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[Reference](http://www.ti.com/general/docs/refdesignsearchresults.tsp?dcmp=dsproject%E2%80%9D&%E2%80%9Dhqs=rd) Design

SNVS405G –DECEMBER 2005–REVISED APRIL 2015

LM3674 2-MHz, 600-mA Step-Down DC-DC Converter in SOT-23

Technical [Documents](http://www.ti.com/product/LM3674?dcmp=dsproject&hqs=td&#doctype2)

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- Internal Synchronous Rectification for High
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- MP3 Players
- Portable Instruments
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- Digital Still Cameras
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1 Features 3 Description

Tools & **[Software](http://www.ti.com/product/LM3674?dcmp=dsproject&hqs=sw&#desKit)**

Input Voltage Range From 2.7 V to 5.5 V The LM3674 step-down DC-DC converter optimized for powering low-voltage circuits from a • 600-mA Maximum Load Current single Li-Ion cell battery and input voltage rails from • Available in Fixed and Adjustable Output Voltages 2.7 V to 5.5 V. It provides up to 600-mA load current over the entire input voltage range. There are several • Operates From a Single Li-Ion Cell Battery fixed output voltages and adjustable output voltage versions.

Support & **[Community](http://www.ti.com/product/LM3674?dcmp=dsproject&hqs=support&#community)**

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Efficiency The device offers superior features and performance For mobile phones and similar portable systems.
• Internal Soft-Start **During the Pulse Width Modulation (PWM) mode, the**
• O.01-µA Typical Shutdown Current device operates at a fixed-frequency of 2 MHz • 2-MHz PWM Fixed Switching Frequency (typical) (typical). Internal synchronous rectification provides • Current Overload Protection and Thermal high efficiency during the PWM mode operation. In shutdown mode, the device turns off and reduces Shutdown Protection battery consumption to 0.01 µA (typical).

2 Applications The LM3674 is available in a 5-pin SOT-23 package. ^A high switching frequency of ² MHz (typical) allows • Mobile Phones use of only three tiny external surface-mount • PDAs components, an inductor and two ceramic capacitors.

Device Information[\(1\)](#page-0-0)

Portable Hard Disk Drives entitled and the end of the data sheet.

the end of the data sheet.

Typical Application Circuit Typical Application Circuit for Adjustable Voltage Option

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4 Revision History

Changes from Revision F (May 2013) to Revision G Page

- Added *Pin Configuration and Functions* section, *ESD Ratings* table, *Feature Description* section, *Device Functional Modes*, *Application and Implementation* section, *Power Supply Recommendations* section, *Layout* section, *Device and Documentation Support* section, and *Mechanical, Packaging, and Orderable Information* section [1](#page-0-3)
- Deleted "in leaded (Pb) and lead-free (no Pb) versions" ... [1](#page-0-4)

Changes from Revision E (April 2013) to Revision F Page

• Changed layout of National Data Sheet to TI format ... [18](#page-17-1)

EXAS **STRUMENTS**

[LM3674](http://www.ti.com/product/lm3674?qgpn=lm3674) www.ti.com SNVS405G –DECEMBER 2005–REVISED APRIL 2015

5 Pin Configuration and Functions

Note: The actual physical placement of the package marking will vary from part to part.

Pin Functions

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) $(1)(2)$

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *[Recommended](#page-3-3) Operating [Conditions](#page-3-3)*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

If Military- or Aerospace-specified devices are required, please contact the TI Sales Office/Distributors for availability and specifications. In applications where high power dissipation and/or poor package resistance is present, the maximum ambient temperature may have to be derated. Maximum ambient temperature (T_{A-MAX}) is dependent on the maximum operating junction temperature (T_{J-MAX}) , the maximum power dissipation of the device in the application (P_{D-MAX}) and the junction-to-ambient thermal resistance of the package (RθJA) in the application, as given by the following equation: TA-MAX = TJ-MAX – (RθJA × PD-MAX). See *[Dissipation](#page-3-5) Ratings* for PD-MAX values at different ambient temperatures.

