

TLV61047 20V_{IN}、28V_{OUT}、2.2A 非同期整流昇圧コンバータ

1 特長

- 入力電圧範囲: 2.6V~20V
- 出力電圧範囲: 4.5V~28V
- 内蔵ローサイド FET: 200mΩ
- 高効率
 - $V_{IN} = 5V$ 、 $V_{OUT} = 12V$ 、 $I_{OUT} = 0.2A$ で最大 91.2% の効率
 - $V_{IN} = 12V$ 、 $V_{OUT} = 28V$ 、 $I_{OUT} = 0.3A$ で最大 91.7% の効率
- 2.2A のピーク スイッチ電流制限
- スイッチング周波数
 - TLV61047: 1.6MHz
 - TLV610471: 0.6MHz
- 基準電圧精度: $\pm 2.0\%$
- 静止電流: 25 μ A (標準値)
- シャットダウン電流: 0.4 μ A (標準値)
- 超軽負荷で、または T_{ON} 最小値がトリガされたときに PFM 動作モード
- 内部補償
- 2.5ms の内部ソフト スタート時間
- サイクル単位の電流制限
- サーマル シャットダウン保護機能
- SOT-23-5 DDC パッケージ

2 アプリケーション

- LED の電源
- デジタル カメラ
- GPS デバイス
- 携帯電話
- OLED パネル用電源
- USB 給電機器

3 概要

TLV61047 は、200mΩ ローサイド パワー スイッチを内蔵した高電圧の非同期昇圧コンバータで、使いやすい小型サイズの電源ソリューションを提供します。TLV61047 は、入力電圧範囲が 2.6V~20V と広く、出力電圧は最大 28V に対応し、2.2A のスイッチ電流能力を備えています。

TLV61047 は、適応型一定オフ時間ピーク電流制御トポロジを使用して、出力電圧をレギュレートします。TLV61047 は、重~軽負荷の状況では、TON 最小値または最小ピーク電流 (通常は 20mA) をトリガするまで、パルス幅変調 (PWM) モードで動作します。非常に軽い負荷の状況では、パルス周波数変調 (PFM) モードで動作して効率およびリップル性能を高めます。

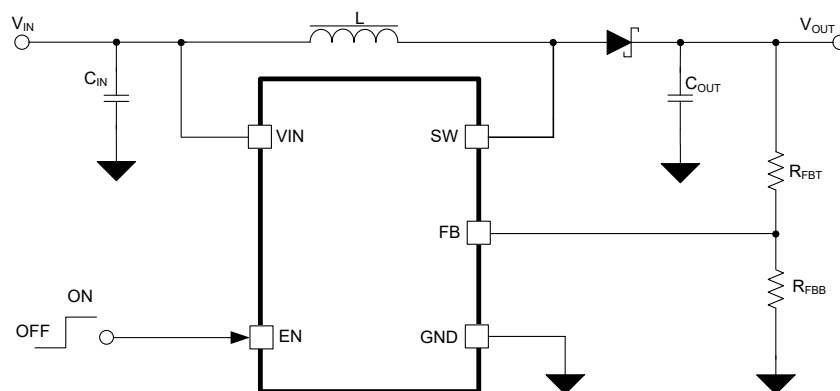
擬似定スイッチング周波数は内部で 1.6MHz (TLV61047) または 0.6MHz (TLV610471) に設定されており、超小型の表面実装インダクタとコンデンサが使用できます。TLV61047 は、2.5ms のソフト スタート機能を搭載しています。これにより、スタートアップ時の突入電流が最小化されます。追加機能として、内部補償、サイクル単位の電流制限、サーマル シャットダウンを備えています。

TLV61047 は、SOT-23-5 DOC パッケージで供給されません。

製品情報 (1)

部品番号	パッケージ	本体サイズ (公称)
TLV61047	SOT-23 (5)	2.90mm × 1.60mm

(1) 利用可能なすべてのパッケージについては、データシートの末尾にある注文情報を参照してください。



代表的なアプリケーション回路



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4 Device Comparison Table

PART NUMBER	FREQUENCY
TLV61047	1.6MHz
TLV610471	0.6MHz

5 Pin Configuration and Functions

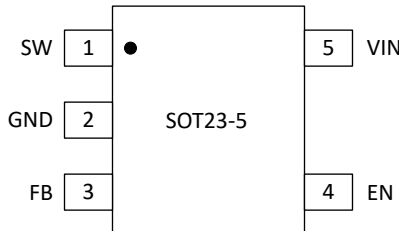


図 5-1. DDC Package 5-Pin SOT-23 Top View

Pin Functions

PIN		TYPE ⁽¹⁾	DESCRIPTION
NAME	DDC NO.		
SW	1	PWR	The switch pin of the converter. It is connected to the drain of the internal power MOSFET.
GND	2	G	Ground.
FB	3	I	Voltage feedback of output voltage. Connected to the center tap of a resistor divider to program the output voltage.
EN	4	I	Enable logic input. Logic high voltage enables the device. Logic low voltage disables the device and turns it into shutdown mode.
VIN	5	I	IC power supply input.

(1) I = Input, G = Ground, PWR = Power

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) ⁽¹⁾

		MIN	MAX	UNIT
Voltage range at terminals ⁽²⁾	VIN,EN	-0.3	20.5	V
	SW	-0.3	32	V
	FB	-0.3	6	V
Operating junction temperature range, T _J		-40	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.

6.2 ESD Ratings

			VALUE	UNIT
V _(ESD) ⁽¹⁾	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins ⁽²⁾	±2000	V
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins ⁽³⁾	±500	V

- (1) Electrostatic discharge (ESD) to measure device sensitivity and immunity to damage caused by assembly line electrostatic discharges in to the device.
- (2) Level listed above is the passing level per ANSI, ESDA, and JEDEC JS-001. JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process. Manufacturing with less than 500-V HBM is possible with the necessary precautions.
- (3) Level listed above is the passing level per EIA-JEDEC JESD22-C101. JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process. Manufacturing with less than 250-V CDM is possible with the necessary precautions.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	TYP	MAX	UNIT
V _{IN}	Input voltage range	2.6		20	V
V _{OUT}	Output voltage range	4.5		28	V
L	Inductance range	2.2	4.7	22	μH
C _{IN}	Effective input capacitance range	1	10		μF
C _{OUT}	Effective output capacitance range	1	10		μF
T _J	Operating junction temperature	-40		125	°C

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TLV61047	UNIT
		DDC (SOT23)	
		5 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	145.8	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	77.6	
R _{θJB}	Junction-to-board thermal resistance	56.5	
ψ _{JT}	Junction-to-top characterization parameter	28.5	
ψ _{JB}	Junction-to-board characterization parameter	54.9	
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	NA	

- (1) For more information about traditional and new thermal metrics, see the [IC Package Thermal Metrics](#) application report.

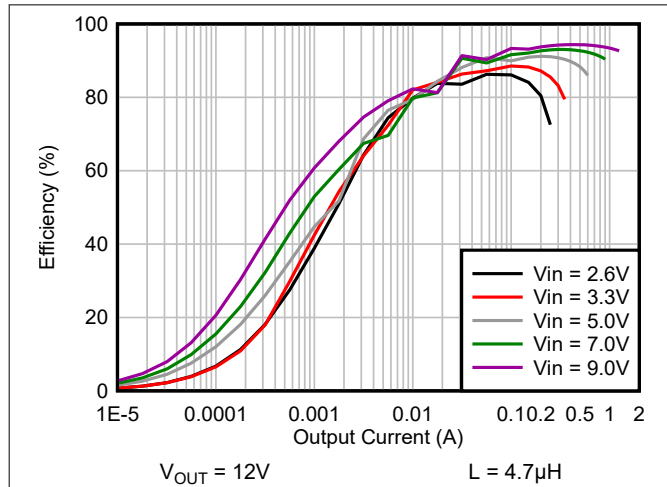
6.5 Electrical Characteristics

$T_J = -40^{\circ}\text{C}$ to 125°C , $V_{IN} = 5.0\text{V}$. Typical values are at $T_J = 25^{\circ}\text{C}$, unless otherwise noted.

