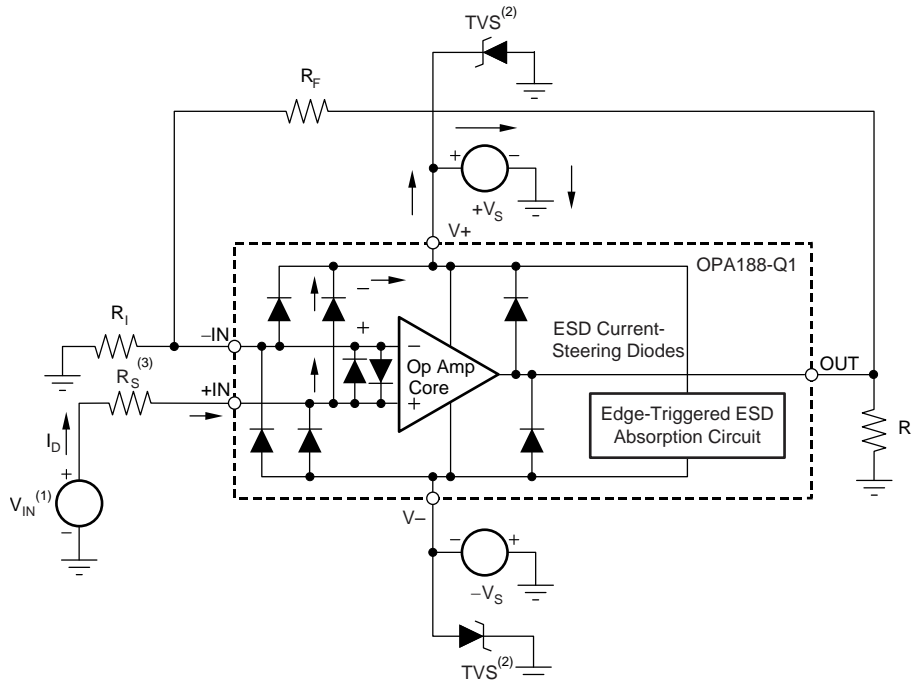
When the operational amplifier connects into a circuit (such as Fig 42 shows), the ESD protection components are intended to remain inactive and do not become involved in the operation of the application circuit. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. If this condition occurs, there is a risk that some internal ESD protection circuits may be biased on and conduct current. Any such current flow occurs through steering-diode paths and rarely involves the absorption device.

Fig 42 shows a specific example where the input voltage,  $V_{IN}$ , exceeds the positive supply voltage ( $+V_S$ ) by 500 mV or more. Much of what happens in the circuit depends on the supply characteristics. If  $+V_S$  can sink the current, one of the upper-input steering diodes conducts and directs current to  $+V_S$ . Excessively high current levels can flow with increasingly higher  $V_{IN}$ . As a result, the data sheet specifications recommend that applications limit the input current to 10 mA.

If the supply is not capable of sinking the current,  $V_{IN}$  may begin sourcing current to the operational amplifier, and then take over as the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the absolute maximum ratings of the operational amplifier.

Another common question involves what happens to the amplifier if an input signal is applied to the input while the power supplies ( $+V_S$  or  $-V_S$ ) are at 0 V. Again, this question depends on the supply characteristic while at 0 V, or at a level below the input signal amplitude. If the supplies appear as high impedance, then the operational amplifier supply current may be supplied by the input source through the current-steering diodes. This state is not a normal bias condition; the amplifier will not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

If there is any uncertainty about the ability of the supply to absorb this current, external zener diodes may be added to the supply pins, as shown in [Figure 42](#). The zener voltage must be selected such that the diode does not turn on during normal operation. However, the zener voltage must be low enough so that the zener diode conducts if the supply pin begins to rise above the safe operating supply voltage level.



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- (1)  $V_{IN} = +V_S + 500 \text{ mV}$ .
- (2) TVS:  $+V_{S(max)} > V_{TVSBR(min)} > +V_S$ .
- (3) Suggested value is approximately 1 k $\Omega$ .

