

# **LMH6732 High Speed Op Amp with Adjustable Bandwidth**

**Check for Samples: [LMH6732](http://www.ti.com/product/lmh6732#samples)**

**<sup>2</sup>• Exceptional Performance at Any Supply • Battery Powered Systems Current: • Video Switching and Distribution**

 $V_S = \pm 5V$ ,  $T_A = 25^{\circ}C$ ,  $A_V = +2V/V$ ,  $V_{OUT} = 2V_{PP}$ , emote Site Instrumentation<br>Typical unless Noted:



- 
- 
- 
- 

 $R_L = 100\Omega$  $A_V = +2$  $Re = 7000$ 

- 
- 
- 

0 1 2 3 8 9 10 11 12  $I_{C}C$  (mA)

 $0.25V<sub>PF</sub>$ 

2.0V<sub>PP</sub>

6

#### **<sup>1</sup>FEATURES APPLICATIONS**

- 
- 
- 
- **• Mobile Communications Gear**

#### $DESCRIPTION$

**The LMH6732 is a high speed op amp with a unique 1.0 55 0.20 / 0.036 400 -70.0 9** combination of high performance, low power **3.4 180 0.022 / 0.017 2100 -78.5 45** consumption, and flexibility of application. The supply **9.0 540 0.025** current is adjustable, over a continuous range of **/ 0.010 2700 -79.6 115** more than 10 to 1, with a single resistor,  $R<sub>P</sub>$ . This **• Ultra High Speed (−3dB BW) 1.5GHz** feature allows the device to be used in a wide variety **(ICC = 10mA, 0.25VPP)** of high performance applications including device turn **Single Resistor Adjustability of Supply Current** on/ turn off (Enable/ Disable) for power saving or multiplexing. Typical performance at any supply **Fast Enable/ Disable Capability 20ns**<br> **(I<sub>CC</sub>** = **9mA)** current is exceptional. The LMH6732's design has<br> **Popless'' Output on "Enable" 15mV** been optimized so that the output is well behaved,<br>
eliminating spurious outpu  $\blacksquare$  **eliminating spurious outputs on "Enable".** 

**(ICC <sup>=</sup> 1mA)** The LMH6732's combination of high performance, **••** Ultra Low Disable Current <1µA **b** low power consumption, and large signal **• Unity Gain Stable** performance makes it ideal for a wide variety of remote site equipment applications such as battery **• Improved Replacement for CLC505 & CLC449** powered test instrumentation and communications gear. Other applications include video switching matrices, ATE and phased array radar systems.

> The LMH6732 is available in the SOIC and SOT-23 packages. To reduce design times and assist in board layout, the LMH6732 is supported by an evaluation board.



**Figure 1. −3dB BW vs. ICC Figure 2. Turn-On/Off Characteristics**

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BW (MHz)

## **[LMH6732](http://www.ti.com/product/lmh6732?qgpn=lmh6732)**

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**RUMENTS** 



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### **Absolute Maximum Ratings(1)(2)**



(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications, see the Electrical Characteristics tables.

(2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/Distributors for availability and specifications..

(3) The maximum output current ( $I_O$ ) is determined by device power dissipation limitations.<br>(4) Human body model: 1.5k $\Omega$  in series with 100pF. Machine model:  $0\Omega$  in series with 200

Human body model: 1.5kΩ in series with 100pF. Machine model: 0Ω in series with 200pF.

### **Operating Ratings(1)**



(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications, see the Electrical Characteristics tables.



### **Electrical Characteristics**  $I_{CC}$  **= 9mA<sup>(1)</sup>**

 $A_V$  = +2,  $R_F$  = 700Ω,  $V_S$  = ±5V,  $R_L$  = 100Ω,  $R_P$  = 39kΩ; Unless otherwise specified.



(1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that T $_{\rm J}$  = T<sub>A</sub>. No ensured specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where T $_{\rm J}$  > T<sub>A</sub>. Min/Max ratings are based on production testing unless otherwise specified.

(2) Typical numbers are the most likely parametric norm. Bold numbers refer to over temperature limits.

(3) Slew Rate is the average of the rising and falling edges.