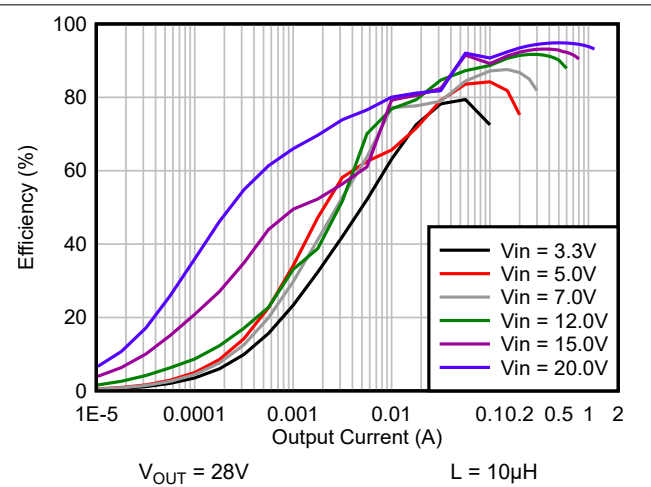
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
POWER SUPPLY						
V_{IN}	Input voltage range		2.6		20	V
V_{IN_UVLO}	Under voltage lockout threshold	V_{IN_UVLO} rising		2.42	2.55	V
		V_{IN_UVLO} falling	2.1	2.26		
V_{IN_HYS}	V_{IN_UVLO} hysteresis			160		mV
I_{Q_VIN}	Quiescent current into VIN pin	IC enabled, no load, no switching, $V_{IN} = 2.6\text{V}$ to 20V , $FB = 1.4\text{V}$, $T_J = -40^{\circ}\text{C}$ to 125°C		25	50	μA
I_{SD}	Shutdown current into VIN pin	IC disabled, $V_{IN} = 2.6\text{V}$ to 20V , $T_J = \text{up to } 85^{\circ}\text{C}$		0.4	1.5	μA
I_{FB_LKG}	Leakage current into FB pin	$T_J = -40^{\circ}\text{C}$ to 125°C			50	nA
I_{SW_LKG}	Leakage current into SW pin	IC disabled, $SW = 28\text{V}$, $T_J = -40^{\circ}\text{C}$ to 125°C			500	nA
OUTPUT						
V_{OUT}	Output voltage range		4.5		28	V
V_{REF}	Reference Voltage at FB pin	PWM and PFM mode, $T_J = -40^{\circ}\text{C}$ to 125°C	1.209	1.233	1.258	V
POWER SWITCH						
$R_{DS(on)}$	Low-side MOSFET on resistance	$V_{IN} = 5\text{V}$, $V_{OUT} = 12\text{V}$		200		m Ω
F_{SW}	TLV61047 Switching frequency	$V_{IN} = 5\text{V}$, $V_{OUT} = 12\text{V}$	1.2	1.6	2.0	MHz
F_{SW}	TLV610471 Switching frequency	$V_{IN} = 5\text{V}$, $V_{OUT} = 12\text{V}$	0.4	0.6	0.8	MHz
t_{ON_min}	Minimum on time			45	150	ns
I_{LIM_SW}	Peak switch current limit	$V_{IN} = 5\text{V}$	1.9	2.2	2.5	A
$t_{STARTUP}$	Soft startup time	Internal SS ramp time, from 0V to V_{REF}		2.5		ms
LOGIC INTERFACE						
V_{EN_H}	EN Logic high threshold				1.2	V
V_{EN_L}	EN Logic low threshold		0.4			V
R_{EN}	EN Pull Down Resistor			1		M Ω
PROTECTION						
T_{SD}	Thermal shutdown threshold	T_J rising		170		$^{\circ}\text{C}$
T_{SD_HYS}	Thermal shutdown hysteresis	T_J falling below T_{SD}		20		$^{\circ}\text{C}$

6.6 Typical Characteristics

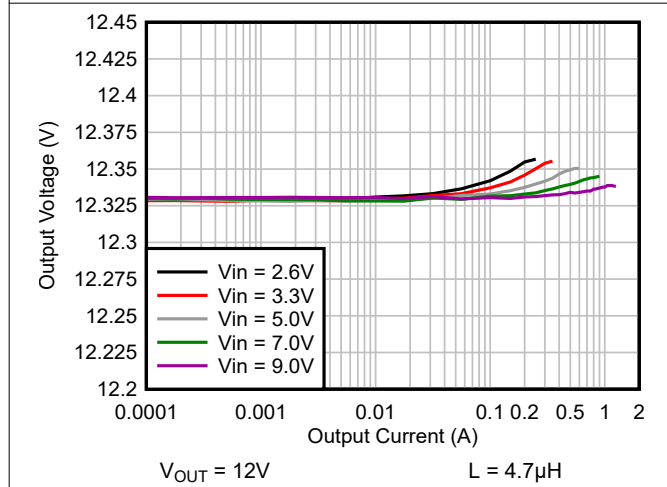
TLV61047, switching frequency = 1.6MHz (typ), $T_A = 25^\circ\text{C}$, unless otherwise noted



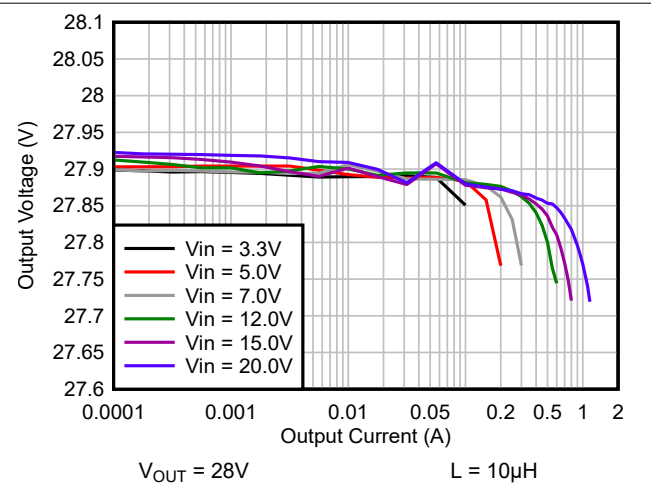
6-1. Efficiency vs Output Current, $V_{OUT} = 12\text{V}$



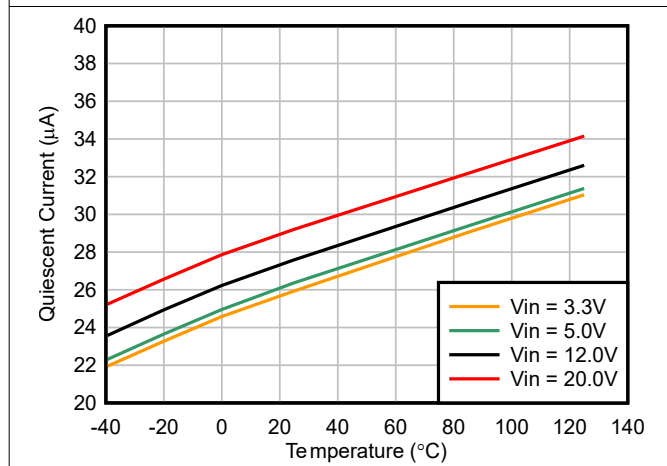
6-2. Efficiency vs Output Current, $V_{OUT} = 28\text{V}$