#### **Figure 42. Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application**

The OPAx188-Q1 series input terminals are protected from excessive differential voltage with back-to-back diodes, as shown in [Figure 42](#). In most circuit applications, the input protection circuitry has no consequence. However, in low-gain and  $G = 1$  circuits, fast-ramping input signals can forward-bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. If the input signal is fast enough to create this forward-bias condition, the input signal current must be limited to 10 mA or less. If the input signal current is not inherently limited, an input series resistor can be used to limit the signal input current. This input series resistor degrades the low-noise performance of the OPAx188-Q1 series. [Figure 42](#) shows an example configuration that implements a current-limiting feedback resistor.

### **8.4 Device Functional Modes**

The OPAx188-Q1 series has a single functional mode, and is operational when the power-supply voltage is greater than 4.5 V ( $\pm 2.25$  V). The maximum power supply voltage for the OPAx188-Q1 family is 36 V ( $\pm 18$  V).

## 9 Application and Implementation

### 注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

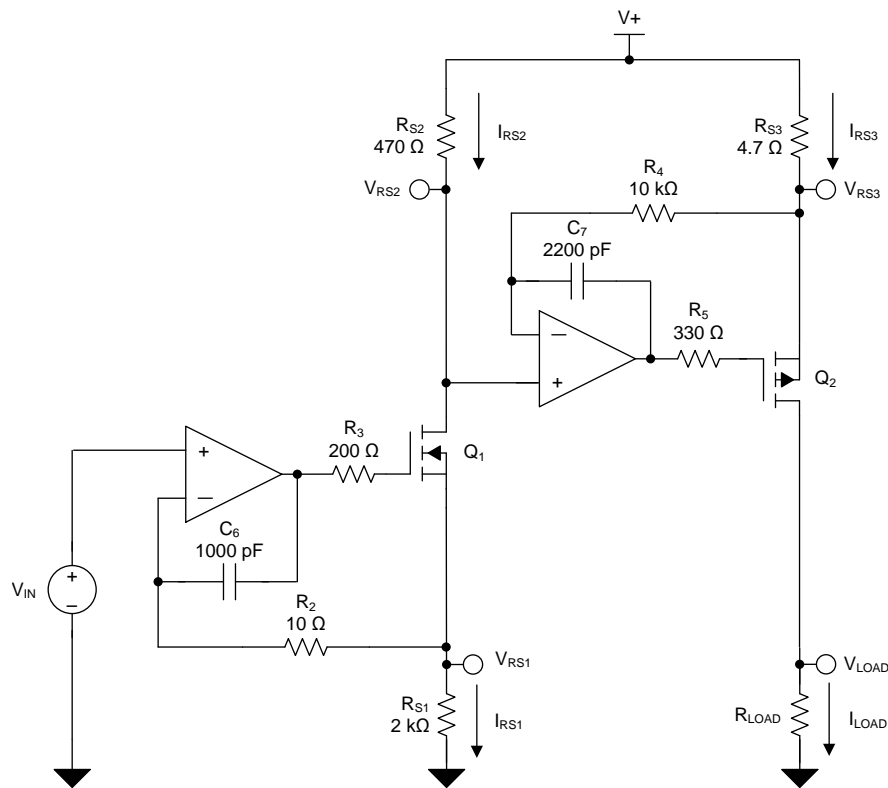
The OPAx188-Q1 operational amplifiers combine precision offset and drift with excellent overall performance, making the series ideal for many precision applications. The precision offset drift of only  $0.085 \mu\text{V}/^\circ\text{C}$  provides stability over the entire temperature range. In addition, the device pairs excellent CMRR, PSRR, and  $A_{OL}$  dc performance with outstanding low-noise operation. As with all amplifiers, applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases,  $0.1\text{-}\mu\text{F}$  capacitors are adequate.

The following application examples highlight only a few of the circuits where the OPAx188-Q1 series can be used.

### 9.2 Typical Applications

#### 9.2.1 High-Side Voltage-to-Current (V-I) Converter

The circuit shown in [Figure 43](#) is a high-side voltage-to-current (V-I) converter. The converter translates an input voltage of  $0\text{ V}$  to  $2\text{ V}$  to an output current of  $0\text{ mA}$  to  $100\text{ mA}$ . [Figure 44](#) shows the measured transfer function for this circuit. The low offset voltage and offset drift of the OPA2188-Q1 facilitate excellent dc accuracy for the circuit.



