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Part number **LM3445MM**
Project Title **9W Retrofit Triac dimming**
Project Number **NSCE0144**

Title		Off line Triac dimmer with 6 LEDs
Description	Input	230V _{AC}
	Output	6 LEDs @ 350 mA
	Power	9W
	Freq.	45 kHz
Date		[2009-10-15]
Revision		[2.0]



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1 Introduction

This technical report describes the retrofit power supply.

The main purpose of the power supply is to convert the rectified AC Input to DC regulated current for 6 LEDs. The power supply provides protection for the LEDs, limits the transient input voltage and protect against inrush current at plug in. The overall power supply conformity (e.g. mains harmonics (EN), mains interference, international safety standards etc.) are not approved for all the applicable European Norms (EN).

The principle of this power supply is a step down. It is regulated by the 350 mCE average current with a fixed Toff time.

At the heart of the power supply is the controller LM3445 current mode control from National Semiconductor. The LM3445 switching frequency is set at a nominal 45 kHz.

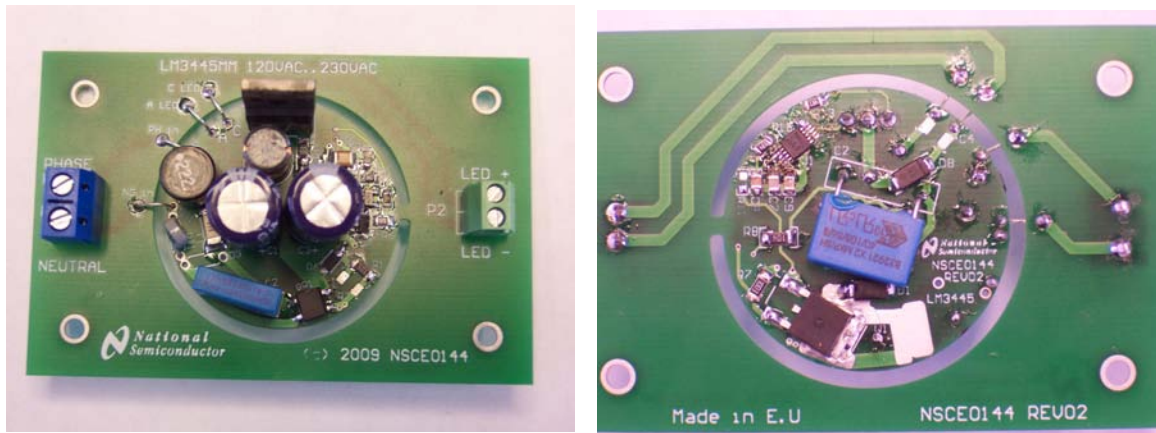
With the LM3445 National Semiconductor provides a device that avoids visible flickering caused by a TRIAC forward or reverse phase dimmer. The LM3445 overcomes this challenge by translating the TRIAC-chopped waveform to a DIM signal and decoding it to a DC signal. In fact, the LED current is linearly regulated according to the dimming signal.

The LM3445 integrates many features to simplify the compatibility with Triac dimmer:

- Triac dim decoder circuit for LED dimming
- Adjustable switching frequency
- Low quiescent current
- Triac dim decoder circuit for LED dimming
- Adaptive programmable off-time allows for constant ripple current
- Thermal shutdown
- No 100Hz flicker
- Patent pending drive architecture

The report includes schematic, design description, bill of materials listing as well as a full set of performance measurements taken from a prototype unit.

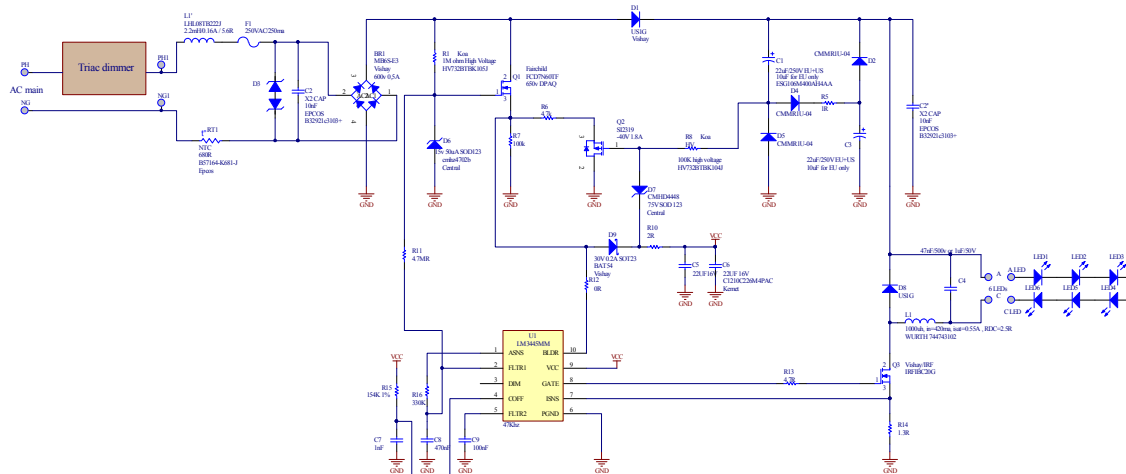
Figure 1:



This LED retrofit power supply is used with a standard Triac dimmer. The LM3445 contains all the necessary circuitry to build a line powered (mains powered) constant current LED driver whose output current can be controlled with a conventional triac dimmer.

The main source can be either 120V_{AC} (60Hz), 240V_{AC} (50Hz) or both, it is only matter of Electrolytic capacitor at the input stage.

Figure 2 shows a diagram of the Triac dimmer, LED Driver and the 7 W retrofit LEDs.



2 Specifications

Specification	Model	NSCE0144
	Max input power (W) DC Output current Nb of LEDs LEDs	9W 350mA 6
Input	Voltage (AC) PF Efficiency (%)	180V_{AC}265 V_{AC} 0.92 77.7%
Output	Voltage (VF) Current (A) Ripple (mA _{pp}) Start up time (ms) Hold up time (input failure) Remote sensing Remote on/off	19V +/-20% 0.350A 400mA 10ms (V_{AC}=230V_{AC}, I_{out}=100%) 28ms @ 100% load Forward Triac dimmer Yes, ON/OFF switch
Isolation	Input/output	No
Standards	Safety Agency approvals IEC 61000-3-2 CLASS C EN55022 conduction EN55022 radiation	No Yes No, over the limit No, not measured
Other	cooling method Temperature range	Non -25°C to +65°C

Maximum component height is 25mm. The overall size area is 35mm diameter.

3 Basic Theory

3.1 Converter Theory

One of the main points is the angle detect and Dim decoder to translate the trigger point into a dc current. National Semiconductor has introduced the LM3445 LED driver that integrates most of these functions needed to translate a TRIAC dimmer angle into an average current running through a number of LEDs. On the schematic **figure 5**, on the top left side we see the entry point for the AC signal, this AC signal is first rectified using a diode bridge. Then is translated to a lower voltage level by a bleeder circuit and is fed to the BLDR pin of the LM3445.

The external bleeder circuit translates the rectified signal to a lower voltage level signal via R1, R2, Q1, D6 and is fed to the BLDR pin of the LM3445. The main function of R7 is to ensure that a minimal amount of current is drawn even at light loads, to make sure the TRIAC in the dimmer remains conductive.

When the valley fill circuit composed by C1, C3, D2, D4, D5 and R5 is drawing current from the line (bulk capacitors charging in series) there is plenty of input line current holding the TRIAC on state. When the valley fill circuit stops charging the capacitors, the output power (LED current) is being delivered by the bulk capacitors, and the line current through the TRIAC became very small. A simple Circuit composed by R6, Q2, D7 and R8 is used to add holding current when valley fill diodes D2, D5 are conducting.

This simple circuit will reduce the power consumption of the holding circuit (Q1) and increase the overall efficiency.

The valley-fill circuit is used to avoid high peak current during charge of the input bulk capacitor. This high input current seen in the 230V line generates high harmonics distortion and therefore is an obstacle to meet the European standard EN-61000-3-2 class C and has a poor power factor. To avoid this, a valley-fill circuit is used.

To be in line with the UL safety standard norm, we implemented a varistor protection on the primary side to absorb any high peak voltages. At plug in, the input voltage charges the input capacitors C1 and C3 with a low peak current due to the inrush current limiter RT1.

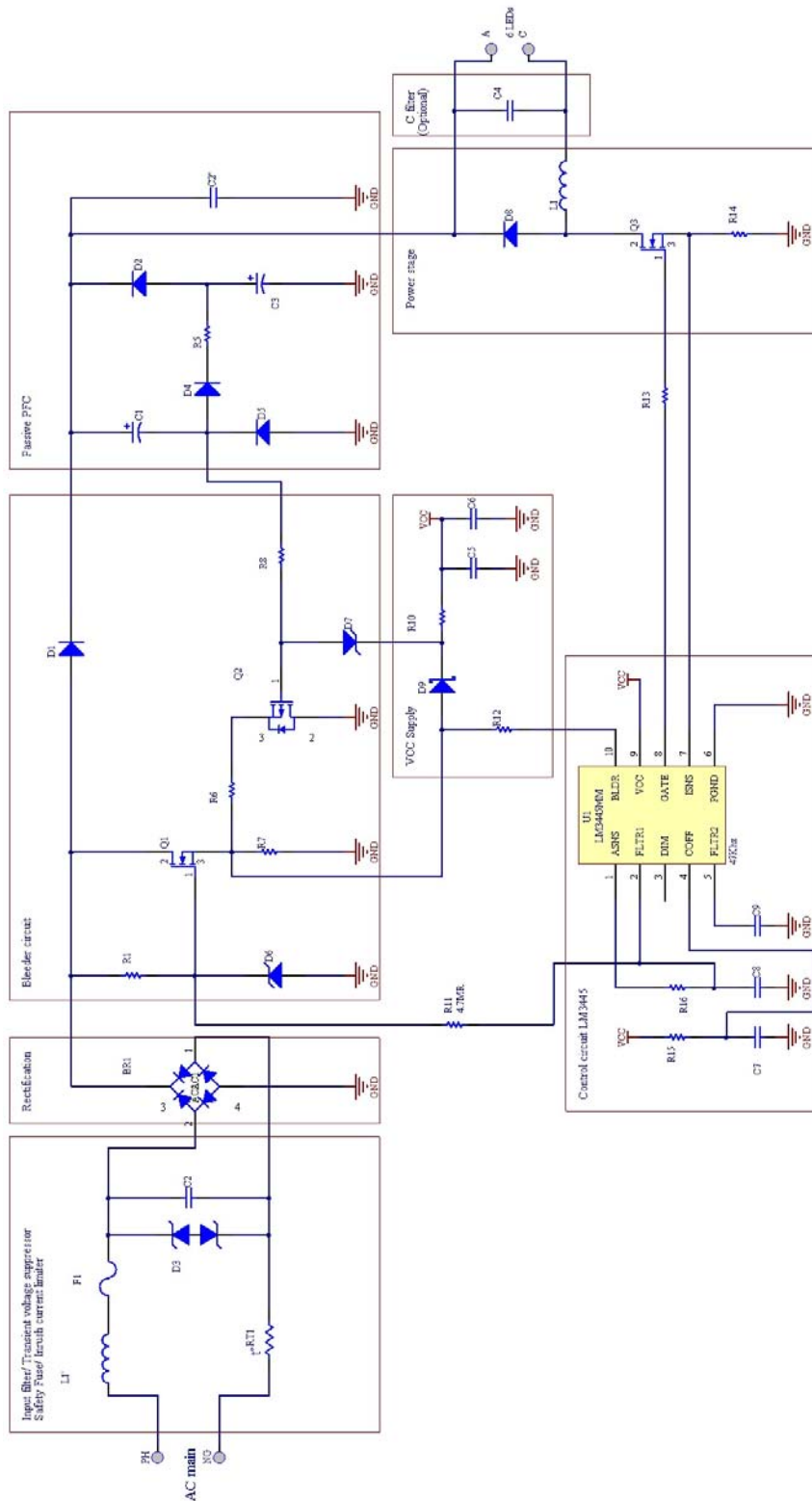
The cycle by cycle current limitation controls the maximum power in case of short circuit or an excessive load. If the voltage across R14 rises above 1.27V, the PWM uses this information to terminate the Mosfet conduction. A delay circuit will prevent the start of another cycle for 180 μ s.