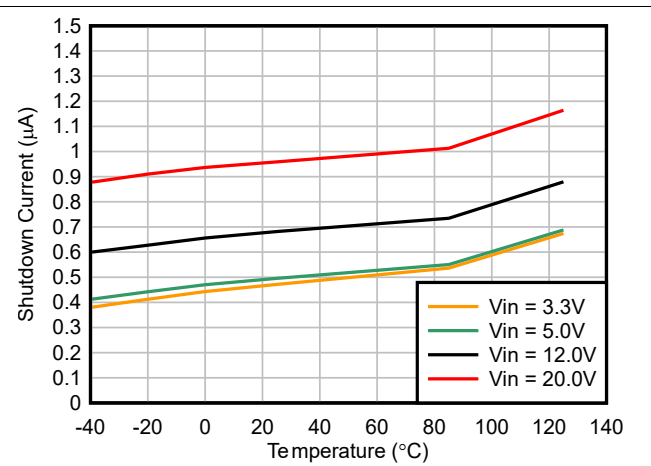
6-3. Load regulation, $V_{OUT} = 12\text{V}$



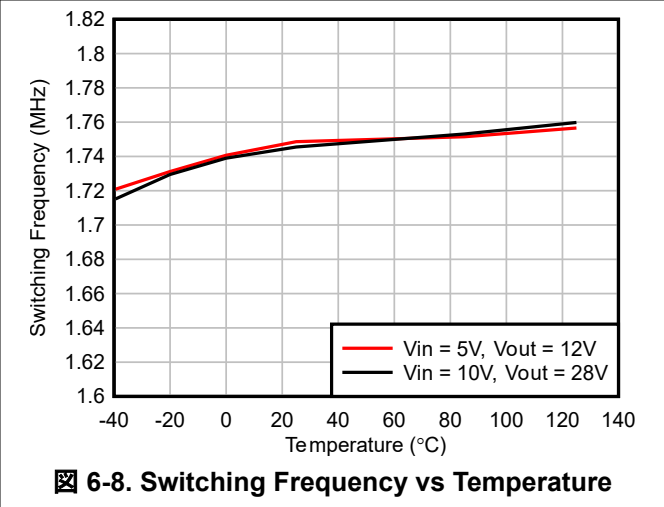
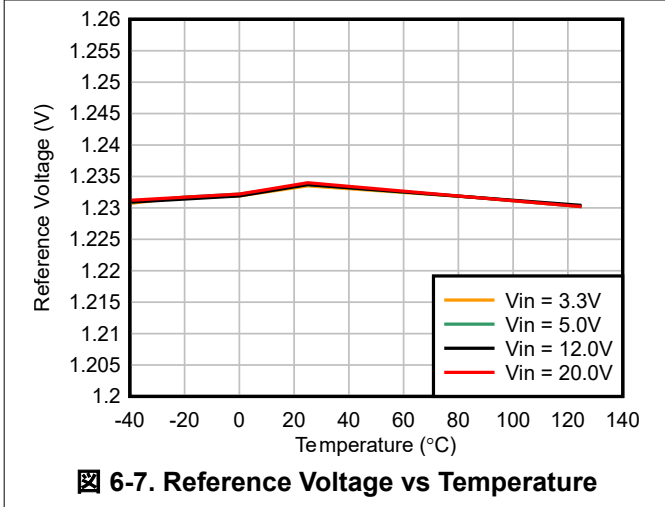
6-4. Load regulation, $V_{OUT} = 28\text{V}$



6-5. Quiescent Current vs Temperature



6-6. Shutdown Current vs Temperature



7 Detailed Description

7.1 Overview

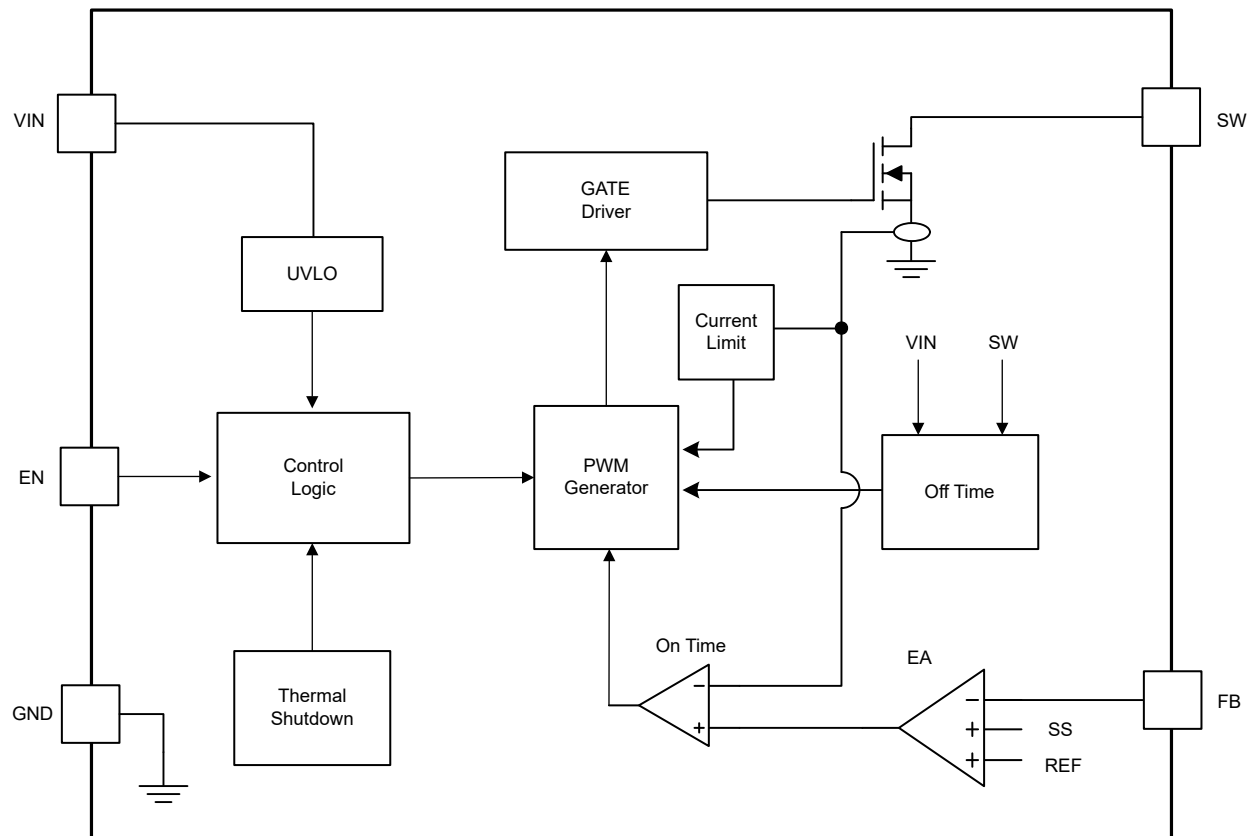
The TLV61047 is a high voltage non-synchronous boost converter integrates a 200mΩ low side power switch to provide a easy use and small size power solution. The TLV61047 has a wide input voltage range from 2.6V to 20V and output voltage covers up to 28V with 2.2A switch current capability.