**STRUMENTS** 

**EXAS** 

## **Electrical Characteristics ICC = 9mA[\(1\)](#page-7-0) (continued)**

 ${\sf A_V}$  = +2,  ${\sf R_F}$  = 700 $\Omega$ ,  ${\sf V_S}$  = ±5V,  ${\sf R_L}$  = 100 $\Omega$ ,  ${\sf R_P}$  = 39k $\Omega$ ; Unless otherwise specified.



(4) Drift determined by dividing the change in parameter distribution average at temperature extremes by the total temperature change

(5) Negative input current implies current flowing out of the device.



## **Electrical Characteristics**  $I_{\text{cc}} = 3.4 \text{mA}^{(1)}$

 $A_V = +2$ ,  $R_F = 1kΩ$ ,  $V_S = ±5V$ ,  $R_L = 100Ω$ ,  $R_P = 137kΩ$ ; Unless otherwise specified.



(1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that T $_{\rm J}$  = T<sub>A</sub>. No ensured specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where T $_{\rm J}$  > T<sub>A</sub>. Min/Max ratings are based on production testing unless otherwise specified.

(2) Typical numbers are the most likely parametric norm. Bold numbers refer to over temperature limits.

(3) Slew Rate is the average of the rising and falling edges.

**RUMENTS** 

**EXAS** 

## **Electrical Characteristics ICC = 3.4mA[\(1\)](#page-7-0) (continued)**

 $A_V$  = +2, R<sub>F</sub> = 1kΩ, V<sub>S</sub> = ±5V, R<sub>L</sub> = 100Ω, R<sub>P</sub> = 137kΩ; Unless otherwise specified.



(4) Drift determined by dividing the change in parameter distribution average at temperature extremes by the total temperature change

(5) Negative input current implies current flowing out of the device.



## **Electrical Characteristics**  $I_{cc} = 1.0 \text{mA}^{(1)}$

 $A_V$  = +2,  $R_F$  = 1kΩ,  $V_S$  = ±5V,  $R_L$  = 500Ω,  $R_P$  = 412kΩ; Unless otherwise specified.



(1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that T $_{\rm J}$  = T<sub>A</sub>. No ensured specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where T $_{\rm J}$  > T<sub>A</sub>. Min/Max ratings are based on production testing unless otherwise specified.

(2) Typical numbers are the most likely parametric norm. Bold numbers refer to over temperature limits.

(3) Slew Rate is the average of the rising and falling edges.

**TRUMENTS** 

**EXAS** 

## **Electrical Characteristics ICC = 1.0mA[\(1\)](#page-7-0) (continued)**

 $A_V$  = +2, R<sub>F</sub> = 1kΩ, V<sub>S</sub> = ±5V, R<sub>L</sub> = 500Ω, R<sub>P</sub> = 412kΩ; Unless otherwise specified.



<span id="page-7-0"></span>(4) Drift determined by dividing the change in parameter distribution average at temperature extremes by the total temperature change

(5) Negative input current implies current flowing out of the device.



<span id="page-8-0"></span>

### **CONNECTION DIAGRAMS**





**Figure 3. 8-Pin SOIC (Top View) Figure 4. 6-Pin SOT-23 (Top View) See Package Number D (R-PDSO-G8) See Package Number DBV (R-PDSO-G6)**

<span id="page-9-0"></span>

**TYPICAL PERFORMANCE CHARACTERISTICS**

**Figure 11. Figure 12. Figure 13.**







20 MHz/DIV

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ςs = 10:

1 dB/DIV

HD (dBc)

HD (dBc)

20 MHz/DIV

**Figure 29. Figure 30. Figure 31.**

36:

برج<br>س  $\tilde{z}$ :

 $R_{S=1}$ = 12:

5 MHz/DIV

 $\overline{I}_{\text{CC}} = 1 \text{mA}$  $A_V = +2$ ,  $-R_L = 1k\Omega$ 

 $C_L = 56pF$  $R_S = 36\Omega$ 



**FXAS NSTRUMENTS** 

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<span id="page-13-2"></span><span id="page-13-1"></span><span id="page-13-0"></span>







### **APPLICATION INFORMATION**



<span id="page-15-0"></span>



**Figure 60. Recommended Inverting Gain Circuit**

### **DESCRIPTION**

The LMH6732 is an adjustable supply current, current-feedback operational amplifier. Supply current and consequently dynamic performance can be easily adjusted by selecting the value of a single external resistor  $(R_P)$ .