6.2 ESD Ratings

JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted) $⁽¹⁾$ </sup>

(1) All voltages are with respect to the potential at the GND pin.

Input voltage range recommended for ideal applications performance for the specified output voltages are given below:

 $V_{IN} = 2.7 \overline{V}$ to 5.5 V for 1 V \leq V_{OUT} < 1.8 V

 $V_{\text{IN}} = (V_{\text{OUT}} + V_{\text{DROP}})$ to 5.5 V for 1.8 \leq V_{OUT} \leq 3.3 V, where V_{DROP} out = I_{LOAD} \times (R_{DSON (P)} + R_{INDUCTOR})

6.4 Thermal Information

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](http://www.ti.com/lit/pdf/spra953).

6.5 Dissipation Ratings

over operating free-air temperature range (unless otherwise noted)

6.6 Electrical Characteristics

(1) All voltages are with respect to the potential at the GND pin.

(2) Minimum and maximum limits are specified by design, test, or statistical analysis. Typical numbers represent the most likely values.
(3) The parameters in the *Electrical Characteristics* are tested at $V_{\text{IN}} = 3.6$ The parameters in the *Electrical Characteristics* are tested at V_{IN} = 3.6 V unless otherwise specified. For performance curves over the input voltage range, see *Typical [Characteristics](#page-5-0)*.

(4) ADJ configured to 1.5-V output.

output voltage drops by 10%.

(5) For V_{OUT} < 2.5 V, V_{IN} = 3.6 V; for V_{OUT} ≥ 2.5 V, V_{IN} = V_{OUT} + 1.

(6) For the ADJ version the resistor dividers should be selected such that at the desired output voltage, the voltage at the FB pin is 0.5 V. (7) See *Typical [Characteristics](#page-5-0)* for closed loop data and its variation with regards to supply voltage and temperature. *Electrical Characteristics* reflect open loop data (FB = 0 V and current drawn from the SW pin ramped up until cycle-by-cycle current limit is activated). Closed-loop current limit is the peak inductor current measured in the application circuit by increasing output current until

EXAS STRUMENTS

[LM3674](http://www.ti.com/product/lm3674?qgpn=lm3674) SNVS405G –DECEMBER 2005–REVISED APRIL 2015 **www.ti.com**

6.7 Typical Characteristics

(unless otherwise stated: V_{IN} = 3.6 V, V_{OUT} = 1.5 V, T_A = 25°C)

Typical Characteristics (continued)

(unless otherwise stated: V_{IN} = 3.6 V, V_{OUT} = 1.5 V, T_A = 25°C)

Product Folder Links: *[LM3674](http://www.ti.com/product/lm3674?qgpn=lm3674)*

Typical Characteristics (continued)

(unless otherwise stated: V_{IN} = 3.6 V, V_{OUT} = 1.5 V, T_A = 25°C)

7 Detailed Description

7.1 Overview

The LM3674, a high-efficiency, step-down, DC-DC switching buck converter, delivers a constant voltage from a single Li-Ion battery and input voltage rails from 2.7 V to 5.5 V to portable devices such as cell phones and PDAs. Using a voltage mode architecture with synchronous rectification, the LM3674 has the ability to deliver up to 600 mA depending on the input voltage, output voltage, ambient temperature, and the inductor chosen.

Additional features include soft-start, undervoltage protection, current overload protection, and thermal overload protection. As shown in *Typical [Application](#page-0-5) Circuit*, only three external power components, C_{IN}, C_{OUT}, and L₁, are required for implementation.

The part uses an internal reference voltage of 0.5 V. It is recommended to keep the part in shutdown mode until the input voltage is 2.7 V or higher.

7.2 Functional Block Diagram

7.3 Feature Description

7.3.1 Circuit Operation

During the first portion of each switching cycle, the control block in the LM3674 turns on the internal PFET switch. This allows current to flow from the input through the inductor to the output filter capacitor and load. The inductor limits the current to a ramp with a slope of:

$$
\frac{V_{IN} - V_{OUT}}{L}
$$
 (1)

by storing energy in a magnetic field. During the second portion of each cycle, the controller turns the PFET switch off, blocking current flow from the input, and then turns the NFET synchronous rectifier on. The inductor draws current from ground through the NFET to the output filter capacitor and load, which ramps the inductor current down with a slope of:

 $-V_{OUT}$ \mathbf{L}

(2)

The output filter stores charge when the inductor current is high, and releases it when the inductor current is low, smoothing the voltage across the load.