The TLV61047 uses adaptive constant off-time peak current control topology to regulate the output voltage. At heavy to light load condition, the TLV61047 works in pulse width modulation (PWM) mode until trigger the Ton min or minimum peak current(around 20mA). At ultra light load condition , the devices work in pulse frequency modulation (PFM) mode to improve the efficiency and ripple performance.

The quasi-constant switching frequency is internally set to either 1.6MHz (TLV61047) or 0.6MHz (TLV610471), allowing the use of extremely small surface mount inductor and chip capacitors. The TLV61047 have built in 2.5ms soft start to minimize the inrush current during start up. Additional features include internal compensation, cycle by cycle current limit and thermal shutdown.

The TLV61047 is available in a SOT-23-5 DDC package.

7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 Undervoltage Lockout

An undervoltage lockout (UVLO) circuit stops the operation of the converter when the input voltage drops below the typical UVLO falling threshold of 2.26V. A hysteresis of 160mV is added so that the device cannot be enabled again until the input voltage goes up to typical UVLO rising threshold of 2.42V. This function is implemented in order to prevent malfunctioning of the device when the input voltage is between 2.24V and 2.42V.

7.3.2 Enable and Disable

When the input voltage is above typical UVLO rising threshold of 2.42V and the EN pin is pulled high, the TLV61047 is enabled. When the EN pin is pulled low, the TLV61047 stops the PWM switch and turns off the low side switch. The EN pin has an internal pull-down resistance of 1M Ω , the device is disabled when the EN pin is floating. In shutdown mode, less than 0.4 μ A(typical) input current is consumed.

7.3.3 Soft Start

The soft-start feature helps the regulator to gradually reach the steady state operating point, thus reducing start-up stresses and surge. When the input voltage is applied, the output capacitor is charged to VIN through the inductor and high side rectifier diode. After reaching the 2.42V (typical) UVLO rising threshold and EN logic high, the internal soft-start control circuit initiates to ramp the reference voltage with slew rate from 0V to 1.233V within 2.5ms (typical).

7.3.4 Thermal Shutdown

A thermal shutdown is implemented to prevent the damage due to the excessive heat and power dissipation. Typically, the thermal shutdown occurs at the junction temperature exceeding 170°C (typical). When the thermal shutdown is triggered, the device stops switching and recovers when the junction temperature falls below 150°C (typical).

7.4 Device Functional Modes

The TLV61047 operates at a quasi-constant frequency pulse width modulation (PWM) under heavy to light load conditions. As the load current decreases, the output of the internal error amplifier also decreases to lower the inductor peak current and delivers less power. The PWM mode can be divided into CCM-PWM mode and DCM-PWM mode based on the load conditions.

- The device operates in CCM-PWM mode with a heavy to moderate load. During this phase, the inductor current valley is always above zero.
- The device operates in DCM-PWM mode as the load continues to decrease from moderate to light. As the name DCM (Discontinuous Current Mode) suggests, an obvious characteristic of this mode is that the inductor current remains at zero for one period in each cycle. During this phase, the inductor peak current can still be reduced by the output of the internal error amplifier to maintain the balance between input and output power. This allows a suitable off-time of the low-side FET to be worked out internally to keep the switching frequency quasi-constant without pulse skipping. This phase ends when the inductor peak current decreases to I_{CLAMP_LOW} , which is typically 20mA.

After the peak inductor current reaches the I_{CLAMP_LOW} and the load decreases to ultra-light or even no load, the peak inductor current can't be smaller. To balance the input and output energy, the low-side FET is turned off for a prolonged period. The duration of the "zero inductor current" is much longer than in the DCM-PWM phase. This phase is called DCM-PFM mode for features of discontinuous inductor current and significantly reduced frequency. The three phases of CCM-PWM, DCM-PWM and DCM-PFM are shown in the [Figure 7-1](#).

In work conditions where the V_{IN} is very close to the V_{OUT} , the V_{IN}/V_{OUT} ratio decided turn on time may be less than the minimum turn on time, the device also enters into the DCM-PFM mode.

At light load, when $T_{ON\ min}$ is triggered the device also enters DCM-PFM mode even if the inductor peak current is greater than I_{CLAMP_LOW} . When the low-side FET is turned on, it remains on for a minimum time, called $T_{ON\ min}$. The inductor is energised for at least $T_{ON\ min}$ time when the low-side FET is on. If the $T_{ON\ min}$ is greater than the ideal time required to maintain the quasi-constant frequency, the device has to extend the off time to balance the input and output energy. So the device is in DCM-PFM mode. Under normal work conditions, the $T_{ON\ min}$ triggered DCM-PFM mode is much more common than that triggered by I_{CLAMP_LOW} , unless an inductor with extremely large inductance is used.

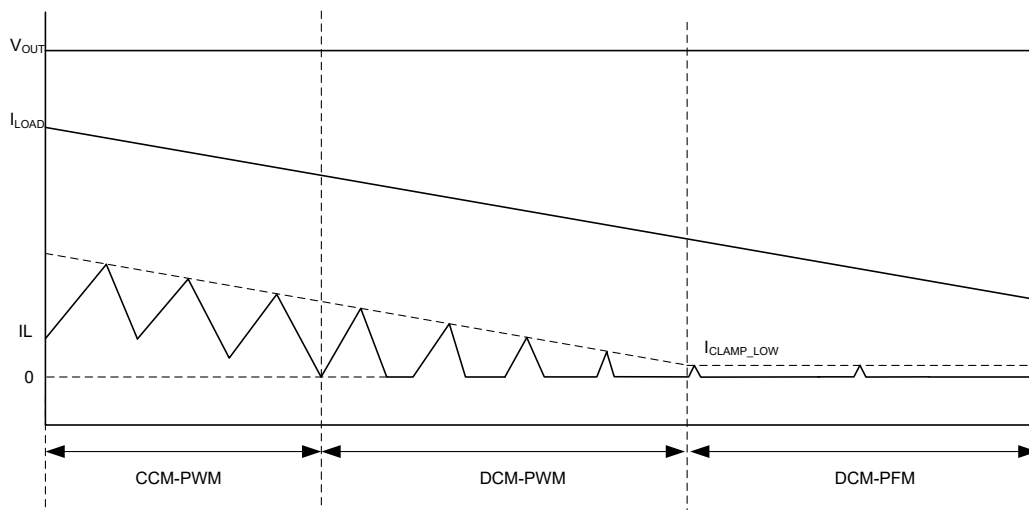


图 7-1. TLV61047 Functional Modes

8 Application and Implementation

注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

TLV61047 is a boost DC/DC converter integrating a power switch and loop compensation circuits. The device has input range from 2.6V to 20V, with output voltage covers up to 28V. The TLV61047 adopts the current-mode control with adaptive constant off-time. The switching frequency is quasi-constant and internally set to either 1.6MHz (TLV61047) or 0.6MHz (TLV610471) allowing the use of extremely small surface mount inductor and capacitors. The following design procedure can be used to select component values for the TLV61047.

8.2 Typical Applications

8.2.1 12V Output Boost Converter

In this design example, TLV61047 V_{OUT} is configured as 12V with a input source from 2.6V to 9V.