In case of open LEDs, the voltage across the capacitor C4 will become higher and clamp to the input voltage, this capacitor has been selected to support 500V.

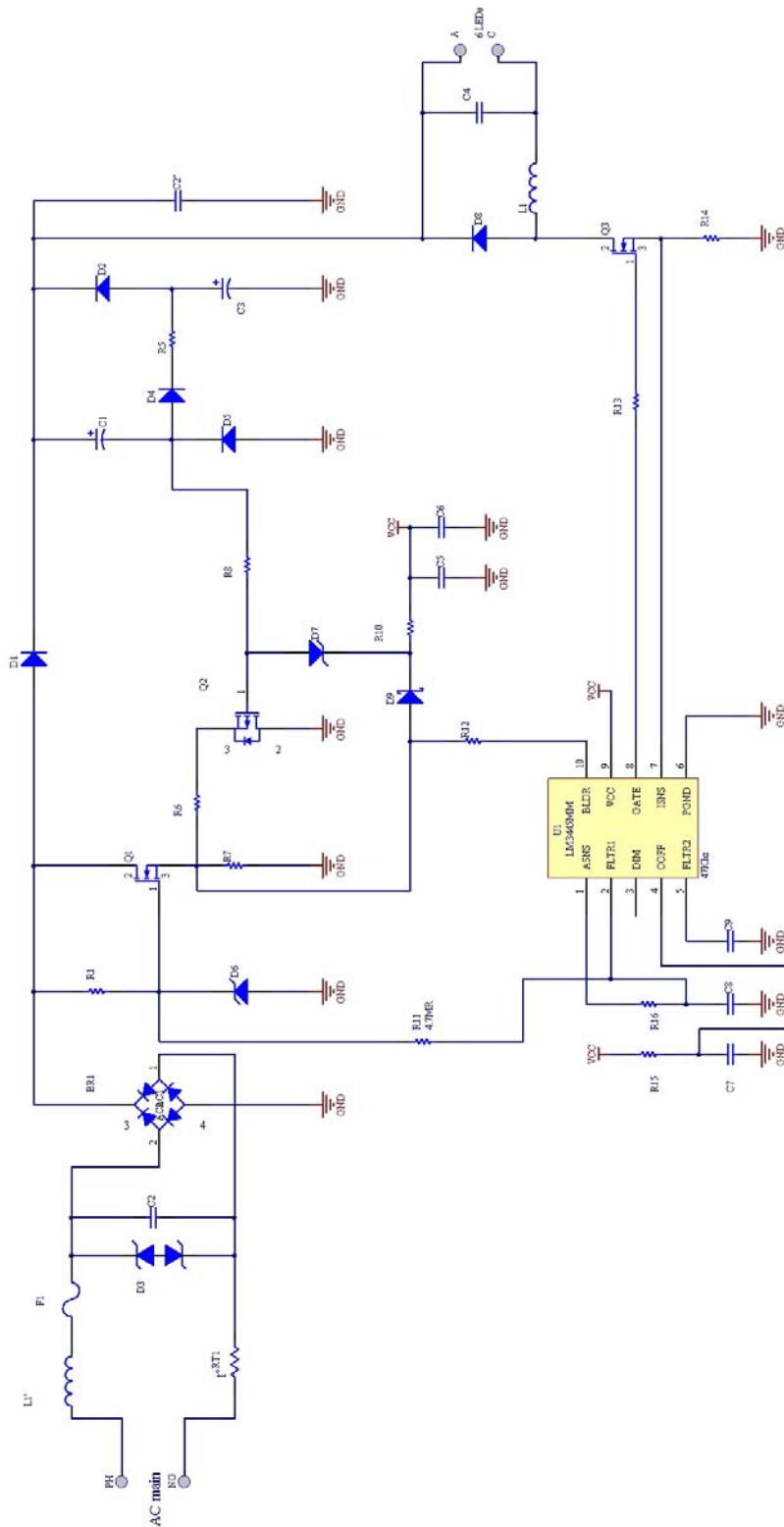
The mains filter is located at the input, consisting of L1' and C2 used to fulfill the EN55022 norm. This filter is necessary to minimize interference transmission from the power supply to the mains and vice versa. The switching frequency has been adjusted close to 50 kHz to keep an easy input filter.

This converter will operate in continuous conduction mode at full power and discontinuous mode at low power during dimming. To eliminate most of the ripple current seen in the inductor, it is possible to have a $1\ \mu\text{F}$ capacitor in parallel to C4. This LED driver uses a constant off-time control to regulate current through a string of LEDs. The resistor R15 and capacitor C7 create a constant current ramp which is fed into the C_{off} pin and thus generates the T_{off} time. While Mosfet Q3 is conducting, the LED current increases through the inductance until reaching the reference FLTR2 fixed by the TRIAC dimmer. With this reference peak current reached the Mosfet turns OFF and diode D8 conducts during the period T_{off} . That means by varying FLTR2 pin (reference) by the TRIAC dimming, the current through the LED is varying. Hence we achieve dimming.

4 Block diagram



5 Schematic



6 Bill of Materials

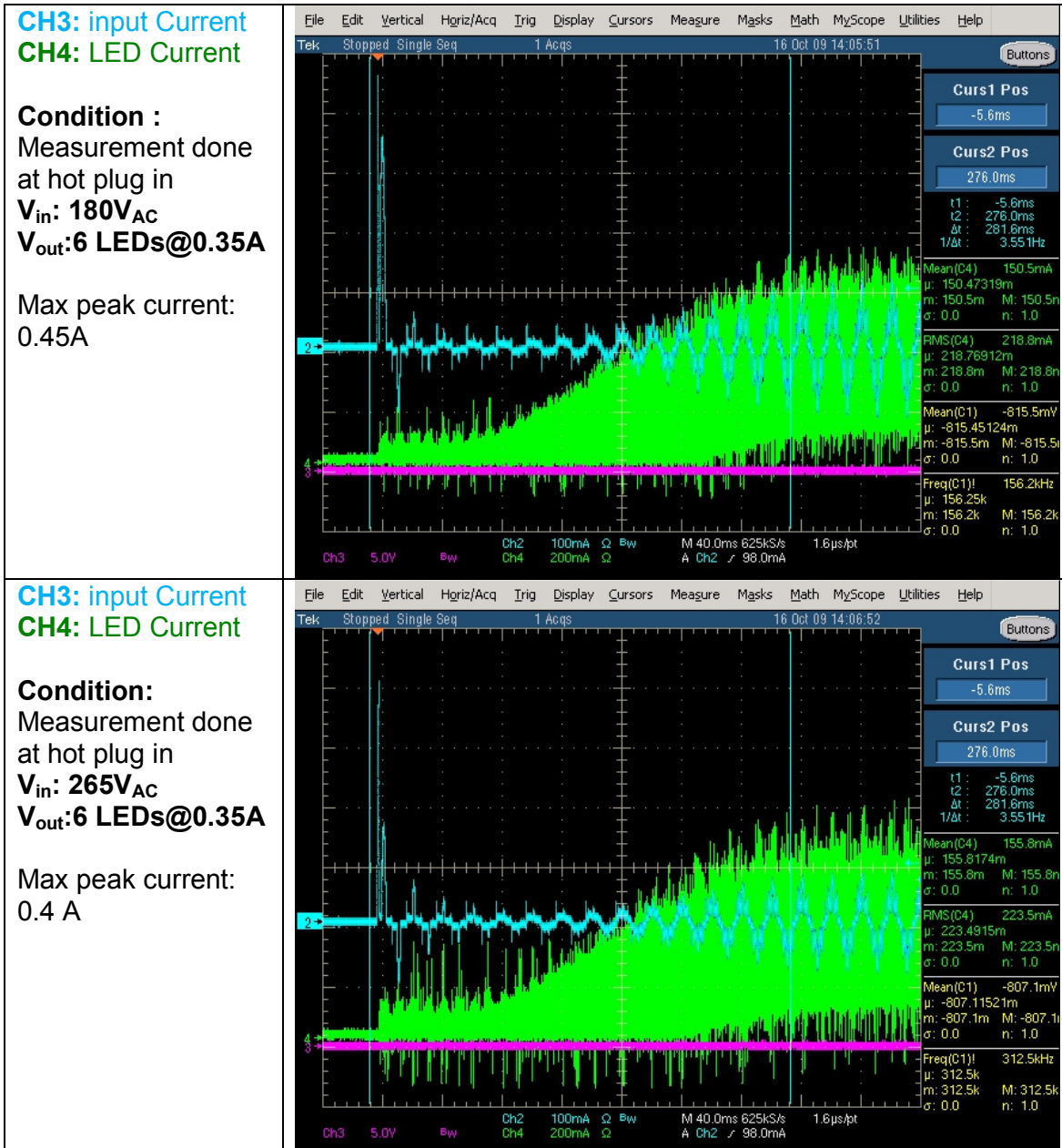
Document P/N: 980None		NSCE0144		Free Documents		National Semiconductor			
Project Name:		Base ID:		PCB Revision:		Assembly Variant:			
NSCE0144		Free Documents		2 nd		None			
Project File:		Schematic Rev:		Build Quantity:		Generated:			
10/16/2009		Rev03		1		10/12/2009 1:58:16 PM			
Time opened:		10/27 51 AM							
Item	Designator	Value	Part Number	Manufacturer	Supplier	2nd sources	Manufacturer	Quantity	Required
1	BRT	600V/0.5A	1MBSES-E3	Vishay	Burklin		Acrotronic	1	1
2	C1	22uF / 250V / EKA / 85deg	12D5238	Vishay / Roederstein EKA	Burklin		ESK226M250AH4AA	1	1
3	C2	10nF 350VAC X2	B32921c3103+	Esocos				1	1
4	C2*	10nF 350VAC X2	B32921c3103+	Esocos				1	1
5	C3	22uF / 250V / EKA / 85deg	12D5238	Vishay / Roederstein EKA	Burklin		ESK226M250AH4AA	1	1
6	C4	47nF/500V or 1uF/50V or NC	C1210C105K5RAC	Kemet				1	1
7	C5	22uF 16V/1210	C1210C226M4PAC	Kemet				1	1
8	C6	22uF 16V/1210	C1210C226M4PAC	Kemet				1	1
9	C7	1nF / 100V	C0805C102JTRAC	Kemet				1	1
10	C8	470nF 25V	C0805C474K3RAC	Kemet				1	1
11	C9	100nF / 50V	C0805C104K5RAC	Kemet				1	1
12	D1	400V / 1A / SMA	US1G	Vishay				1	1
13	D2	400V / 1A / SOT123 ULTRAFAST	CMR1U-04	Central				1	1
14	D3	V390ZA05	846-8204	Harris Semiconductor	RS-ONLINE			1	1
15	D4	400V / 1A / SOT123 ULTRAFAST	CMR1U-04	Central				1	1
16	D6	400V / 1A / SOT123 ULTRAFAST	CMR1U-04	Central				1	1
17	D6	15v 50uA SOD123	cm1z4702b	Central				1	1
18	D7	75V SOD 123	CMFD448	Central				1	1
19	D8	400V / 1A / SMA	US1G	Vishay				1	1
20	D9	BAT54	BAT54	Faichild				1	1
21	F1	30V 0.2A SOT 23 shottky	54718-11	ESKA	Conrad			1	1
22	L1	SMD SSQF 250ma FUSE	744743102	Wurth				1	1
23	L1*	WURTH 744743102	LHL08TB472J	tayo.yuden				1	1
24	Q1	4.7mH0.1A / 14R	FCDT160TF	Faichild	RM-GMBH			1	1
25	Q2	650V DPAC	SI2319	Vishay-Siliconix				1	1
26	Q3	40V 1.6A	IRF1BC20G	Vishay				1	1
27	R1	600V 3A DPAC	HV732ETBK105J	Koa				1	1
28	R5	1M ohm High Voltage 1206	YAGEO					1	1
29	R6	1R / 5% / 1206	YAGEO					1	1
30	R7	3.3k / 5% / 0805	YAGEO					1	1
31	R8	100k / 5% / 1206	YAGEO					1	1
32	R10	100K high voltage 1206	HV732ETBK104J	Koa				1	1
33	R11	2R / 5% / 0805	YAGEO					1	1
34	R12	NC						1	1
35	R13	0R / 5% / 0805	YAGEO					1	1
36	R14	1R / 5% / 0805	YAGEO					1	1
37	R15	1.3R / 1% / 1206	WISHAY					1	1
38	R16	154K / 1% / 0805	WISHAY					1	1
39	RT1	330K / 5% / 0805	YAGEO					1	1
40	U1	680R 5%	B577164-K681-J	Esocos				1	1
			LM334G3MM	NATIONAL SEMICONDUCTOR				1	1