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**Figure 43. High-Side Voltage-to-Current (V-I) Converter**

## Typical Applications (continued)

### 9.2.1.1 Design Requirements

The design requirements are:

- Supply voltage: 5 V dc
- Input: 0 V to 2 V dc
- Output: 0 mA to 100 mA dc

### 9.2.1.2 Detailed Design Procedure

The V-I transfer function of the circuit is based on the relationship between the input voltage,  $V_{IN}$ , and the three current sensing resistors,  $R_{S1}$ ,  $R_{S2}$ , and  $R_{S3}$ . The relationship between  $V_{IN}$  and  $R_{S1}$  determines the current that flows through the first stage of the design. The current gain from the first stage to the second stage is based on the relationship between  $R_{S2}$  and  $R_{S3}$ .

For a successful design, pay close attention to the dc characteristics of the operational amplifier chosen for the application. To meet the performance goals, this application benefits from an operational amplifier with low offset voltage, low temperature drift, and rail-to-rail output. The OPAx188-Q1 CMOS operational amplifier is a high-precision, ultra-low offset, ultra-low drift amplifier, optimized for low-voltage, single-supply operation, with an output swing to within 15 mV of the positive rail. The devices in the OPAx188-Q1 family use chopping techniques to provide low initial offset voltage and near-zero drift over time and temperature. Low offset voltage and low drift reduce the offset error in the system, making this device appropriate for precise dc control. The rail-to-rail output stage of the OPAx188-Q1 makes sure that the output swing of the operational amplifier is able to fully control the gate of the MOSFET devices within the supply rails.

A detailed error analysis, design procedure, and additional measured results are given in reference design TIPD102, a step-by-step process to design a [High-Side Voltage-to-Current \(V-I\) Converter](#).



For step-by-step design procedure, circuit schematics, bill of materials, PCB files, simulation results, and test results, refer to [TI Precision Design TIPD102, High-Side Voltage-to-Current \(V-I\) Converter \(SLAU502\)](#).

### 9.2.1.3 Application Curves

Figure 44 shows the measured transfer function for the high-side voltage-to-current converter shown in Figure 43.