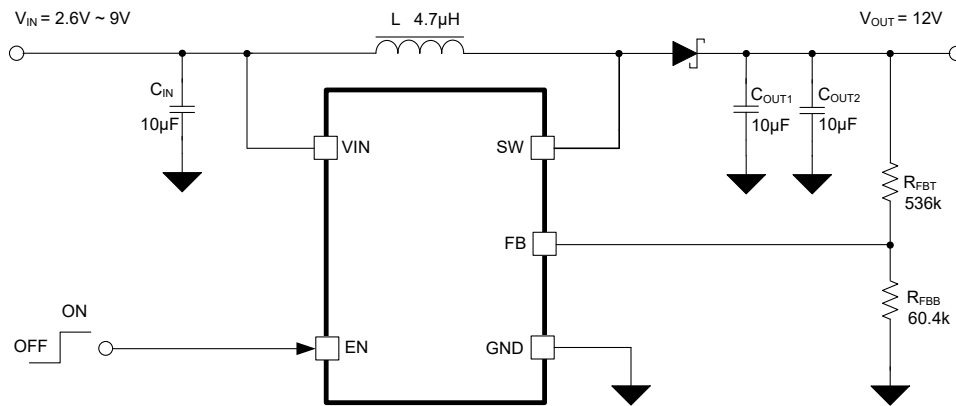


図 8-1. Typical 12V Application

8.2.1.1 Design Requirements

For this design example, the parameters are shown in 表 8-1:

表 8-1. Design Requirements

PARAMETERS	VALUE
Input voltage	2.6V to 9V
Output voltage	12V
Frequency	1.6MHz
Output current	0 - 600mA (When $V_{IN} \geq 5V$)

8.2.1.2 Detailed Design Procedure

8.2.1.2.1 Programming the Output Voltage

Output voltage is programmed via external resistor divider. By selecting the external resistor divider R_{FBT} and R_{FBB} , as shown in 図 8-1, the output voltage is programmed to the desired value. When the output voltage is regulated, the typical voltage at the FB pin is V_{REF} of 1.233V.

$$R_{FBT} = \left(\frac{V_{OUT}}{V_{REF}} - 1 \right) \times R_{FBB} \quad (1)$$

where

- V_{OUT} is the desired output voltage
- V_{REF} is the internal reference voltage at the FB pin

For best accuracy, R_{FBB} should be kept smaller than 150k Ω to ensure the current flowing through R_{FBB} is at least 100 times larger than the FB pin leakage current. Changing R_{FBB} towards a lower value increases the immunity against noise injection. Changing the R_{FBB} towards a higher value reduces the quiescent current for achieving higher efficiency at low load currents.

8.2.1.2.2 Inductor Selection

Because the selection of the inductor affects steady state operation, transient behavior, and loop stability, the inductor is the most important component in power regulator design. There are three important inductor specifications, inductor value, saturation current, and DC resistance (DCR). The TLV61047 is designed to work with inductor values between 2.2 μ H and 10 μ H. Use 式 2 to 式 4 to calculate the peak current of the application inductor. To calculate the current in the worst case, use the minimum input voltage, maximum output voltage, and maximum load current of the application. To have enough design margin, choose the inductor value with – 30% tolerance, and a low power-conversion efficiency for the calculation. In a boost regulator, the inductor dc current can be calculated with 式 2.

$$I_{L(DC)} = \frac{V_{OUT} \times I_{OUT}}{V_{IN} \times \eta} \quad (2)$$

where

- V_{OUT} = output voltage
- I_{OUT} = output current
- V_{IN} = input voltage
- η = power conversion efficiency, use 80% for most applications

The inductor ripple current is calculated with the with the equation below for an asynchronous boost converter in continuous conduction mode (CCM).

$$\Delta I_{L(P-P)} = \frac{V_{IN} \times (V_{OUT} + V_D - V_{IN})}{L \times f_{SW} \times (V_{OUT} + V_D)} \quad (3)$$

where

- $\Delta I_{L(P-P)}$ = inductor ripple current
- L = inductor value
- f_{SW} = switching frequency
- V_{OUT} = output voltage
- V_{IN} = input voltage
- V_D = the forward voltage of the Schottky diode

Therefore, the inductor peak current is calculated with the below equation.

$$I_{L(P)} = I_{L(DC)} + \frac{\Delta I_{L(P-P)}}{2} \quad (4)$$

Normally, it is advisable to work with an inductor peak-to-peak current of less than 40% of the average inductor current for maximum output current. A smaller ripple from a larger valued inductor reduces the magnetic hysteresis losses in the inductor and EMI. However, in the same way, load transient response time is increased. 表 8-2 lists the recommended inductor for the TLV61047 in the 1.6MHz configuration.

表 8-2. Recommended Inductors for the TLV61047 at 1.6MHz Configuration

PART NUMBER	L (μH)	DCR MAX (mΩ)	SATURATION CURRENT TYPICAL (A)	SIZE (L×W×H) (mm)	VENDOR ⁽¹⁾
SWPA5040S4R7NT	4.7	39	3.9	5 × 5 × 4	Sunlord
XAL4030-472ME	4.7	44.1	4.5	4 × 4 × 3	Coilcraft
SWPA5040S100MT	10	83	2.9	5 × 5 × 4	Sunlord
XAL4040-103ME	10	92.4	3	4 × 4 × 4	Coilcraft

(1) See [Third-party Products Disclaimer](#)

8.2.1.2.3 Input and Output Capacitor Selection

The output capacitor is mainly selected to meet the requirements for output ripple and loop stability. This ripple voltage is related to the capacitor's capacitance and its equivalent series resistance (ESR). Assuming a ceramic capacitor with zero ESR, the minimum capacitance needed for a given ripple can be calculated by 式 5:

$$C_{OUT} = \frac{I_{OUT} \times D_{MAX}}{f_{SW} \times V_{RIPPLE}} \quad (5)$$

where

- D_{MAX} = maximum switching duty cycle
- V_{RIPPLE} = peak to peak output voltage ripple

The ESR impact on the output ripple must be considered if tantalum or aluminum electrolytic capacitors are used.

Take care when evaluating the derating of a ceramic capacitor under DC bias, aging, and AC signal. For example, the DC bias can significantly reduce capacitance. A ceramic capacitor can lose more than 50% of its capacitance at its rated voltage. Therefore, always leave margin on the voltage rating to ensure adequate capacitance at the required output voltage.

TI recommends using the output capacitor with effective capacitance 10μF, which covers the major applications. TI also recommends placing a small 1μF capacitor right across the rectifier diode cathode to the GND pin of the TLV61047 to reduce the high RMS current loop's inductance. The output capacitor affects the small signal control loop stability of the boost regulator. If the output capacitor is below the range, the boost regulator can potentially become unstable. Increasing the output capacitor makes the output voltage ripple smaller in PWM mode. 表 8-3 lists the recommended capacitor for the TLV61047.

表 8-3. Recommended Output Capacitors for the TLV61047

PART NUMBER	C _{OUT} (μF)	RATING	PACKAGE	VENDOR ⁽¹⁾
TMK316BLD106KL	10	25 V, X5R	1206	Taiyo Yuden
CC1206KKX5R8BB106	10	25 V, X5R	1206	Yageo
CGA5L1X7R1H106K160AC	10	50V, X7R	1206	TDK

(1) See [Third-party Products Disclaimer](#).

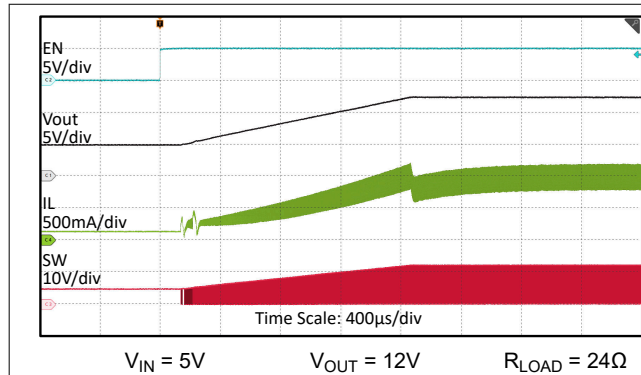
The ceramic capacitors are an excellent choice for the input decoupling of the step-up converter since they have extremely low ESR and are available in small footprints. Input capacitors must be located as close as possible to the device. While a 10μF input capacitor or equivalent is sufficient for the most applications, larger values can be used to reduce input current ripple.