7 Start up phase

7.1 Plug in into the network line

At plug in, the input voltage charges the input capacitor with a low peak current due to the DCR of the input filter and the NTC.

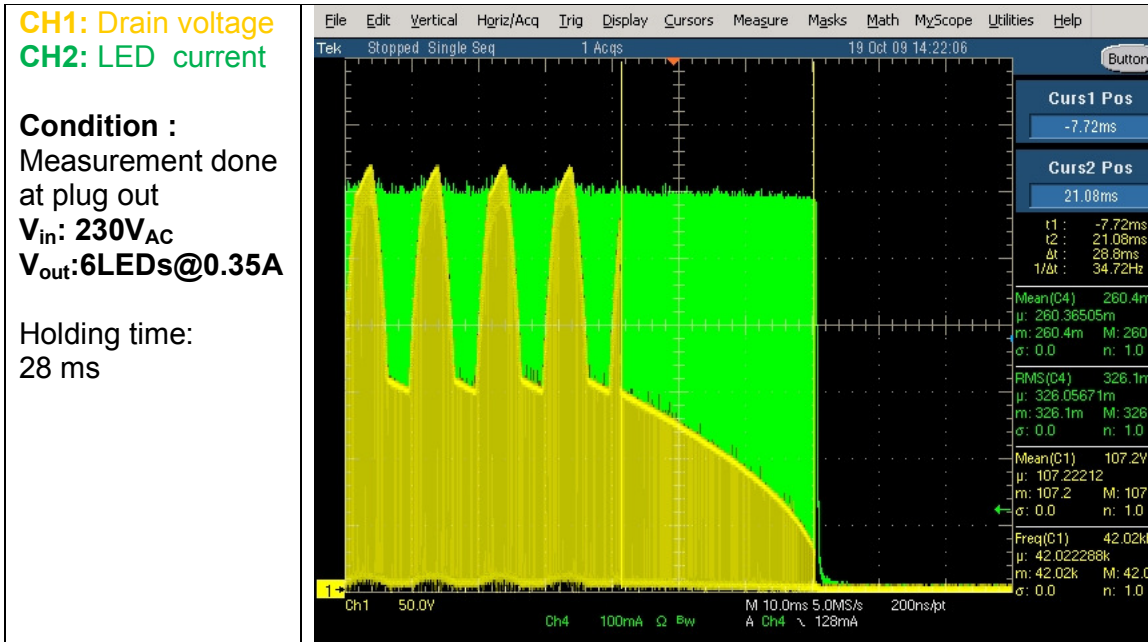
As soon as the voltage on the pin 9 reaches the voltage threshold of the VCC, the device turns into active mode and start switching.



7.2 Holding time

The LED current must wait at least this minimum time before switching off the AC/DC converters. This is to ensure that any peak current is seen in the main during main disturbances.

The following plot shows the timing between the plug out and LED current off with V_{in} 230VAC.



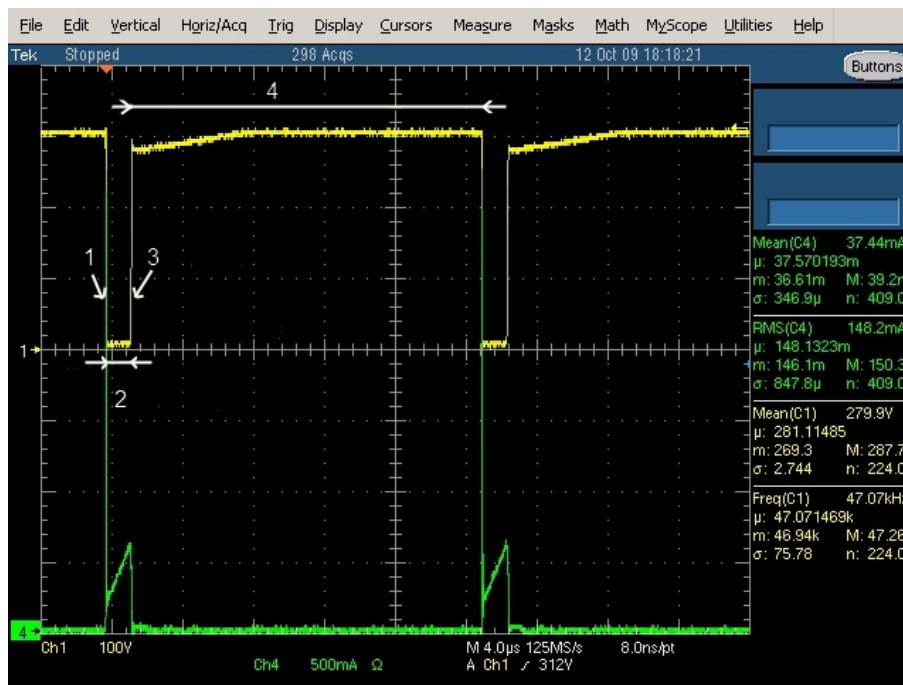
8 Measurement

8.1 One complete cycle:

This plot shows in detail the drain source voltage and drain current of Q3 for one complete cycle in on mode.

The cycle can be divided into different phases as shown on the plot:

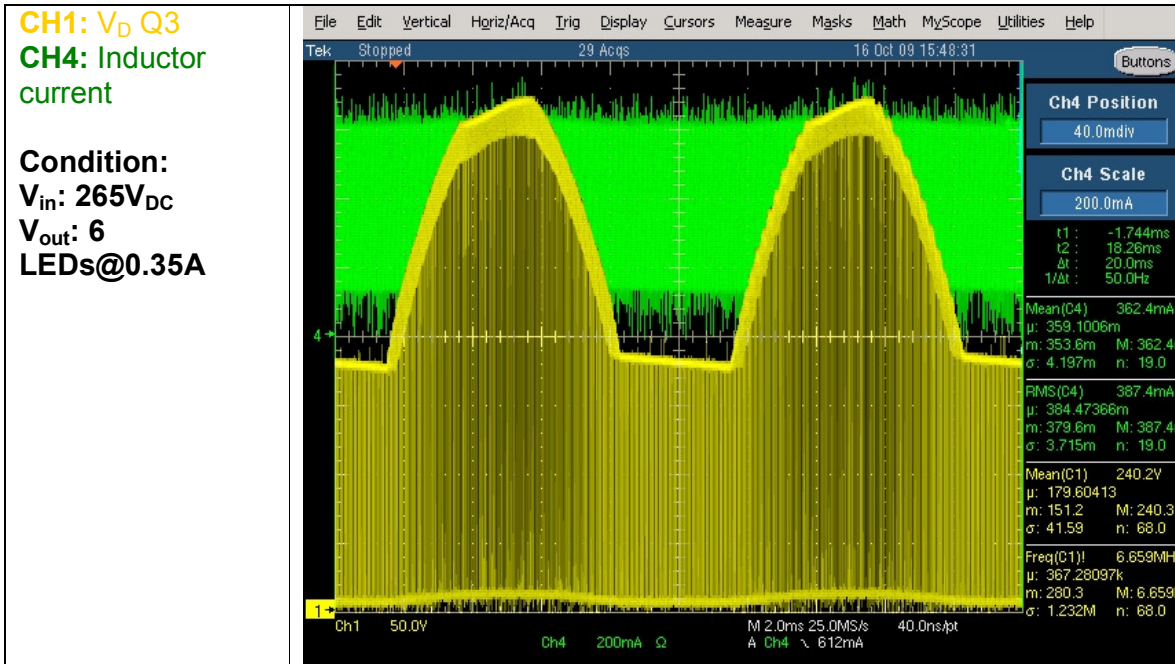
1. Switch on phase
2. Conducting phase
3. Switch off phase
4. Off phase, Energy released into the load