#### **NOTE**

The following discussion uses the SOIC package pin numbers. For the corresponding SOT-23 package pin numbers, please refer to the [Connection](#page-8-0) Diagrams section.

### **SELECTING AN OPERATING POINT**

The operating point is determined by the supply current which in turn is determined by current  $(I_P)$  flowing out of pin 8. As the supply current is increased, the following effects will be observed:







Both the Electrical Characteristics pages and the TYPICAL PERFORMANCE [CHARACTERISTICS](#page-9-0) section illustrate these effects to help make the supply current vs. performance trade-off. The supply current is adjustable over a continuous range of more than 10 to 1 with a single resistor, R<sub>P</sub>, allowing for easy trade-off between power consumption and speed. Performance is specified and tested at  $I_{CC} = 1 \text{mA}$ , 3.4mA, and 9mA. (Note: Some test conditions and especially the load resistances are different for the three supply current settlings.) The performance plots show typical performance for all three supply currents levels.

When making the supply current vs. performance trade-off, it is first a good idea to see if one of the standard operating points ( $I_{CC}$  = 1mA, 3.4mA, or 9mA) fits the application. If it does, performance ensured on the specification pages will apply directly to your application. In addition, the value of  $R<sub>P</sub>$  may be obtained directly from the Electrical Characteristics pages.

#### **BEYOND 1GHz BANDWIDTH**

As stated above, the LMH6732 speed can be increased by increasing the supply current. The −3dB Bandwidth can even reach the unprecedented value of 1.5GHz ( $A_V = +2$ ,  $V_{OUT} = 0.25V_{PP}$ ). Of course, this comes at the expense of power consumption (i.e. supply current). The relationship between −3dB BW and supply current is shown in [Figure](#page-13-0) 48 to [Figure](#page-13-1) 50. The supply current would nominally have to be set to around 10mA to achieve this speed. The absolute maximum supply current setting for the LMH6732 is 14mA. Beyond this value, the operation may become unpredictable.

#### The following discussion will assist in selecting  $I_{CC}$  for applications that cannot operate at one of the **specified supply current settlings.**

Use the typical performance plots for critical specifications to select the best  $I_{CC}$ . For parameters containing Min/Max ratings in the data sheet tables, interpolate between the values of  $I_{CC}$  in the plots & specification tables to estimate the max/min values in the application.

The simplified schematic for the supply current setting path  $(I_P)$  is shown below in [Figure](#page-16-0) 61.



**Figure 61. Supply Current Control's Simplified Schematic**

<span id="page-16-0"></span>The terminal marked "R<sub>P</sub>" is tied to a potential through a resistor R<sub>P</sub>. The current flowing through R<sub>P</sub> (I<sub>P</sub>) sets the LMH6732's supply current. Throughout the data sheet, the voltages applied to R<sub>P</sub> and V<sup>-</sup> are both considered to be −5V. However, the two potentials do not necessarily have to be the same. This is beneficial in applications where non-standard supply voltages are used or when there is a need to power down the op amp via digital logic control.

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The relationship between  $I_{CC}$  and  $I_P$  is given by:

 $I_P = I_{CC}/57$  (approximate ratio at  $I_{CC} = 3.4$  mA; consult [Figure](#page-13-2) 45 for relationship at any  $I_{CC}$ ).

Knowing  $I_P$  leads to a direct calculation of  $R_P$ .

 $R_P$  + 5kΩ = [(V<sup>+</sup> -1.6)-V<sup>-</sup>]/ I<sub>P</sub>

 $R_P$ + 5kΩ= =8.4 /l<sub>P</sub> (for V<sup>+</sup> = 5V and V<sup>-</sup> = -5V).

First, an operating point needs to be determined from the plots & specifications as discussed above. From this, I<sub>P</sub> is obtained. Knowing  $I_P$  and the potential  $R_P$  is tied to,  $R_P$  can be calculated.