Take care when using only ceramic input capacitors. When a ceramic capacitor is used at the input and the power is being supplied through long wires, such as from a wall adapter, a load step at the output can induce ringing at the VIN pin. This ringing can couple to the output and be mistaken as loop instability or can even damage the device. Additional "bulk" capacitor (electrolytic or tantalum) in this circumstance, must be placed between C_{IN} and the power source lead to reduce ringing that can occur between the inductance of the power source leads and C_{IN}.

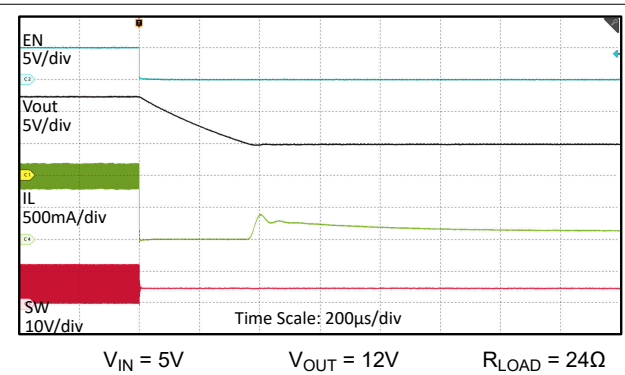
8.2.1.2.4 Diode Rectifier Selection

A Schottky diode is the preferred type due to its low forward voltage drop and small reverse recovery charge. Low reverse leakage current is important parameter when selecting the Schottky diode. The diode must be rated to handle the maximum output voltage plus any switching node ringing. Also, it must be able to handle the average output current.

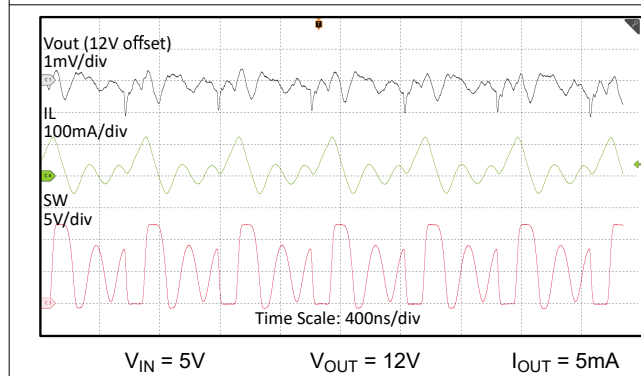
8.2.1.3 Application Curves



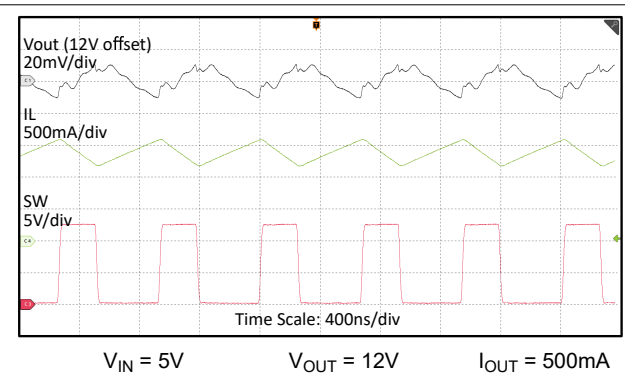
8-2. Start-up by EN Waveforms



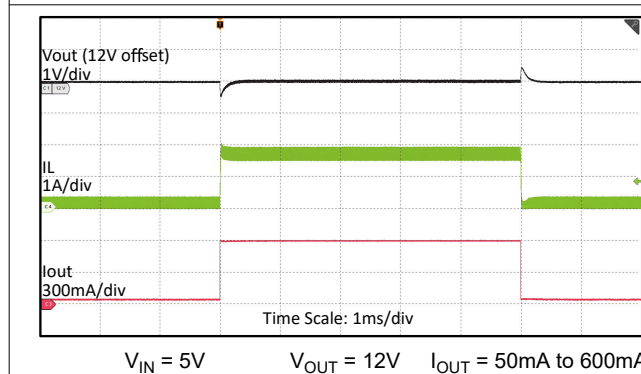
8-3. Shutdown by EN Waveforms



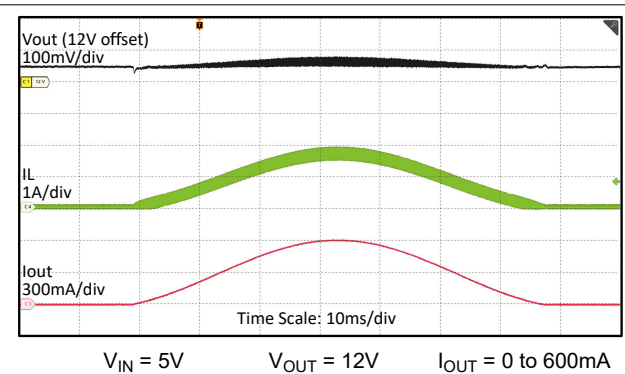
8-4. Switching Waveforms in Steady State



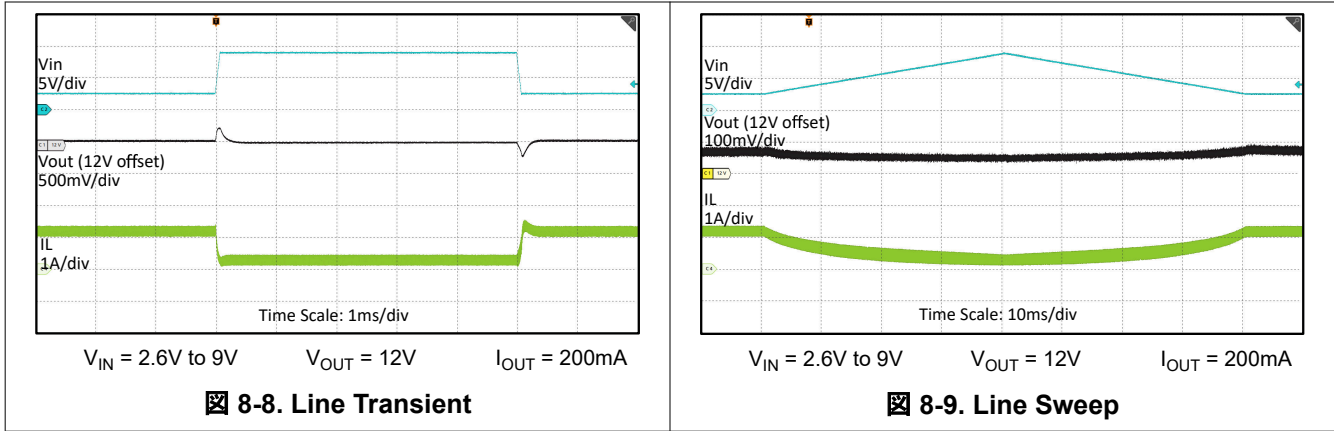
8-5. Switching Waveforms in Steady State