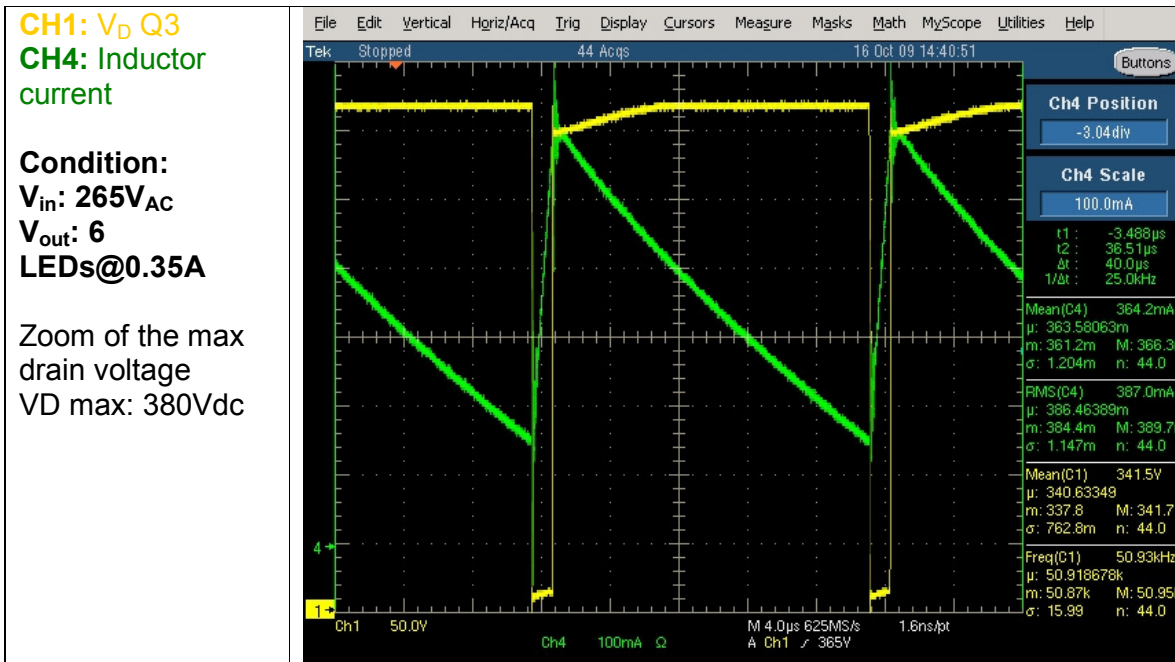
CH1: V_D Q3

CH4: I_D Q3

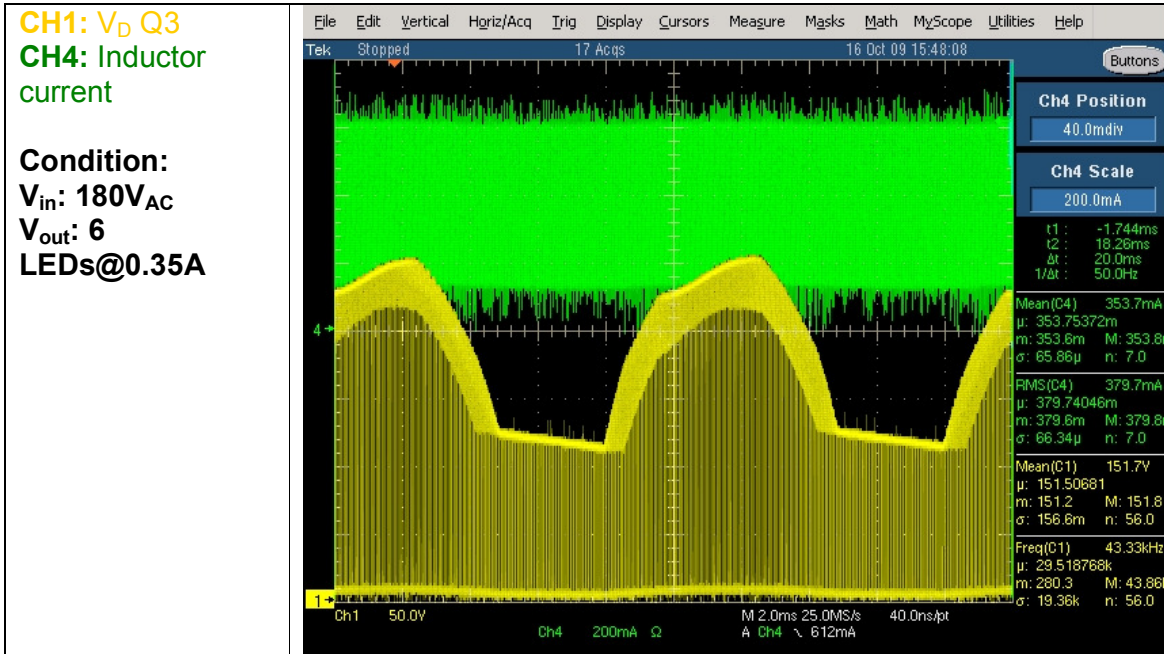
8.2 One complete 50 Hz cycle: $V_{IN\ max}$ with max power



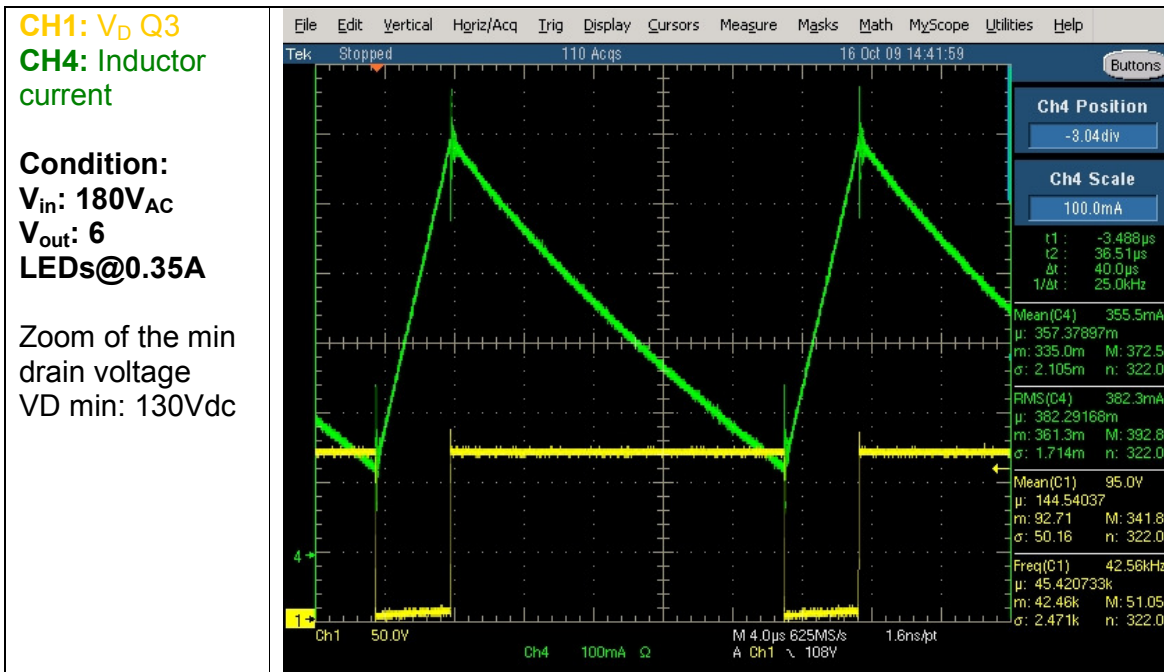
8.3 One complete PWM cycle: $V_{IN\ max}$ with max power



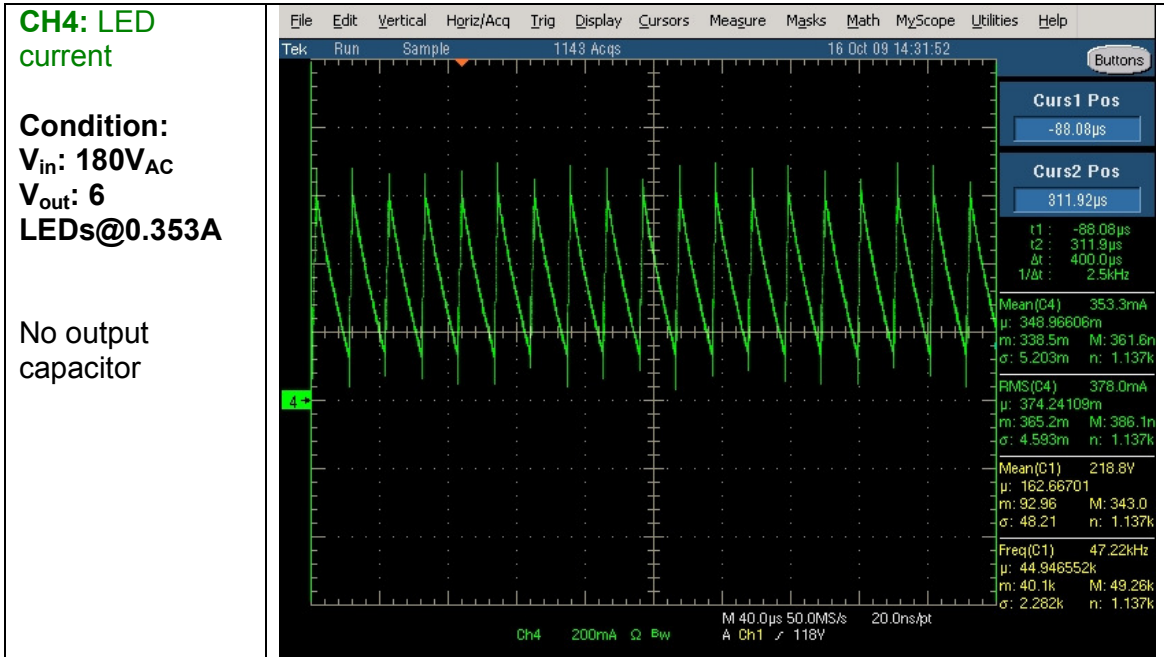
8.4 One complete 50 Hz cycle: $V_{IN\ min}$ with max power



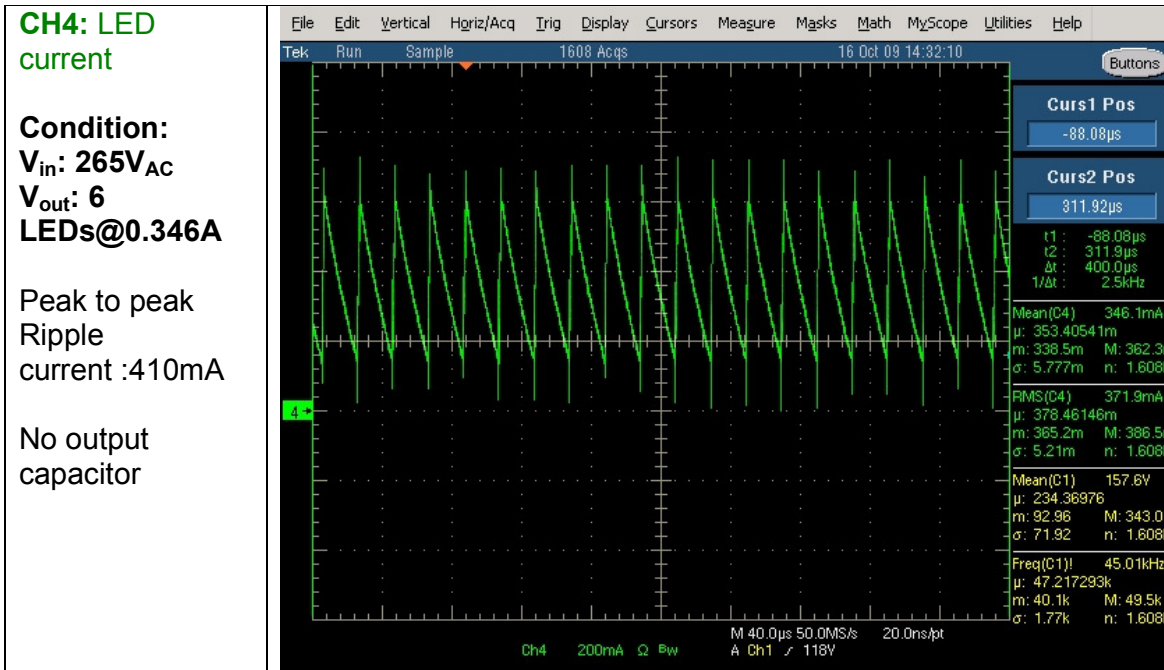
8.5 One complete PWM cycle: $V_{IN\ min}$ with max power