The output voltage is regulated by modulating the PFET switch-on time to control the average current sent to the load. The effect is identical to sending a duty-cycle modulated rectangular wave formed by the switch and synchronous rectifier at the SW pin to a low-pass filter formed by the inductor and output filter capacitor. The output voltage is equal to the average voltage at the SW pin.

7.3.2 PWM Operation

During PWM operation, the converter operates as a voltage-mode controller with input voltage feed-forward. This allows the converter to achieve excellent load and line regulation. The DC gain of the power stage is proportional to the input voltage. To eliminate this dependence, feed-forward inversely proportional to the input voltage is introduced.

While in PWM mode, the output voltage is regulated by switching at a constant frequency and then modulating the energy per cycle to control power to the load. At the beginning of each clock cycle, the PFET switch is turned on and the inductor current ramps up until the comparator trips and the control logic turns off the switch.

The current limit comparator can also turn off the switch in case the current limit of the PFET is exceeded. Then the NFET switch is turned on and the inductor current ramps down. The next cycle is initiated by the clock turning off the NFET and turning on the PFET.

Figure 18. PWM Operation

7.3.2.1 Internal Synchronous Rectification

While in PWM mode, the LM3674 uses an internal NFET as a synchronous rectifier to reduce rectifier forward voltage drop and associated power loss. Synchronous rectification provides a significant improvement in efficiency whenever the output voltage is relatively low compared to the voltage drop across an ordinary rectifier diode.

7.3.2.2 Current Limiting

A current limit feature allows the LM3674 to protect itself and external components during overload conditions. PWM mode implements current limiting using an internal comparator that trips at 1020 mA (typical). If the output is shorted to ground, then the device enters a timed current-limit mode where the NFET is turned on for a longer duration until the inductor current falls below a low threshold, ensuring inductor current has more time to decay, and thereby preventing runaway.

7.4 Device Functional Modes

There are two modes of operation depending on the current required: Pulse Width Modulation (PWM) and shutdown. The device operates in PWM mode throughout the I_{OUT} range. Shutdown mode turns off the device, offering the lowest current consumption (I_{SHUTDOWN} = 0.01 µA, typical). Additional features include soft-start, undervoltage protection, and current overload protection.

STRUMENTS

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

8.1.1 Soft-Start

The LM3674 has a soft-start circuit that limits in-rush current during start-up. During start-up the switch current limit is increased in steps. Soft-start is activated only if EN goes from logic low to logic high after V_{IN} reaches 2.7 V. Soft-start is implemented by increasing switch current limit in steps of 70 mA, 140 mA, 280 mA, and 1020 mA (typical switch current limit). The start-up time thereby depends on the output capacitor and load current demanded at start-up. Typical start-up times with 10-µF output capacitor and a 300-mA load current is 350 µs and with a 10-mA load current is 240 µs.

8.1.2 Low-Dropout (LDO) Operation

The LM3674-ADJ can operate at 100% duty-cycle (no switching, PMOS switch completely on) for low-dropout support of the output voltage. In this way the output voltage will be controlled down to the lowest possible input voltage. When the device operates near 100% duty-cycle, the output voltage supply ripple is slightly higher, approximately 25 mV.

The minimum input voltage needed to support the output voltage is:

 $V_{IN,MIN} = I_{LOAD} \times (R_{DSON(P)} + R_{INDUCTOR}) + V_{OUT}$

where:

- \bullet I_{LOAD} is load current
- $R_{DSON (P)}$ is drain-to-source resistance of PFET switch in the triode region
- R_{INDUCTOR} is inductor resistance (3)

8.2 Typical Applications

Figure 19. Fixed-Voltage Typical Application Circuit

8.2.1.1 Design Requirements

8.2.1.2 Detailed Design Procedure

8.2.1.2.1 Inductor Selection

There are two main considerations when choosing an inductor:

- The inductor should not saturate.
- The inductor current ripple should be small enough to achieve the desired output voltage ripple.