8-6. Load Transient

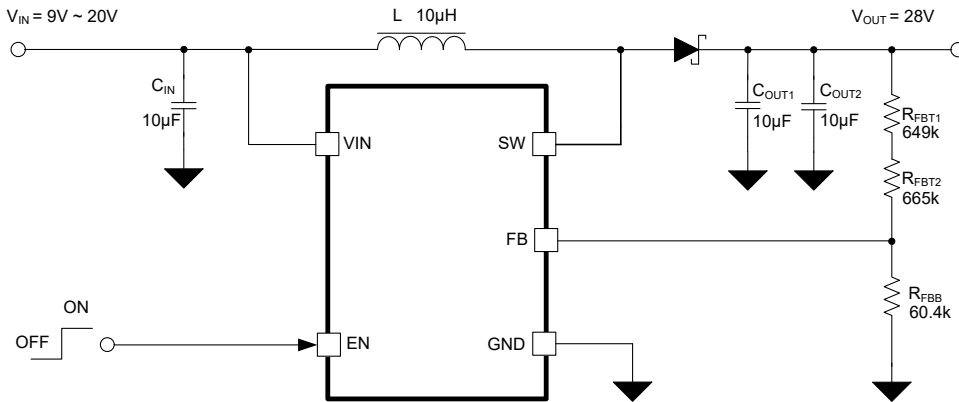


8-7. Load Sweep



8.2.2 28V Output Boost Converter

In this design example, TLV61047 V_{OUT} is configured as 28V with a input source from 9V to 20V. The principles of the components selection, including the inductor, input and output capacitors diode are the same with those in the example of [12V Output Boost Converter](#).



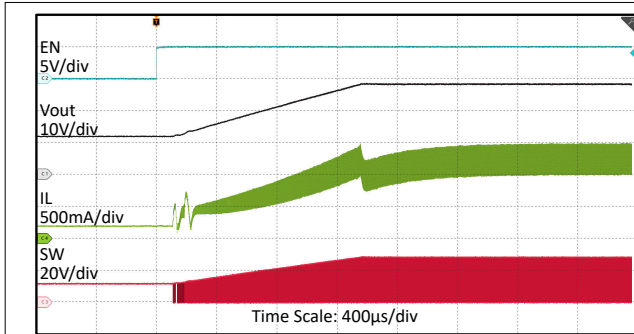
8-10. Typical 28V Application

8.2.2.1 Design Requirements

表 8-4. Design Requirements

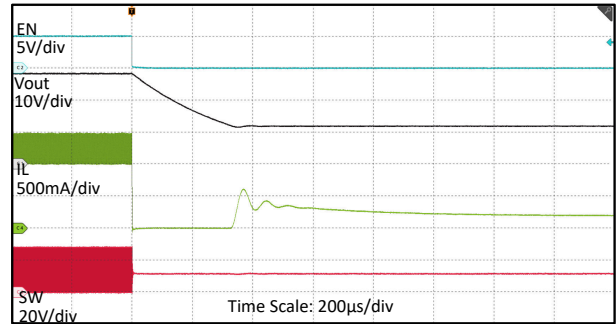
PARAMETER	VALUE
Input voltage	9V to 20V
Output voltage	28V
Frequency	1.6MHz
Output current	0 to 600mA (When $V_{IN} \geq 12V$)

8.2.2.2 Application Curves



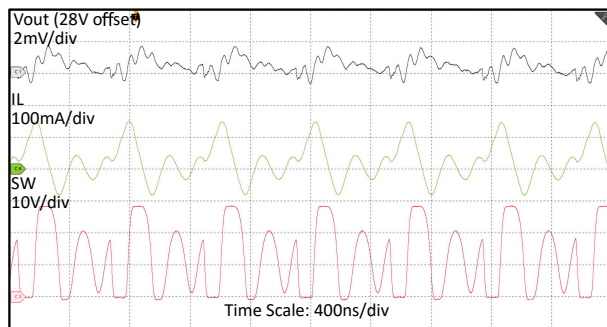
$V_{IN} = 12V$ $V_{OUT} = 28V$ $R_{LOAD} = 56\Omega$

8-11. Start-up by EN Waveforms



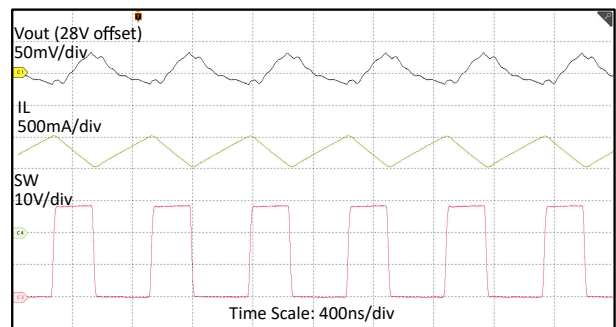
$V_{IN} = 12V$ $V_{OUT} = 28V$ $R_{LOAD} = 56\Omega$

8-12. Shutdown by EN Waveforms



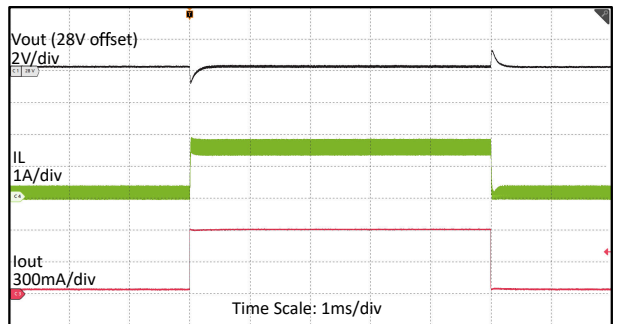
$V_{IN} = 12V$ $V_{OUT} = 28V$ $I_{OUT} = 5mA$

8-13. Switching Waveforms in Steady State



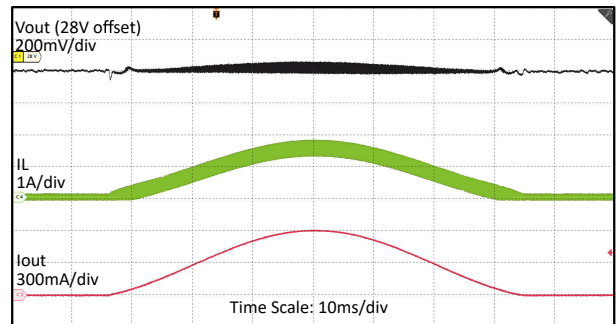
$V_{IN} = 12V$ $V_{OUT} = 28V$ $I_{OUT} = 500mA$

8-14. Switching Waveforms in Steady State



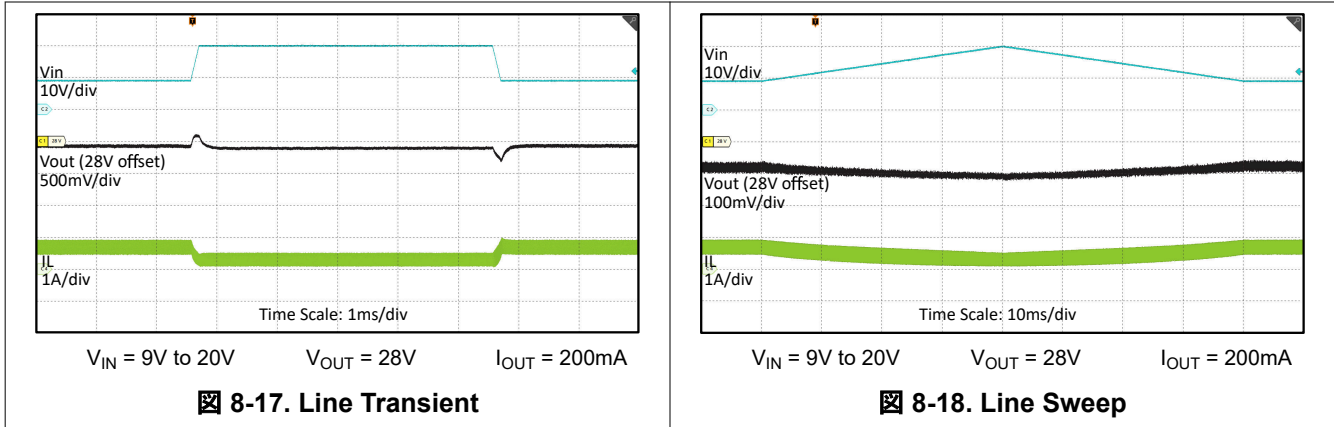
$V_{IN} = 12V$ $V_{OUT} = 28V$ $I_{OUT} = 50mA$ to $600mA$