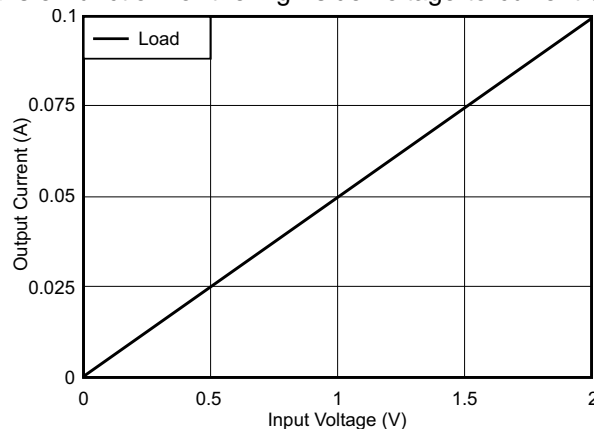


Figure 44. Measured Transfer Function for High-Side V-I Converter

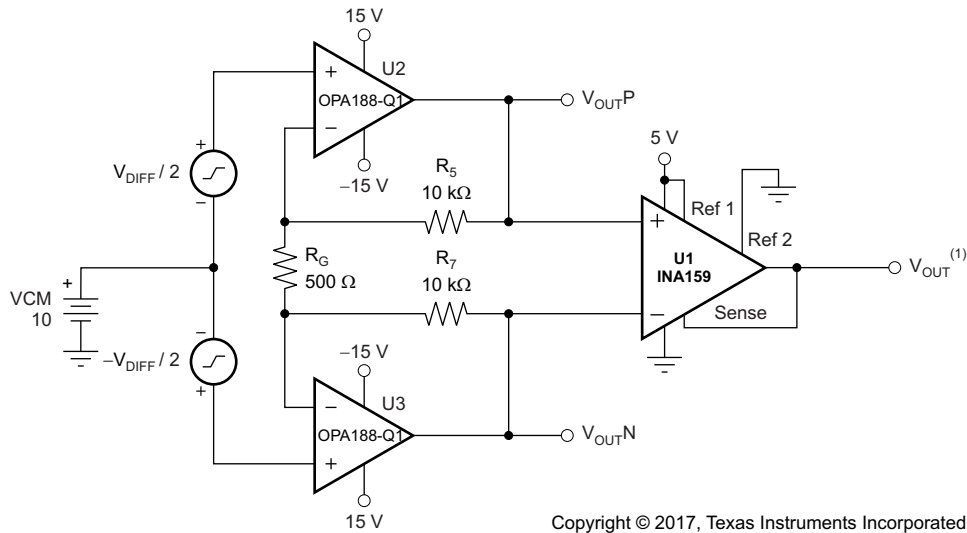


### 9.2.2 Discrete INA + Attenuation for ADC With 3.3-V Supply

注

The TINA-TI files shown in the following sections require that either the TINA software (from DesignSoft™) or TINA-TI software be installed. Download the free TINA-TI software from the [TINA-TI folder](#).

Figure 45 shows an example of how the OPA188-Q1 series is used as a high-voltage, high-impedance front-end for a precision, discrete instrumentation amplifier with attenuation. The INA159 provides the attenuation that allows this circuit to easily interface with 3.3-V or 5-V analog-to-digital converters (ADCs). Click the following link to download the TINA-TI file: [Discrete INA](#).



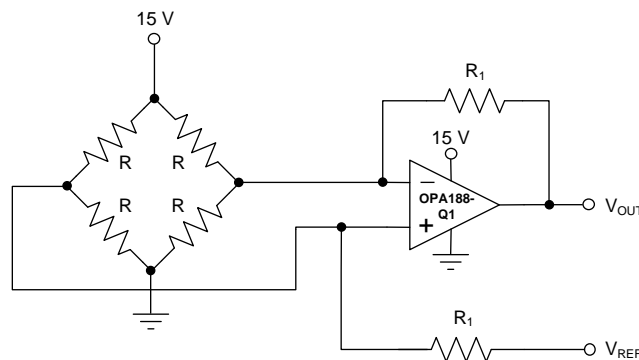
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$$(1) V_{OUT} = V_{DIFF} \times (41 / 5) + (Ref 1) / 2.$$

Figure 45. Discrete INA + Attenuation for ADC With 3.3-V Supply

### 9.2.3 Bridge Amplifier


Figure 46 shows the basic configuration for a bridge amplifier. Click the following link to download the TINA-TI file: [Bridge Amplifier Circuit](#).