8.6 Output regulation: Ripple current at 180V_{in} AC



8.7 Output regulation: Ripple current at 265V_{in} AC

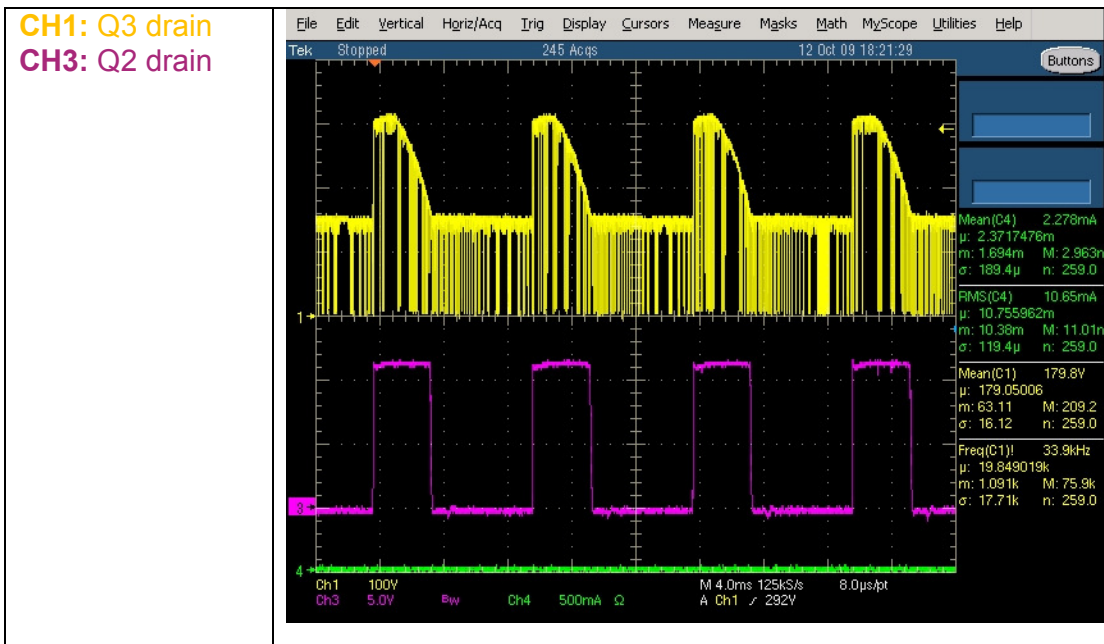


8.8 Dimming

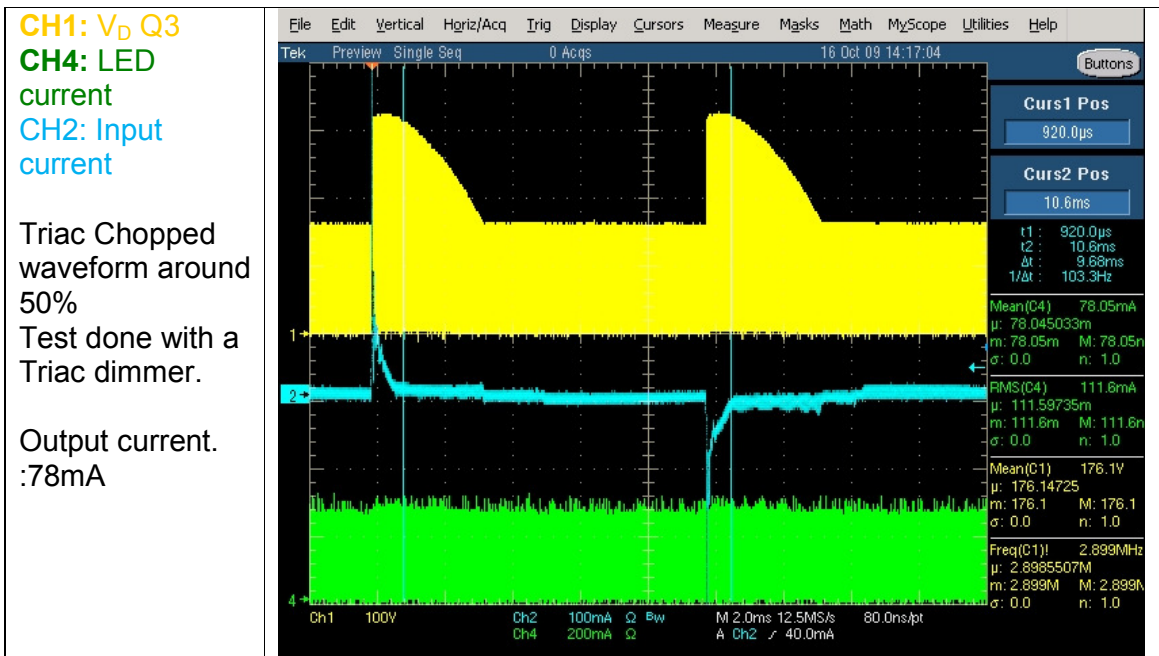
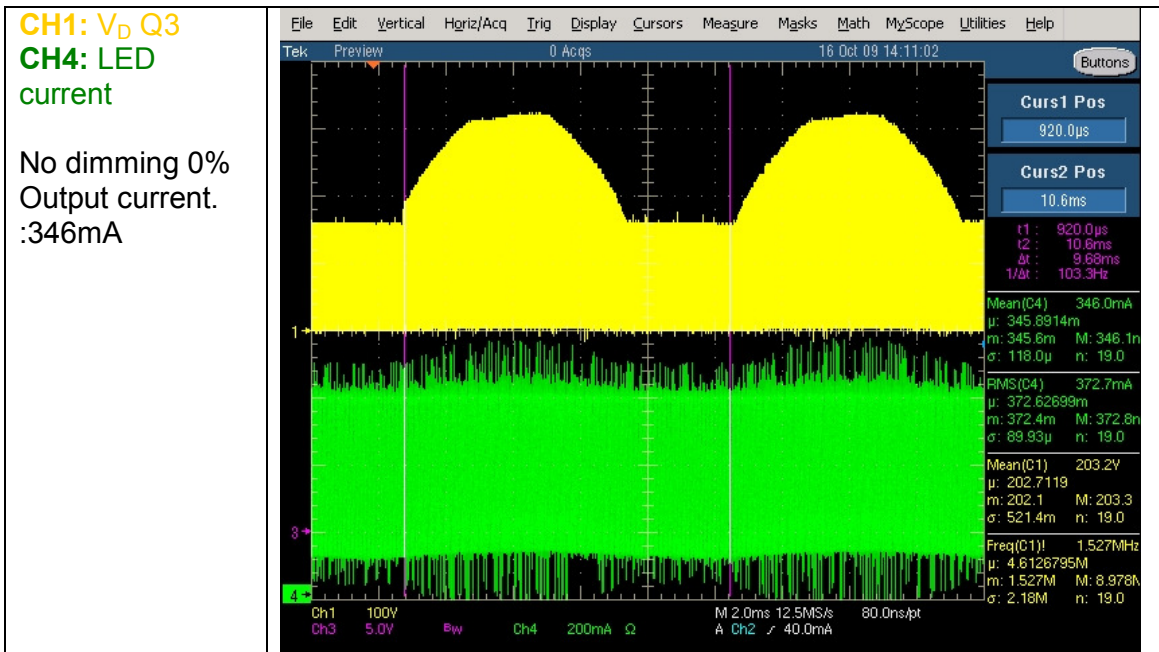
A simple Circuit composed by R6, Q2, D7 and R8 is used to add holding current when valley fill diodes D2, D5 are conducting.

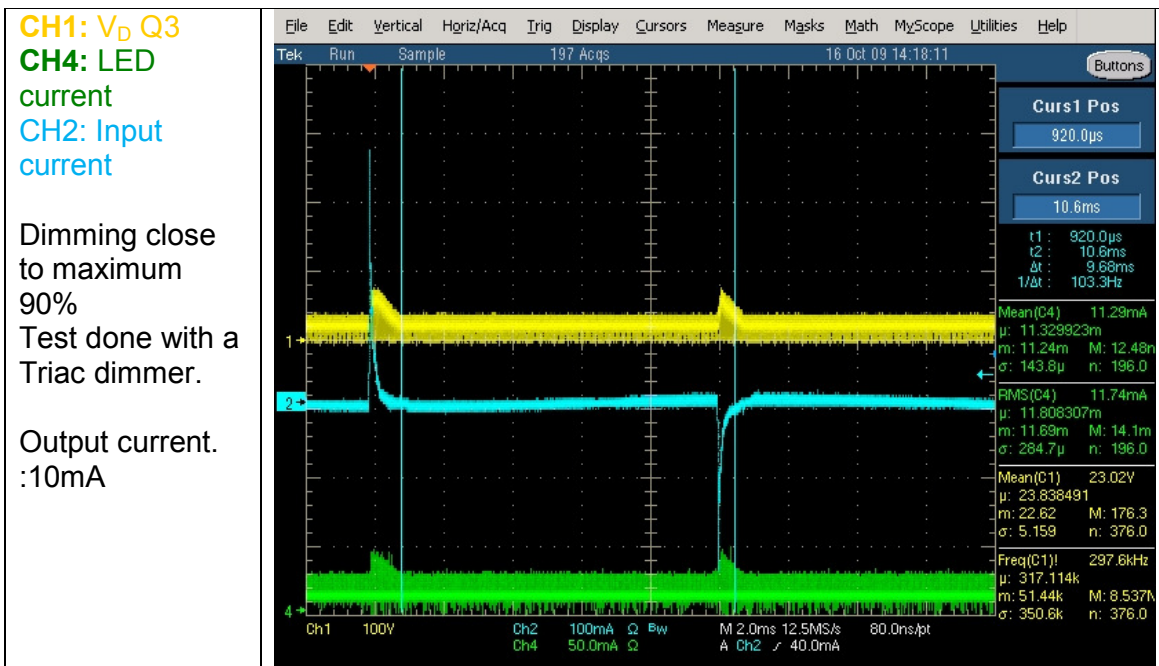
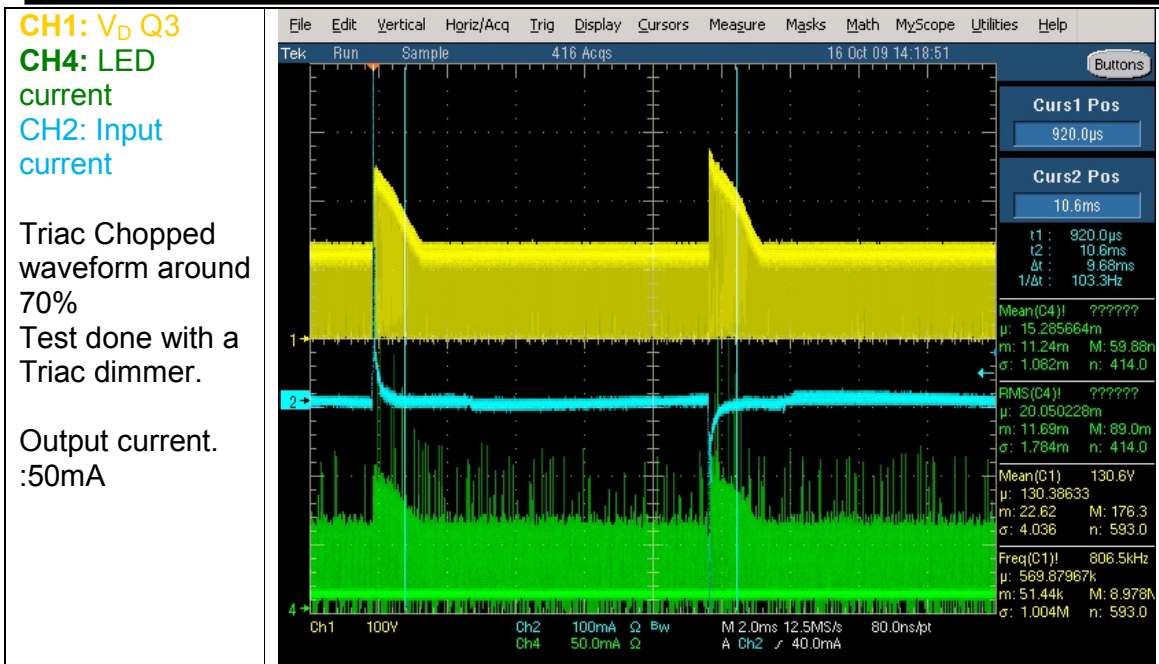
This simple circuit will reduce the power consumption of the holding circuit (Q1) and increase the overall efficiency. The Ch3 shows Q2 p mosfet ON when the output cap are in parallel discharging to the LEDs via the diode D2 and D5.