Different saturation current rating specifications are followed by different manufacturers so attention must be given to details. Saturation current ratings are typically specified at 25°C. However, ratings at the maximum ambient temperature of the application should be requested from the manufacturer. The minimum value of inductance to ensure good performance is 1.76 μ H at I_{LIM} (typical) DC current over the ambient temperature range. Shielded inductors radiate less noise and should be preferred.

There are two methods to choose the inductor saturation current rating:

Method 1:

The saturation current is greater than the sum of the maximum load current and the worst case average to peak inductor current. This can be written as:

ISAT > IOUTMAX + IRIPPLE

where
$$
I_{RIPPLE} = \left(\frac{V_{IN} - V_{OUT}}{2 \times L}\right) \left(\frac{V_{OUT}}{V_{IN}}\right) \left(\frac{1}{f}\right)
$$

and

- I_{RIPPLE} is average-to-peak inductor current
- I_{OUTMAX} is maximum load current (600 mA)
- \bullet V_{IN} is maximum input voltage in application
- L is minimum inductor value including worst case tolerances (30% drop can be considered for method 1
- f is minimum switching frequency (1.6 MHz)
- V_{OUT} is output voltage (5)

Method 2:

A more conservative and recommended approach is to choose an inductor that has saturation current rating greater than the maximum current limit of 1200 mA.

A 2.2-µH inductor with a saturation current rating of at least 1200 mA is recommended for most applications. The resistance of the inductor should be less than 0.3 Ω for good efficiency. [Table](#page-12-0) 1 lists suggested inductors and suppliers. For low-cost applications, an unshielded bobbin inductor is suggested. For noise critical applications, a toroidal or shielded-bobbin inductor should be used. A good practice is to lay out the board with overlapping footprints of both types for design flexibility. This allows substitution of a low-noise toroidal inductor in the event that noise from low-cost bobbin models is unacceptable.

Table 1. Suggested Inductors and Their Suppliers

(4)

[LM3674](http://www.ti.com/product/lm3674?qgpn=lm3674)

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8.2.1.2.2 Input Capacitor Selection

A ceramic input capacitor of 4.7 µF, 6.3 V is sufficient for most applications. Place the input capacitor as close as possible to the V_{IN} pin of the device. A larger value may be used for improved input voltage filtering. Use X7R or X5R types; do not use Y5V. DC bias characteristics of ceramic capacitors must be considered when selecting case sizes like 0805 and 0603. The minimum input capacitance to ensure good performance is 2.2 µF at 3-V DC bias; 1.5 µF at 5-V DC bias including tolerances and over ambient temperature range. The input filter capacitor supplies current to the PFET switch of the LM3674 in the first half of each cycle and reduces voltage ripple imposed on the input power source. The low equivalent series resistance (ESR) of a ceramic capacitor provides the best noise filtering of the input voltage spikes due to this rapidly changing current. Select a capacitor with sufficient ripple current rating. The input current ripple can be calculated as:

$$
I_{RMS} = I_{OUTMAX} \times \sqrt{\frac{V_{OUT}}{V_{IN}}} \times (1 - \frac{V_{OUT}}{V_{IN}} + \frac{r^2}{12})
$$

$$
r = \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{L \times f \times I_{OUTMAX} \times V_{IN}} \text{ The worst case is when}
$$

(6)

(8)

8.2.1.2.3 Output Capacitor Selection

A ceramic output capacitor of 10 µF, 6.3 V is sufficient for most applications. Use X7R or X5R types; do not use Y5V. DC bias characteristics of ceramic capacitors must be considered when selecting case sizes like 0805 and 0603. DC-bias characteristics vary from manufacturer to manufacturer and DC-bias curves should be requested from them as part of the capacitor selection process.