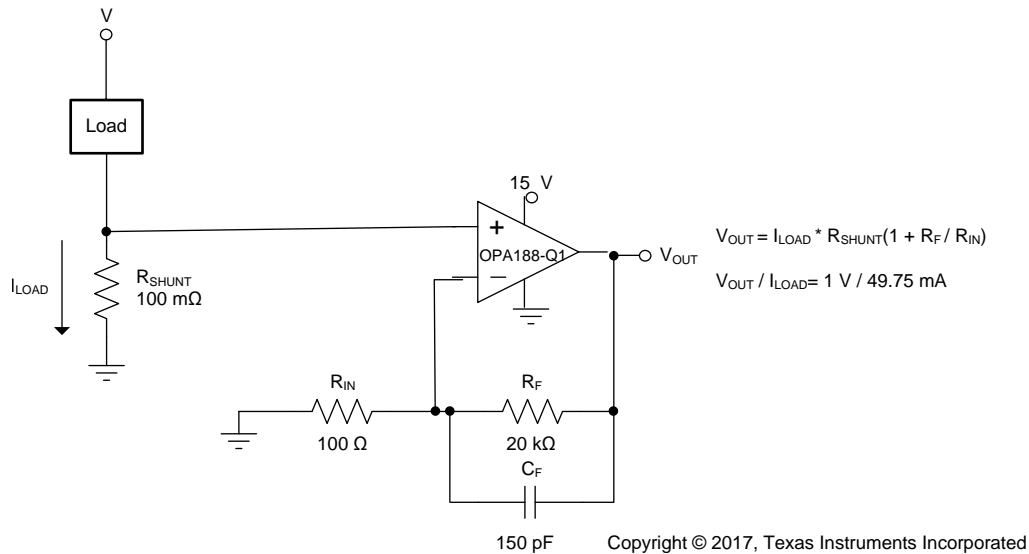


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Figure 46. Bridge Amplifier


### 9.2.4 Low-Side Current Monitor

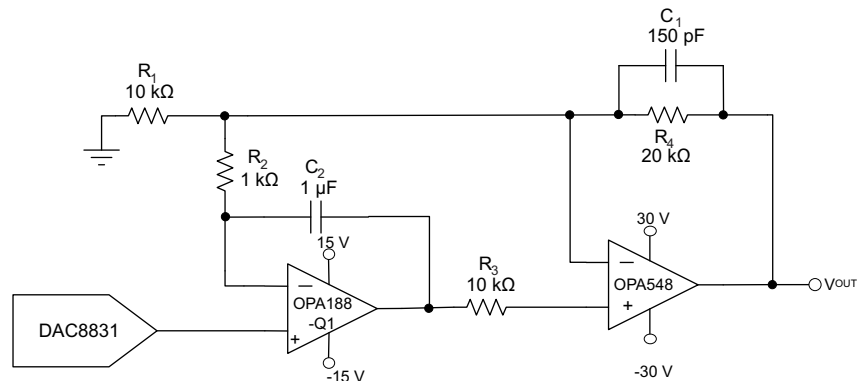

**47** shows the OPAx188-Q1 configured in a low-side current-sensing application. The load current ( $I_{LOAD}$ ) creates a voltage drop across the shunt resistor ( $R_{SHUNT}$ ). This voltage is amplified by the OPAx188-Q1, with a gain of 201. The load current is set from 0 A to 500 mA, which corresponds to an output voltage range from 0 V to 10 V. The output range can be adjusted by changing the shunt resistor or gain of the configuration. Click the following link to download the TINA-TI file: [Current-Sensing Circuit](#).



**47. Low-Side Current Monitor**

### 9.2.5 Programmable Power Supply

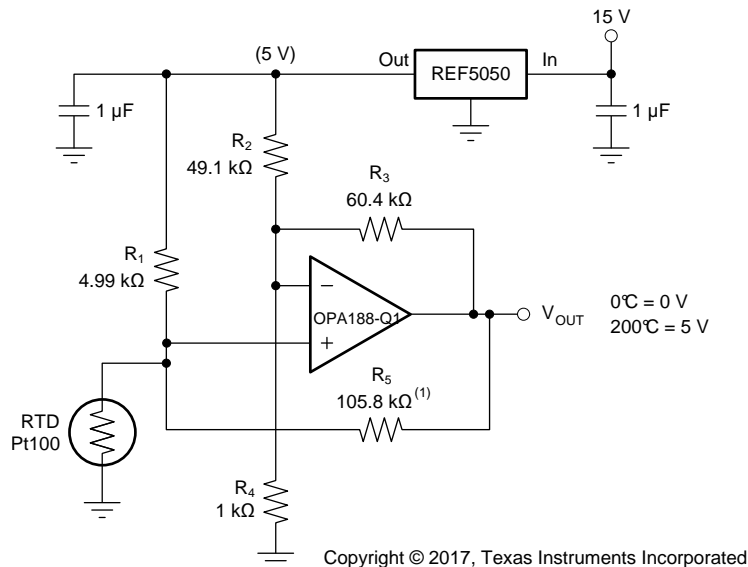

**48** shows the OPA188-Q1 configured as a precision programmable power supply using the 16-bit, voltage output [DAC8581](#) and the [OPA548](#) high-current amplifier. This application amplifies the digital-to-analog converter (DAC) voltage by a value of five, and handles a large variety of capacitive and current loads. The OPA188-Q1 in the front-end provides precision and low drift across a wide range of inputs and conditions. Click the following link to download the TINA-TI file: [Programmable Power-Supply Circuit](#).