Only forward phase Triac dimmer can be used. To make it working with a reverse phase Triac, a simple circuit must implemented.



The following plots show dimming at different phase.





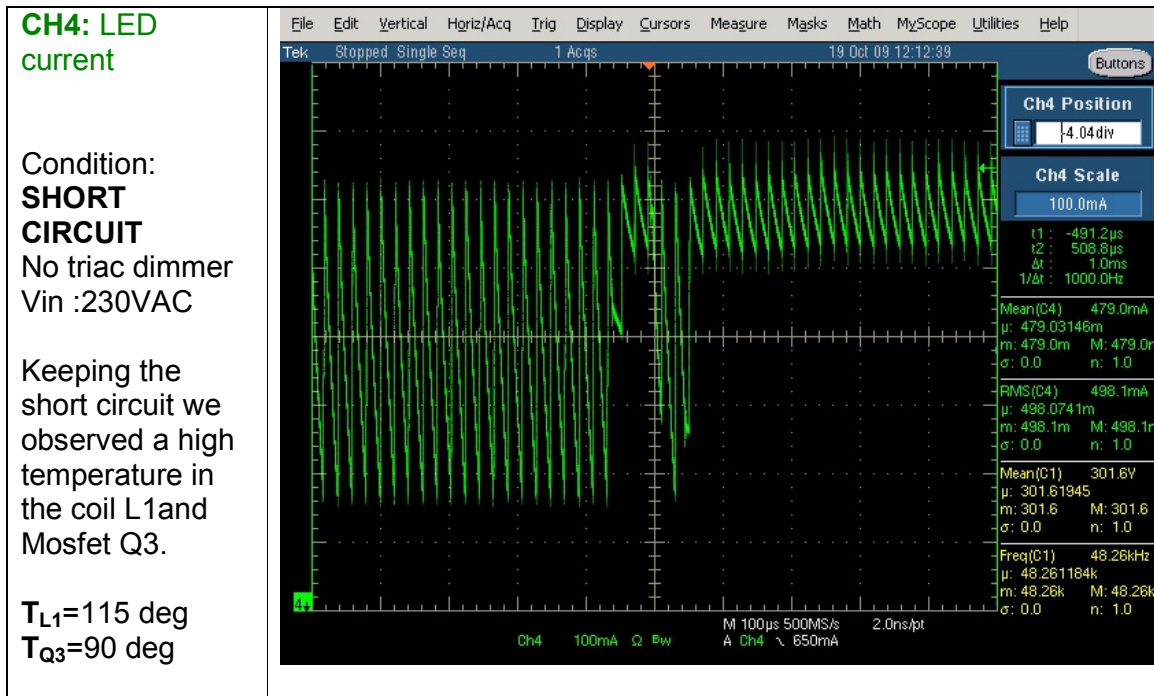
8.9 Protection

For safety reasons and to fulfill short circuit requirements, it has been ensured that no component should overheat and burn in case of short circuit.

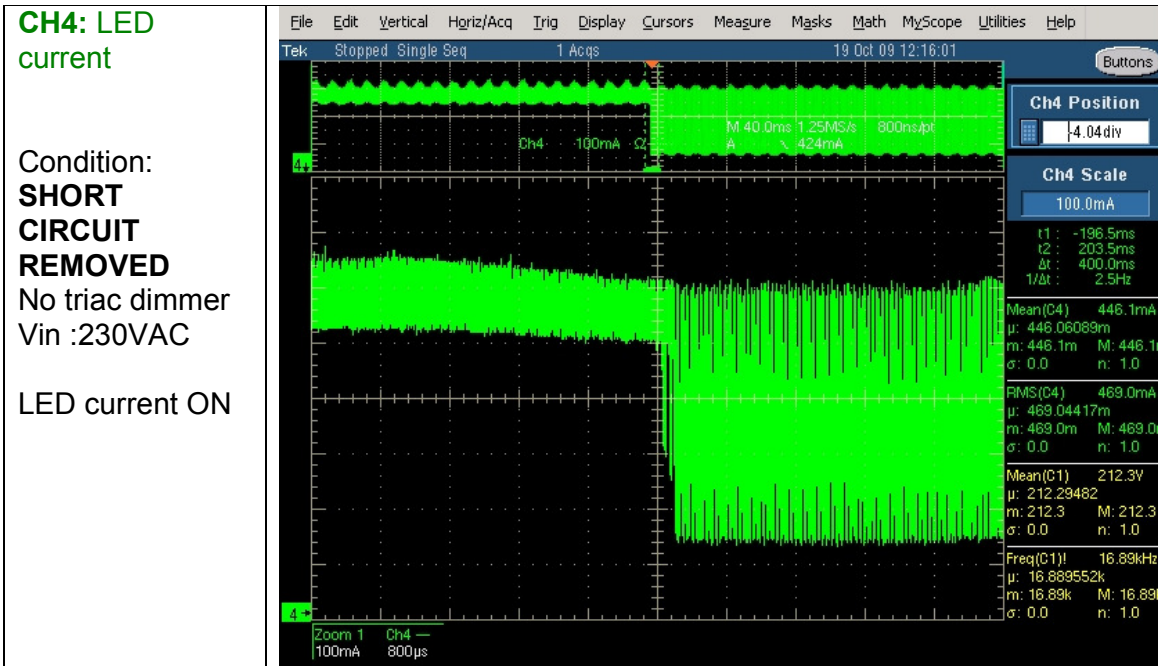
8.9.1 Short circuit protection

The cycle by cycle current limitation controls the maximum power in case of short circuit or an excessive load. The voltage across resistor R14 is proportional to the drain current and is sensed by the input ISNS pin 7 of the LM3445. If the voltage across R14 rises above 1.27V, the PWM uses this information to terminate the Mosfet conduction. It will also inhibit the Start Pulse Generator and the COFF comparator by holding the COFF pin low. A delay circuit will prevent the start of another cycle for 180 μ s. The typical threshold of the I_{SEN} signal in working condition is 750mV.

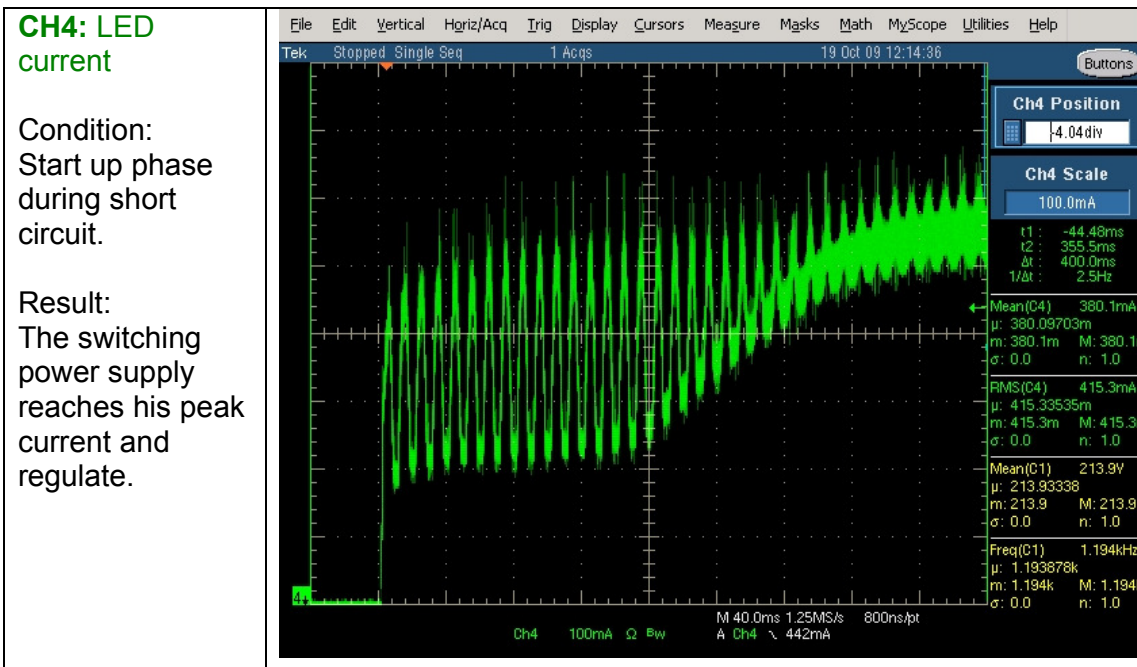
The following plots show a typical protection after short circuit on the LEDs.