#### **EXAMPLE**

An application requires that  $V_S = \pm 3V$  and performance in the 1mA operating point range. The required I<sub>P</sub> can therefore be determined as follows:

 $I_P = 21 \mu A$ 

 $R_P$  is connected from pin 8 to  $V^-$ . Calculate  $R_P$  under these conditions:

 $R_P$ + 5kΩ = [(V<sup>+</sup> -1.6)-V<sup>-</sup>] / I<sub>P</sub>  $R_P$ + 5kΩ = [(3V-1.6V) - (-3V)] / 21μA

 $R_P = 205k\Omega$ 

The LMH6732 will have performance similar to  $R_P = 412kΩ$  shown on the datasheet, but with 40% less power dissipation due to the reduced supply voltages. The op amp will also have a more restricted common-mode range and output swing.

#### **DYNAMIC SHUTDOWN CAPABILITY**

The LMH6732 may be powered on and off very quickly by controlling the voltage applied to  $R_P$ . If  $R_P$  is connected between pin 8 and the output of a CMOS gate powered from ±5V supplies, the gate can be used to turn the amplifier on and off. This is shown in [Figure](#page-17-0) 62 below:



#### **Figure 62. Dynamic Control of Power Consumption Using CMOS Logic**

<span id="page-17-0"></span>When the gate output is switched from high to low, the LMH6732 will turn on. In the off state, the supply current typically reduces to 1μA or less. The LMH6732's "off state" supply current is reduced significantly compared to the CLC505. This extremely low supply current in the "off state" is quite advantageous since it allows for significant power saving and minimizes feed-through. To improve switching time, a speed up capacitor from the gate output to pin 8 is recommended. The value of this capacitor will depend on the  $R<sub>P</sub>$  value used and is best established experimentally. Turn-on and turn-off times of  $\langle$ 20ns ( $I_{CC}$  = 9mA) are achievable with ordinary CMOS gates.

#### **EXAMPLE**

An open collector logic device is used to dynamically control the power dissipation of the circuit. Here, the desired connection for  $R_P$  is from pin 8 to the open collector logic device.





**Figure 63. Controlling Power On State with TTL Logic (Open Collector Output)**

When the logic gate goes low, the LMH6732 is turned on. The LMH6732 V<sup>+</sup> connection would be to +5V supply.

Performance desired is that given for  $I_{CC} = 3.4$ mA under standard conditions. From the  $I_{CC}$  vs. I<sub>P</sub> plot, I<sub>P</sub> = 61µA. Then calculating  $R_P$ :

 $R_P$  + 5kΩ = [(5V-1.6V)- 0] / 61µA

 $R_P = 51k\Omega$ 

### **"POPLESS OUTPUT" & OFF CONDITION OUTPUT STATE**

The LMH6732 has been especially designed to have minimum glitches during turn-on and turn-off. This is advantageous in situations where the LMH6732 output is fed to another stage which could experience false autoranging, or even worse reset operation, due to these transient glitches. Example of this application would be an AGC circuit or an ADC with multiple ranges set to accommodate the largest input amplitude. For the LMH6732, these sorts of transients are typically less than 50mV in amplitude (see Electrical Characteristics Tables for Typical values). Applications designed to utilize the CLC505's low output glitch would benefit from using the LMH6732 instead since the LMH6732's output glitch is improved to be even lower than the CLC505's. In the "Off State", the output stage is turned off and is in effect put into a high-Z state. In this sate, output can be forced by other active devices. No significant current will flow through the device output pin in this mode of operation.

### **MUX APPLICATION**

Since The LMH6732's output is essentially open in the "off" state, it is a good candidate for a fast 2:1 MUX. [Figure](#page-18-0) 64 shows one such application along with the output waveform in [Figure](#page-19-0) 65 displaying the switching between a continuous triangle wave and a single cycle sine wave (signals trigger locked to each other for stable scope photo). Switching speed of the MUX will be less than 50 ns and is governed by the "Ton" and "Toff" times for U1 and U2 at the supply current set by  $R_{P1}$  and  $R_{P2}$ . Note that the "Control" input is a 5V CMOS logic level.