**48. Programmable Power Supply**

## 9.2.6 RTD Amplifier With Linearization

See [Analog Linearization Of Resistance Temperature Detectors](#) for an in-depth analysis of [Figure 49](#). Click the following link to download the TINA-TI file: [RTD Amplifier with Linearization](#).



(1)  $R_5$  provides positive-varying excitation to linearize output.

**Figure 49. RTD Amplifier With Linearization**

## 10 Power Supply Recommendations

The OPAx188-Q1 series is specified for operation from 4 V to 36 V ( $\pm 2$  V to  $\pm 18$  V); many specifications apply from  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ . [Typical Characteristics](#) presents parameters that can exhibit significant variance with regard to operating voltage or temperature.

### 注意

Supply voltages larger than 40 V can permanently damage the device (see the [Absolute Maximum Ratings](#)).

Place 0.1- $\mu\text{F}$  bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, see [Layout](#).

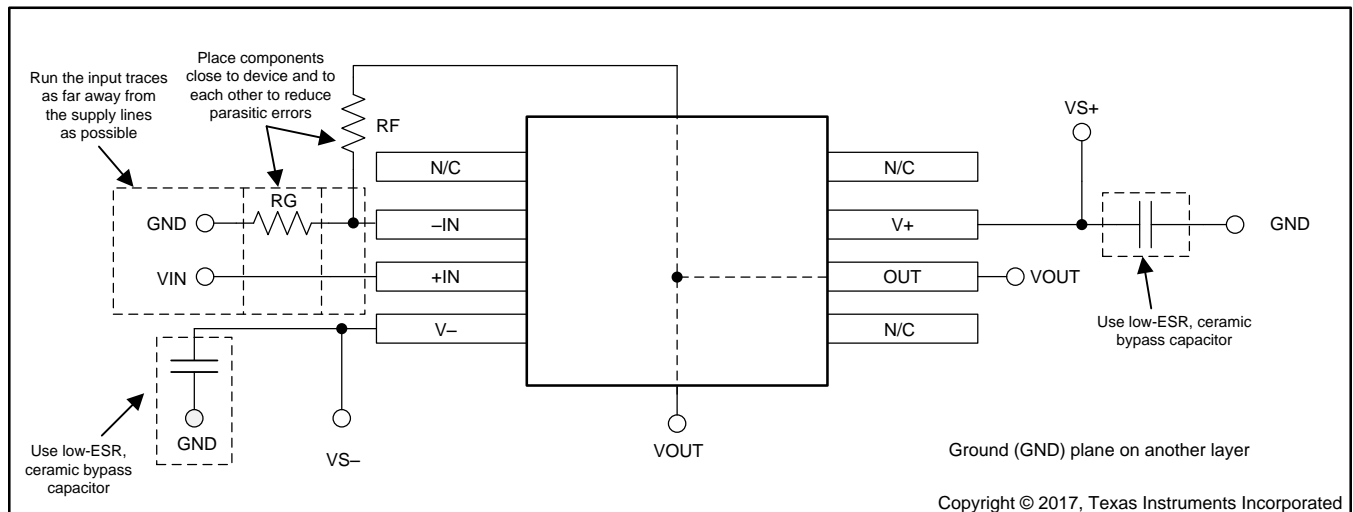
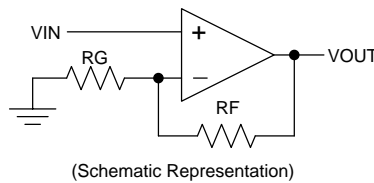
## 11 Layout

### 11.1 Layout Guidelines

For best operational performance of the device, use good printed circuit board (PCB) layout practices, including:

- Low-ESR, 0.1- $\mu$ F ceramic bypass capacitors must be connected between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable to single-supply applications.
- To reduce parasitic coupling, run the input traces as far away from the supply lines as possible.
- A ground plane helps distribute heat and reduces EMI noise pickup.
- Place the external components as close to the device as possible. This configuration prevents parasitic errors (such as the Seebeck effect) from occurring.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.