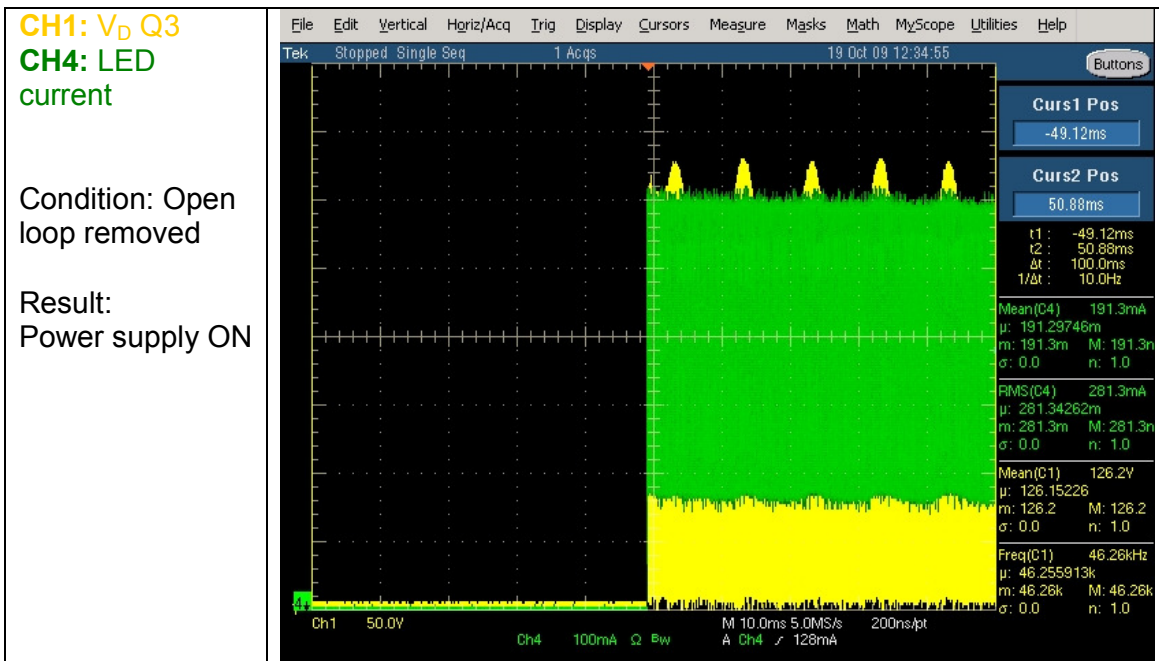
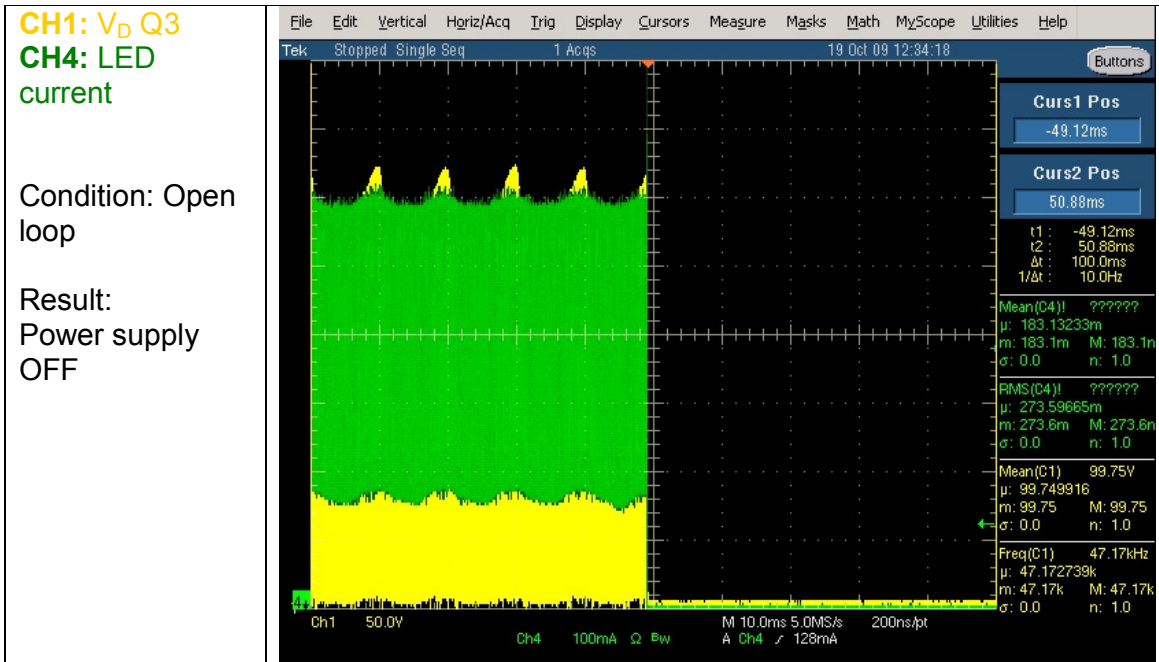
As soon as the short circuit is removed from the output, the power supply will go back to the regulated current 350mA.



The following plot shows a start up phase during short circuit. This is to ensure that switching ON and OFF the retrofit, it doesn't break.



8.9.2 Open loop protection



8.10 Efficiency

The following picture shows the efficiency for different input configuration.

PF	0.92			
Ithd	39.20%			
Vin (V)	180VAC	230VAC	265VAC	
Iin (A)	0.0537	0.0429	0.0384	
Pin (W)	8.94	9.16	9.39	
Vout (V)	19.86	19.86	19.87	
Iout (A)	0.35	0.355	0.357	
Eff (%)	0.778	0.770	0.755	

The test has been done with the following configuration.

R5 = 0R

R13= 1R

R6 = 3K3

8.11 EN630003-2 CLASS C

The measurement has been done with the Chroma model 61603 and Zimmer LMG95.

The harmonics are within the Class C limits of EN61000-3-2, the PF is 0.92 and the I THD is 40%.

As the input power is lower than 25W, the harmonic currents shall not exceed the power-related limits Class D, table 3, column 2:

3th harm 3.4mA/W, 5th harm 1.9mA/W...

Or

3th harm. < 86% of fundamental

5th harm. < 61% “ “

Harmonics (n)	Result (mA)	Class C limit (mA)
AH0	0.64	
AH1	39.85	
AH2	0.018	
AH3	7.46	31.17
AH4	0.021	
AH5	4.83	
AH6	0.023	
AH7	10.69	9.17
AH8	0.037	
AH9	6.19	4.58

8.12 Conductive EMI

In switched mode power supplies, there is a high dV/dt across the FET when it switches off. This is caused by abruptly cutting off the current through the inductance. This high dV/dt is undesirable for a number of reasons:

- High switching losses in the FET.
- Cause EMI Emission.
- High output ripple.

This high dV/dt can be reduced by a clamp network.

The next plots show the conducted EMI result for Neutral and Phase following the EN55022.

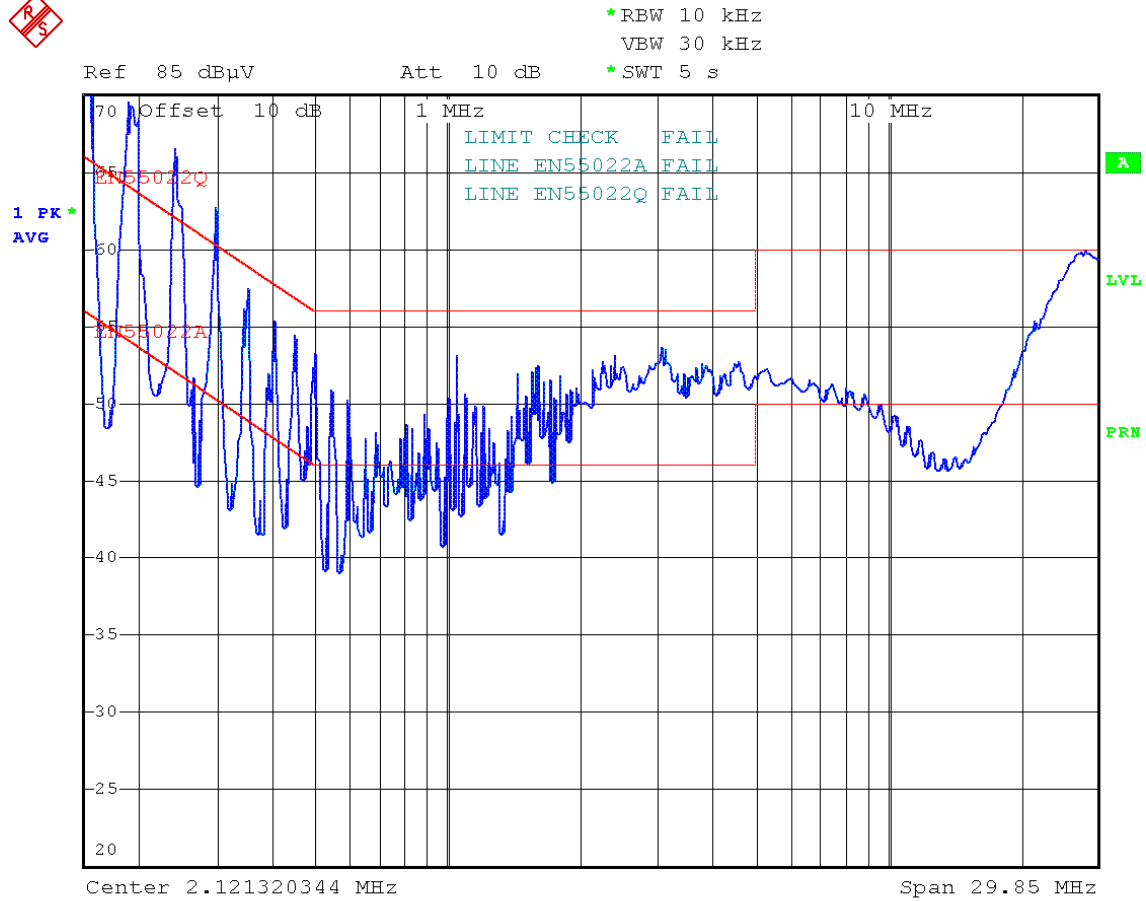
As the layout is not yet finalized, some peak frequencies are over the limit at very low frequency.

Phase L1:



Date: 16.OCT.2009 17:36:54

Neutral : N1



Date: 16.OCT.2009 17:19:15

8.13 Thermal behavior

The tests have been done with AC input voltage from 180 VAC to 260VAC with an output current of 350mA over a temperature range from -25°C to +65°C.

Due to the fact of the small factor, a small core of the inductance has been used and therefore saturate at ambient temperature higher than 65°C.
For higher ambient temperature, a higher core density is necessary.

The temperature measurement has been taken on key components as L1, Q3, D8, C3 and C2'.

Start up test has been as well done at this ambient temperature.

Vin 180VAC

Ambient Temperature		-25°C	25°C	45°C	65°C
Components					
Inductor	L1	38°C	82°C	97°C	117°C
Mosfet	Q3	8°C	57°C	74°C	82°C
Switching diode	D8	25°C	71°C	88°C	107°C
Passif PFC	C3	0°C	49°C	66°C	71°C
X2 cap	C2'	0°C	46°C	64°C	82°C

Vin 230VAC

Ambient Temperature		-25°C	25°C	45°C	65°C
Components					
Inductor	L1	41°C	85°C	100°C	120°C
Mosfet	Q3	12°C	60°C	79°C	84°C
Switching diode	D8	27°C	73°C	90°C	111°C
Passif PFC	C3	1°C	49°C	66°C	71°C
X2 cap	C2'	0°C	49°C	66°C	83°C

Vin 260VAC

Ambient Temperature		-25°C	25°C	45°C	65°C
Components					
Inductor	L1		86°C	103°C	122°C
Mosfet	Q3		63°C	83°C	87°C
Switching diode	D8		74°C	95°C	114°C
Passif PFC	C3		49°C	68°C	74°C
X2 cap	C2'		49°C	67°C	85°C

9 Inductor specification

Spezifikation für Freigabe / specification for release

Kunde / customer : _____

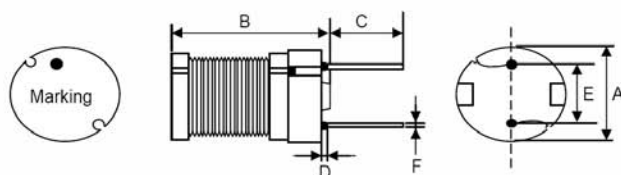
Artikelnummer / part number : **744743102**



Bezeichnung : **Tonneninduktivität WE-TI**
description : **Filter Choke WE-TI**

DATUM / DATE : 2004-11-30

A Mechanische Abmessungen / dimensions:



	7,8 X 12	
A	8,0 max.	mm
B	12,5 max.	mm
C	5,0 ± 1,0	mm
D	1,5 max.	mm
E	5,0 ± 0,5	mm
F	ø 0,70 ref	mm

● = Start of winding Marking = Inductance code

B Elektrische Eigenschaften / electrical properties:

Eigenschaften / properties	Testbedingungen / test conditions		Wert / value	Einheit / unit	tol.
Leerlauf-Induktivität / inductance	1 kHz / 0,25V	L_0	1000,0	μ H	±10%
Nenn-Induktivität / nominal inductance	1 kHz/0,25V/IN	L_N		μ H	typ.
DC-Widerstand / DC-resistance	@20°C	$R_{DC \max}$	2,50	Ω	max.
Nennstrom / nominal current	$\Delta T=40 \text{ K}$	I_N	0,42	A	max.
Sättigungsstrom / saturating current	$ \Delta L/L_0 -10\%$	I_{sat}	0,55	A	typ.