<span id="page-18-0"></span>





**Figure 65. MUX "VOUT" and "Control" Waveform**

### <span id="page-19-0"></span>**DIFFERENTIAL GAIN AND PHASE**

Differential gain and phase are measurements useful primarily in composite video channels. They are measured by monitoring the gain and phase changes of a high frequency carrier (3.58MHz for NTSC and 4.43MHz for PAL systems) as the output of the amplifier is swept over a range of DC voltages. Specifications for the LMH6732 include differential gain and phase. Test signals used are based on a  $1V_{PP}$  video level. Test conditions used are the following:

DC sweep range: 0 to 100 IRE units (black to white)

Carrier: 4.43MHz at 40 IRE units peak to peak

 $A<sub>V</sub>$  = +2, R<sub>L</sub> = 75Ω + 75Ω

#### **SOURCE IMPEDANCE**

For best results, source impedance in the non-inverting circuit configuration (see [Figure](#page-15-0) 59) should be kept below 5kΩ.

Above 5kΩ it is possible for oscillation to occur, depending on other circuit board parasitics. For high signal source impedances, a resistor with a value of less than 5kΩ may be used to terminate the non-inverting input to ground.

#### **FEEDBACK RESISTOR**

In current-feedback op amps, the value of the feedback resistor plays a major role in determining amplifier dynamics. It is important to select the correct value. The LMH6732 provides optimum performance with feedback resistors as shown in [Table](#page-19-1) 2 below. Selection of an incorrect value can lead to severe roll-off in frequency response, (if the resistor value is too large) or , peaking or oscillation (if the value is too low).

<span id="page-19-1"></span>

Gain (V/V)	$I_{CC}$ (mA)			
	9	3.4		Unit
$A_V = +1$	700	1k	1k	Ω
$A_V = +2$	700	1k	1 <sub>k</sub>	Ω
$A_V = -1$	500	750	1 <sub>k</sub>	Ω
$A_V = -2$	400	450	1k	Ω
$A_V = +6$	500	500	1k	Ω
$A_V = -6$	200	200	1k	Ω
$A_V = +21$	1k	1k	1 <sub>k</sub>	Ω
$A_V = -20$	500	500	1 <sub>k</sub>	Ω

**Table 2. Feedback Resistor Selection for Various Gain Settings and ICC's**



For  $I_{CC}$  > 9mA at any closed loop gain setting, a good starting point for R<sub>F</sub> would be the 9mA value stated in [Table](#page-19-1) 2 above. This value could then be readjusted, if necessary, to achieve the desired response.

#### **PRINTED CIRCUIT LAYOUT & EVALUATION BOARDS**

Generally, a good high frequency layout will keep power supply and ground traces away from the inverting input and output pins. Parasitic capacitances on these nodes to ground will cause frequency response peaking and possible circuit oscillations (see Application Note OA-15 [\(SNOA367](http://www.ti.com/lit/pdf/snoa367)) for more information).

Use the following evaluation boards as a guide for high frequency layout and as an aid in device testing and characterization:



<span id="page-20-0"></span>The supply current adjustment resistor,  $R<sub>P</sub>$ , in both evaluation boards should be tied to the appropriate potential to get the desired supply current. To do so, leave R2 (LMH730216) [ R5 (LMH730227) ] uninstalled. Jumper "Dis" connector to V−. Install R1 (LMH730216) [ R4 (LMH730227) ] to set the supply current.





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**(1)** The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

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**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

**(6)** Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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### **TAPE AND REEL INFORMATION**





### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**







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# **PACKAGE MATERIALS INFORMATION**



\*All dimensions are nominal





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### **TUBE**



#### \*All dimensions are nominal





# **PACKAGE OUTLINE**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



# **EXAMPLE BOARD LAYOUT**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



# **EXAMPLE STENCIL DESIGN**

## **D0008A SOIC - 1.75 mm max height**

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.





# **PACKAGE OUTLINE**

# **DBV0006A SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.25 per side.
- 4. Leads 1,2,3 may be wider than leads 4,5,6 for package orientation.
- 5. Refernce JEDEC MO-178.



# **EXAMPLE BOARD LAYOUT**

# **DBV0006A SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



# **EXAMPLE STENCIL DESIGN**

# **DBV0006A SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.



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