The minimum output capacitance to ensure good performance is 5.75 µF at 1.8 V DC bias including tolerances and over ambient temperature range. The output filter capacitor smoothes out current flow from the inductor to the load, helps maintain a steady output voltage during transient load changes, and reduces output voltage ripple. These capacitors must be selected with sufficient capacitance and sufficiently low ESR to perform these functions.

The output voltage ripple is caused by the charging and discharging of the output capacitor and by the R_{ESR} and can be calculated as:

Voltage peak-to-peak ripple due to capacitance can be expressed as:

$$
V_{\rm PP-C} = \frac{I_{\rm ripple}}{f \times 4 \times C} \tag{7}
$$

Voltage peak-to-peak ripple due to ESR:

$$
V_{\text{OUT}} = V_{\text{PP-ESR}} = I_{\text{PP}} \cdot R_{\text{ESR}}
$$

Because these two components are out of phase, the root mean squared (rms) value can be used to get an approximate value of peak-to-peak ripple.

Voltage peak-to-peak ripple, rms:

$$
V_{PP\text{-RMS}} = \sqrt{V_{PP\text{-}C}^2 + V_{PP\text{-}ESR}^2}
$$
\n(9)

Note that the output ripple is dependent on the current ripple and the equivalent series resistance of the output capacitor (R_{ESR}) .

The R_{ESR} is frequency-dependent (as well as temperature-dependent); make sure the value used for calculations is at the switching frequency of the part.

Table 2. Suggested Capacitors and Their Suppliers

8.2.1.3 Application Curves

Table 3. Related Plots

8.2.2 Typical Application Circuit for Adjustable Voltage Option

8.2.2.1 Design Requirements

8.2.2.2 Detailed Design Procedure

8.2.2.2.1 Output Voltage Selection for Adjustable (LM3674-ADJ)

The output voltage of the adjustable parts can be programmed through the resistor network connected from V_{OUT} to FB then to GND. V_{OUT} will be adjusted to make FB equal to 0.5 V. The resistor from FB to GND (R2) should be 200 kΩ to keep the current drawn through this network small but large enough that it is not susceptible to noise. If R₂ is 200 kΩ, and given the V_{FB} is 0.5 V, then the current through the resistor feedback network will be 2.5 µA. The output voltage formula is:

$$
V_{OUT} = V_{FB} * (\frac{R_1}{R_2} + 1)
$$

where:

- V_{OUT} = Output voltage (V)
- V_{FB} = Feedback voltage (0.5 V typical)
- R_1 = Resistor from V_{OUT} to FB (Ω)
- R_2 = Resistor from FB to GND (Ω) (10)

For any output voltage greater than or equal to 1.0 V, a frequency zero must be added at 45 kHz for stability. The formula is:

$$
C_1 = \frac{1}{2 \times \pi \times R_1 \times 45 \text{ kHz}}
$$
\n(11)

 $C_1 = \frac{1}{2 \times \pi \times R_1 \times 45 \text{ kHz}}$
tput voltages greate
re at the same frequence For output voltages greater than or equal to 2.5 V, a pole must also be placed at 45 kHz as well. If the pole and zero are at the same frequency the formula for calculation of C2 is:

$$
C_2 = \frac{1}{2 \times \pi \times R_2 \times 45 \text{ kHz}}
$$
(12)

The formula for location of zero and pole frequency created by adding C1,C2 are given below. It can be seen that by adding C1, a zero as well as a higher frequency pole is introduced.

$$
Fz = \frac{1}{(2 * \pi * R1 * C1)} Fp = \frac{1}{2 * \pi * (R1 \| R2) * (C1 + C2)}
$$
\n(13)

See [Table](#page-15-0) 4.