D Prüfgeräte / test equipment:

HP 4274 A & HP E3633 A für/for L_0
HP 34401 A für/for I_N und/and R_{DC}

E Testbedingungen / test conditions:

Luftfeuchtigkeit / humidity: 33%
Umgebungstemperatur / temperature: +20°C

F Werkstoffe & Zulassungen / material & approvals

Basismaterial / base material: Ferrit/ferrite
 Draht / wire: 2-UEW 155°C

G Eigenschaften / general specifications:

Lagertemperatur / storage temperature: -25°C - +85°C
Betriebstemp. / operating temperature: -25°C - +85°C
It is recommended that the temperature of the part does not exceed 125°C under worst case operating conditions.

Freigabe erteilt / general release:	Kunde / customer		

Datum / date	Unterschrift / signature		

Geprüft / checked	Würth Elektronik		
	ME	Version 3	04-11-30
	ME	Version 2	04-11-05
	ME	Version 1	04-08-10
	Name	Änderung / modification	Datum / date

Würth Elektronik eiSos GmbH & Co.KG

D-74638 Waldenburg · Max-Eyth-Strasse 1 - 3 · Germany · Telefon (+49) (0) 7942 - 945 - 0 · Telefax (+49) (0) 7942 - 945 - 400
<http://www.we-online.com>

Spezifikation für Freigabe / specification for release

Kunde / customer : _____

Artikelnummer / part number : **744743102**

LF

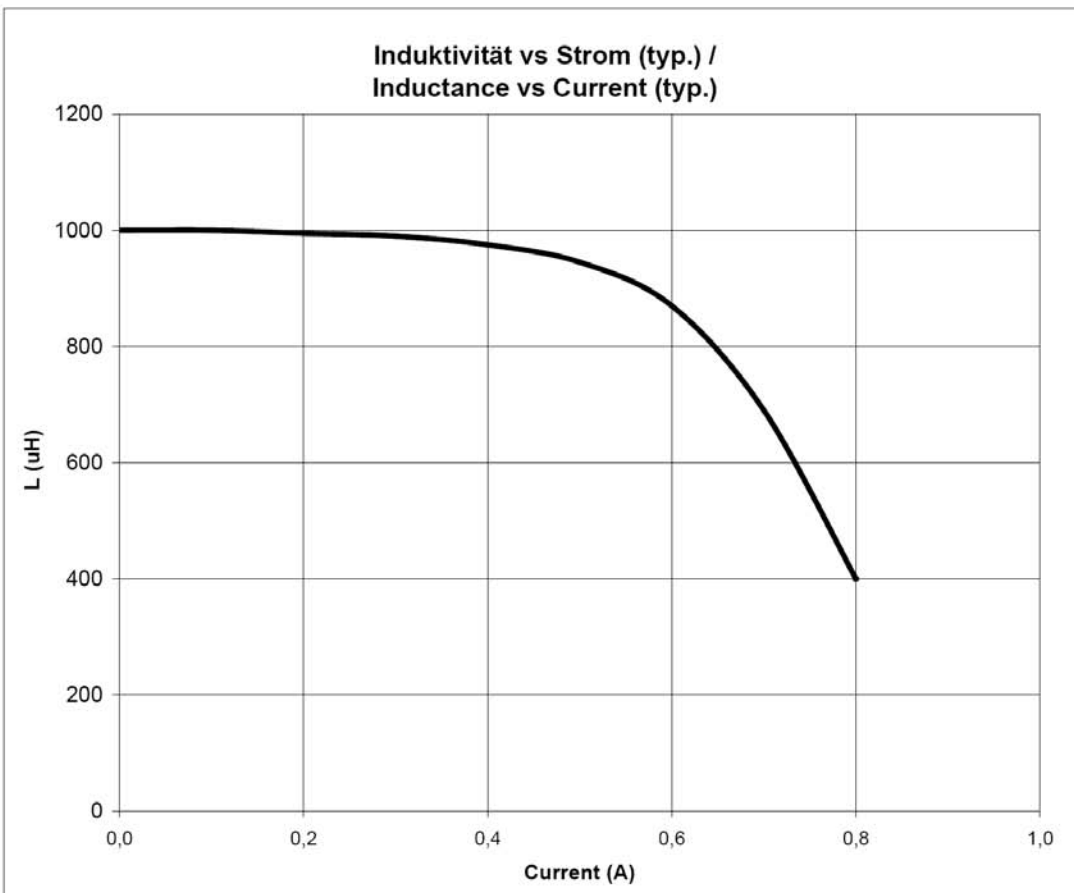


Bezeichnung : **Tonneninduktivität WE-TI**

description : **Filter Choke WE-TI**

DATUM / DATE : 2004-11-30

H Induktivitätskurve / Inductance curve :



Freigabe erteilt / general release:	Kunde / customer			
Datum / date	Unterschrift / signature			
	Würth Elektronik	ME	Version 3	04-11-30
		ME	Version 2	04-11-05
		ME	Version 1	04-08-10
Geprüft / checked	Kontrolliert / approved	Name	Änderung / modification	Datum / date

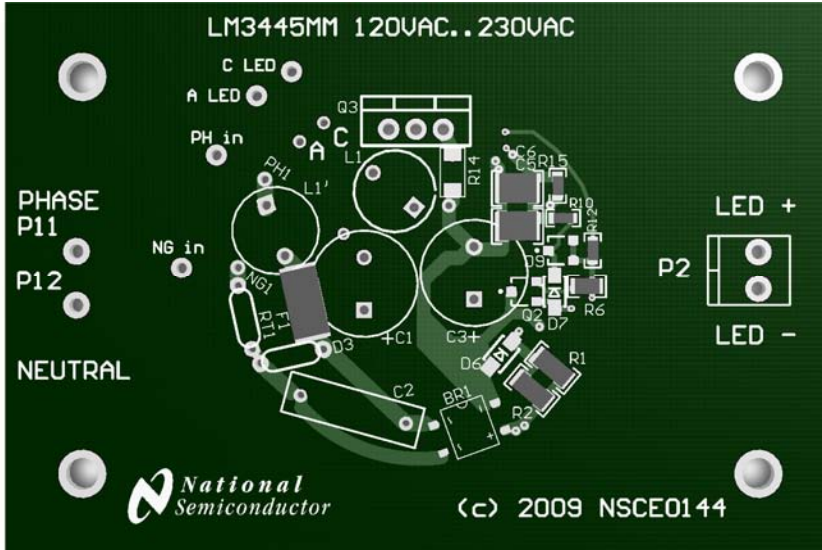
This electronic component is designed and developed with the intention for use in general electronics equipments. Before incorporating the components into any equipments in the field such as aerospace, aviation, nuclear control, submarine, transportation, (automotive control, train control, ship control), transportation signal, disaster prevention, medical, public information network etc. where higher safety and reliability are especially required or if there is possibility of direct damage or injury to human body. In addition, even electronic component in general electronic equipments, when used in electrical circuits that require high safety, reliability functions or performance, the sufficient reliability evaluation-check for the safety must be performed before use. It is essential to give consideration when to install a protective circuit at the design stage.

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10 Layout Design

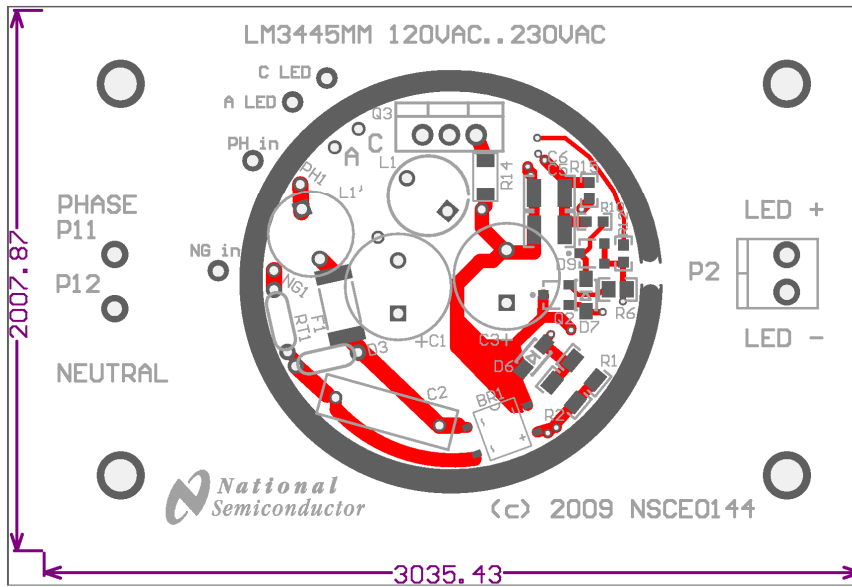
TOP 3D SOLDER AND COMPONENTS



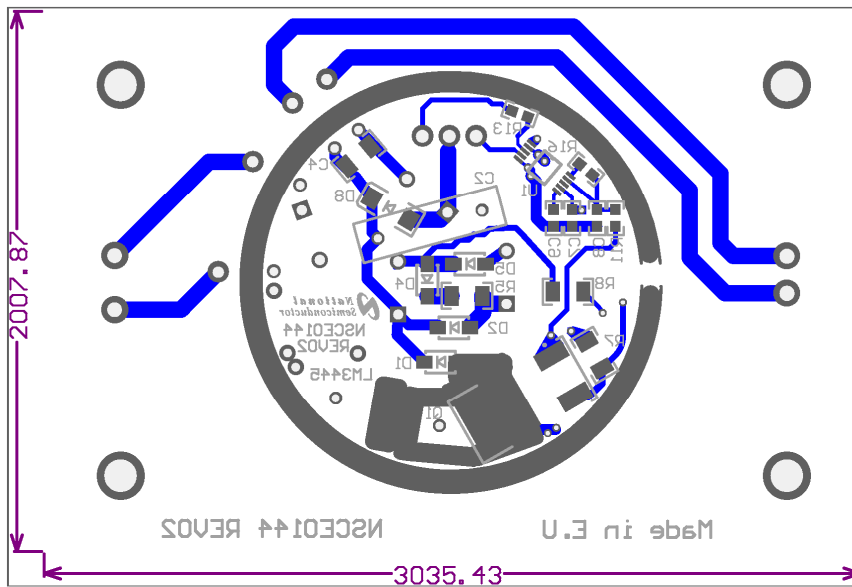
BOTTOM 3D SOLDER AND COMPONENTS



TOP SOLDER AND COMPONENTS



BOTTOM SOLDER AND COMPONENTS



11 Summary Table

12 Revision History

Status	Date	Description of change (s)
Rev. 2.0	2009-10-01	Efficiency improved

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