8-15. Load Transient



$V_{IN} = 12V$ $V_{OUT} = 28V$ $I_{OUT} = 0$ to $600mA$

8-16. Load Sweep



8.3 Power Supply Recommendations

The device is designed to operate from an input voltage supply range between 2.6V to 20V. This input supply must be well regulated. If the input supply is located more than a few inches from the converter, additional bulk capacitance may be required in addition to the ceramic bypass capacitors. A typical choice is an electrolytic or tantalum capacitor with a value of 47 μ F. Output current of the input power supply must be rated according to the supply voltage, output voltage and output current of the TLV61047.

8.4 Layout

8.4.1 Layout Guidelines

As for all switching power supplies, especially those running at high switching frequency and high currents, layout is an important design step. If the layout is not carefully done, the regulator could suffer from instability and noise problems. To maximize efficiency, switch rise and fall time are very fast. To prevent radiation of high frequency noise (for example, EMI), proper layout of the high-frequency switching path is essential. Minimize the length and area of all traces connected to the SW pin, and always use a ground plane under the switching regulator to minimize interplane coupling. The input capacitor must not only be close to the VIN pin, but also to the GND pin in order to reduce input supply ripple.

The most critical current path for all boost converters is from the switching FET, through the rectifier diode, then the output capacitors, and back to ground of the switching FET. This high current path contains nanosecond rise and fall time and must be kept as short as possible. Therefore, the output capacitor must not only be close to the GND pin, but also to the cathode of the high side rectifier to reduce the overshoot at the SW pin.

8.4.2 Layout Example

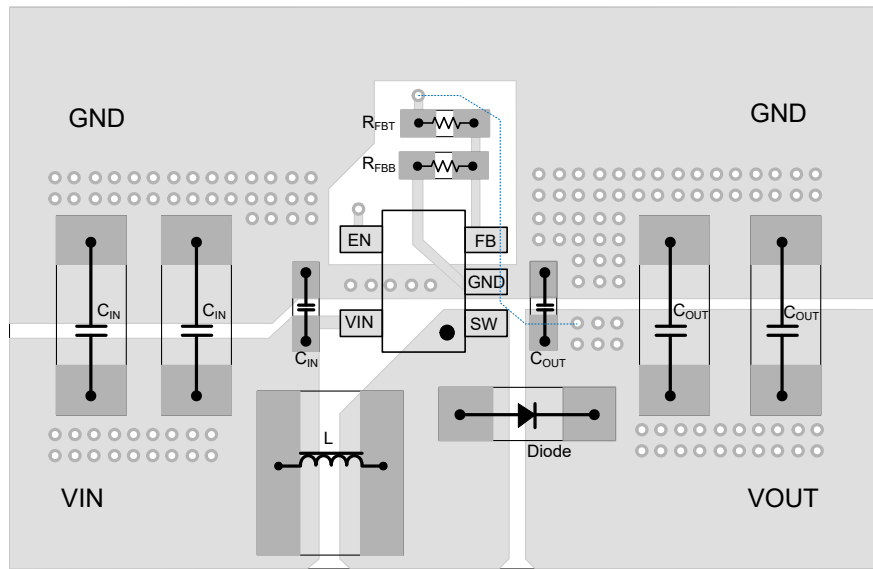


図 8-19. TLV61047 Layout

9 Device and Documentation Support

9.1 Device Support

9.1.1 サード・パーティ製品に関する免責事項

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9.2 Receiving Notification of Documentation Updates

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9.6 用語集

[テキサス・インスツルメンツ用語集](#) この用語集には、用語や略語の一覧および定義が記載されています。

10 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

Changes from Revision * (July 2019) to Revision A (January 2025)	Page
• 量産データのリリースを代表的特性曲線に変更。.....	1
• Updated Max 22 to 20.5.....	4

DATE	REVISION	NOTES
November 2024	*	Initial release

11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TLV61047DDCR	ACTIVE	SOT-23-THIN	DDC	5	3000	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 125	047	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSELETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

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(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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TAPE AND REEL INFORMATION

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV61047DDCR	SOT-23-THIN	DDC	5	3000	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3

TAPE AND REEL BOX DIMENSIONS


*All dimensions are nominal

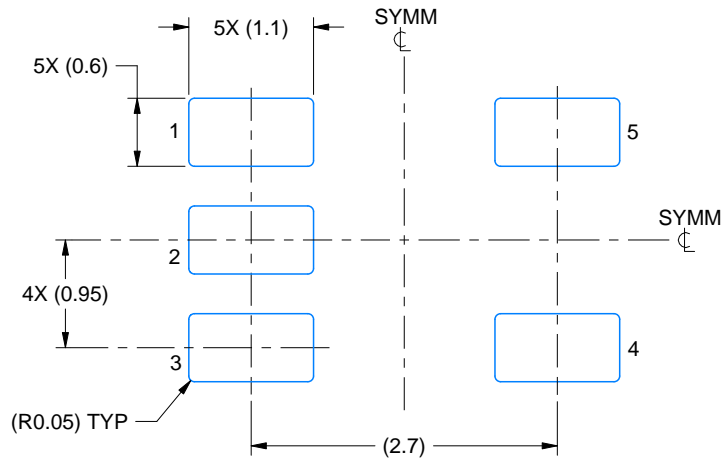
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV61047DDCR	SOT-23-THIN	DDC	5	3000	210.0	185.0	35.0

EXAMPLE BOARD LAYOUT

DDC0005A

SOT-23 - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE
EXPLODED METAL SHOWN
SCALE:15X



SOLDERMASK DETAILS

4220752/C 08/2024

NOTES: (continued)

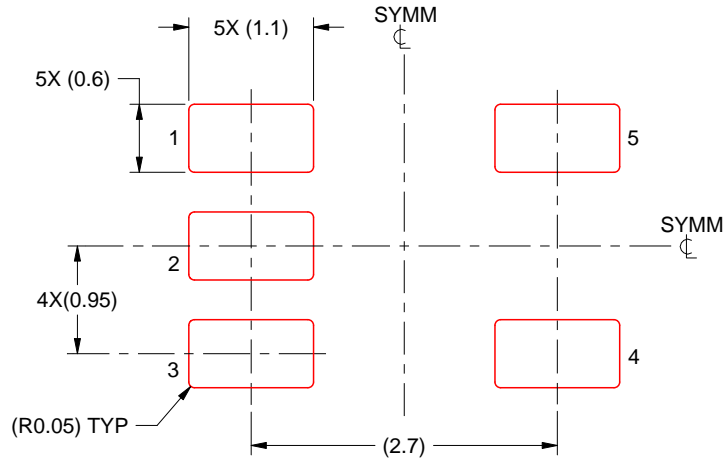
- 4. Publication IPC-7351 may have alternate designs.
- 5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

DDC0005A

SOT-23 - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE
BASED ON 0.125 THICK STENCIL
SCALE:15X

4220752/C 08/2024

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
7. Board assembly site may have different recommendations for stencil design.

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