### 11.2 Layout Example



☒ 50. Layout Example

## 12 デバイスおよびドキュメントのサポート

### 12.1 デバイス・サポート

#### 12.1.1 開発サポート

##### 12.1.1.1 TINA-TI™(無償のダウンロード・ソフトウェア)

TINA™ は、SPICEエンジンをベースにした単純かつ強力な、使いやすい回路シミュレーション・プログラムです。また、TINA-TIは、TINA-TIソフトウェアのフル機能を持つ無償バージョンで、パッシブ・モデルとアクティブ・モデルに加えて、マクロ・モデルのライブラリがプリロードされています。TINA-TIには、SPICEの標準的なDC解析、過渡解析、周波数ドメイン解析などの全機能に加え、追加の設計機能が搭載されています。

TINA-TIは無償でダウンロードでき、ユーザーが結果をさまざまな方法でフォーマットできる、広範な後処理機能を備えています。仮想計測器により、入力波形を選択し、回路ノード、電圧、および波形をプローブして、動的なクイック・スタート・ツールを作成できます。

### 12.2 ドキュメントのサポート

#### 12.2.1 関連資料

関連資料については、以下を参照してください:

- 『オペアンプのEMI除去率』(SBOA128)
- 『フィードバック・プロットによるオペアンプAC性能の定義』(SBOA015)
- 『抵抗温度検出器のアナログ線形化』(SLYT442)
- 『ハイサイドの電圧/電流(V-I)コンバータ』(SLAU502)

### 12.3 関連リンク

表 4 に、クイック・アクセス・リンクの一覧を示します。カテゴリには、技術資料、サポートおよびコミュニティ・リソース、ツールとソフトウェア、およびサンプル注文またはご購入へのクイック・アクセスが含まれます。

表 4. 関連リンク

製品	プロダクト・フォルダ	ご注文はこちら	技術資料	ツールとソフトウェア	サポートとコミュニティ
OPA188-Q1	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>
OPA2188-Q1	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>

### 12.4 ドキュメントの更新通知を受け取る方法

ドキュメントの更新についての通知を受け取るには、[ti.com](http://ti.com)のデバイス製品フォルダを開いてください。右上の隅にある「通知を受け取る」をクリックして登録すると、変更されたすべての製品情報に関するダイジェストを毎週受け取れます。変更の詳細については、修正されたドキュメントに含まれている改訂履歴をご覧ください。

### 12.5 コミュニティ・リソース

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

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**設計サポート** TIの設計サポート 役に立つE2Eフォーラムや、設計サポート・ツールをすばやく見つけることができます。技術サポート用の連絡先情報も参照できます。

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*Bluetooth* is a registered trademark of Bluetooth SIG, Inc.  
 DesignSoft, TINA are trademarks of DesignSoft, Inc.

## 12.7 静電気放電に関する注意事項



すべての集積回路は、適切なESD保護方法を用いて、取扱いと保存を行うようにして下さい。

静電気放電はわずかな性能の低下から完全なデバイスの故障に至るまで、様々な損傷を与えます。高精度の集積回路は、損傷に対して敏感であり、極めてわずかなパラメータの変化により、デバイスに規定された仕様に適合しなくなる場合があります。

## 12.8 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 13 メカニカル、パッケージ、および注文情報

以降のページには、メカニカル、パッケージ、および注文に関する情報が記載されています。この情報は、そのデバイスについて利用可能な最新のデータです。このデータは予告なく変更されることがあり、ドキュメントが改訂される場合もあります。本データシートのブラウザ版を使用されている場合は、画面左側の説明をご覧ください。

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA188AQDGKRQ1	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	188	<a href="#">Samples</a>
OPA2188AQDGKRQ1	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	2188	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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# DGK0008A



# PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



4214862/A 04/2023

**NOTES:**

PowerPAD is a trademark of Texas Instruments.

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

# EXAMPLE BOARD LAYOUT

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

# EXAMPLE STENCIL DESIGN

DGK0008A

<sup>TM</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
SCALE: 15X

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NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.

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