Table 4. Adjustable LM3674 Configurations for Various V_{OUT}

VOUT (V)	$R1$ (k Ω)	$R2$ (k Ω)	C1(pF)	C2(pF)	$L(\mu H)$	$C_{IN}(\mu F)$	C_{OUT} (µF)
1.0	200	200	18	None	2.2	4.7	10
1.1	191	158	18	None	2.2	4.7	10
1.2	280	200	12	None	2.2	4.7	10
1.5	357	178	10	None	2.2	4.7	10
1.6	442	200	8.2	None	2.2	4.7	10
1.7	432	178	8.2	None	2.2	4.7	10
1.8	464	178	8.2	None	2.2	4.7	10
1.875	523	191	6.8	None	2.2	4.7	10
2.5	402	100	8.2	None	2.2	4.7	10
2.8	464	100	8.2	33	2.2	4.7	10
3.3	562	100	6.8	33	2.2	4.7	10

8.2.2.3 Application Curves

Table 5. Related Plots

9 Power Supply Recommendations

The LM3674 requires a single supply input voltage. This voltage can range between 2.7 V to 5.5 V and be able to supply enough current for a given application.

10 Layout

10.1 Layout Guidelines

PC board layout is an important part of DC-DC converter design. Poor board layout can disrupt the performance of a DC-DC converter and surrounding circuitry by contributing to EMI, ground bounce, and resistive voltage loss in the traces. These can send erroneous signals to the DC-DC converter device, resulting in poor regulation or instability.

Good layout for the LM3674 can be implemented by following a few simple design rules, as illustrated in [Figure](#page-17-2) 21.

- 1. Place the LM3674, inductor and filter capacitors close together and make the traces short. The traces between these components carry relatively high switching currents and act as antennas. Following this rule reduces radiated noise. Special care must by given to place the input filter capacitor very close to the V_{IN} and GND pin.
- 2. Arrange the components so that the switching current loops curl in the same direction. During the first half of each cycle, current flows from the input filter capacitor, through the LM3674 and inductor to the output filter capacitor and back through ground, forming a current loop. In the second half of each cycle, current is pulled up from ground, through the LM3674 by the inductor, to the output filter capacitor and then back through ground, forming a second current loop. Routing these loops so the current curls in the same direction prevents magnetic field reversal between the two half-cycles and reduces radiated noise.
- 3. Connect the ground pins of the LM3674, and filter capacitors together using generous component-side copper fill as a pseudo-ground plane. Then, connect this to the ground-plane (if one is used) with several vias. This reduces ground-plane noise by preventing the switching currents from circulating through the ground plane. It also reduces ground bounce at the LM3674 by giving it a low-impedance ground connection.
- 4. Use wide traces between the power components and for power connections to the DC-DC converter circuit. This reduces voltage errors caused by resistive losses across the traces.
- 5. Route noise sensitive traces, such as the voltage feedback path, away from noisy traces between the power components. The voltage feedback trace must remain close to the LM3674 circuit and should be direct but should be routed opposite to noisy components. This reduces the EMI radiated onto the voltage feedback trace of the DC-DC converter. A good approach is to route the feedback trace on another layer and to have a ground plane between the top layer and layer on which the feedback trace is routed. In the same manner for the adjustable part it is desired to have the feedback dividers on the bottom layer.
- 6. Place noise sensitive circuitry, such as radio IF blocks, away from the DC-DC converter, CMOS digital blocks

Layout Guidelines (continued)

and other noisy circuitry. Interference with noise-sensitive circuitry in the system can be reduced through distance.

In mobile phones, for example, a common practice is to place the DC-DC converter on one corner of the board, arrange the CMOS digital circuitry around it (because this also generates noise), and then place sensitive preamplifiers and IF stages on the diagonally opposing corner. Often, the sensitive circuitry is shielded with a metal pan and power to it is post-regulated to reduce conducted noise by using low-dropout linear regulators.

10.2 Layout Example

Figure 21. Board Layout Design Rules for the LM3674

11 Device and Documentation Support

11.1 Device Support

11.1.1 Third-Party Products Disclaimer

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11.2 Trademarks

All trademarks are the property of their respective owners.

11.3 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.4 Glossary

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

PACKAGE OPTION ADDENDUM

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

PACKAGE MATERIALS INFORMATION

www.ti.com 10-Jan-2024

PACKAGE OUTLINE

DBV0005A SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. Refernce JEDEC MO-178.
- 4. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25 mm per side.
- 5. Support pin may differ or may not be present.

EXAMPLE BOARD LAYOUT

DBV0005A SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

DBV0005A SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.

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