

# TLV935x 3.5-MHz, 40-V, RRO, MUX-Friendly Operational Amplifier for Cost-Sensitive Systems

## 1 Features

- Low offset voltage:  $\pm 350 \mu\text{V}$
- Low offset voltage drift:  $\pm 1.5 \mu\text{V}/^\circ\text{C}$
- Low noise:  $15 \text{ nV}/\sqrt{\text{Hz}}$  at 1 kHz
- High common-mode rejection: 110 dB
- Low bias current:  $\pm 10 \text{ pA}$
- Rail-to-rail output
- MUX-friendly/comparator inputs
  - Amplifier operates with differential inputs up to supply rail
  - Amplifier can be used in open-loop or as comparator
- Wide bandwidth: 3.5-MHz GBW
- High slew rate:  $20 \text{ V}/\mu\text{s}$
- Low quiescent current:  $600 \mu\text{A}$  per amplifier
- Wide supply:  $\pm 2.25 \text{ V}$  to  $\pm 20 \text{ V}$ , 4.5 V to 40 V
- Robust EMIRR performance: EMI/RFI filters on input pins
- Differential and common-mode input voltage range to supply rail

## 2 Applications

- [AC and motor drive servo control module](#)
- [AC and motor drive power stage module](#)
- [Test and measurement equipment](#)
- [Programmable logic controllers](#)

## 3 Description

The TLV935x family (TLV9351, TLV9352, and TLV9354) is a family of 40-V cost-optimized operational amplifiers.

These devices offer strong DC and AC specifications, including rail-to-rail output, low offset ( $\pm 350 \mu\text{V}$ , typical), low offset drift ( $\pm 1.5 \mu\text{V}/^\circ\text{C}$ , typical), and 3.5-MHz bandwidth.

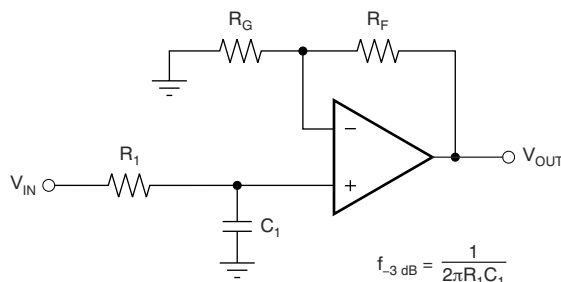
Unique features such as differential input-voltage range to the supply rail, high output current ( $\pm 60 \text{ mA}$ ), and high slew rate ( $20 \text{ V}/\mu\text{s}$ ) make the TLV935x a robust operational amplifier for high-voltage, cost-sensitive applications.

The TLV935x family of op amps is available in standard packages and is specified from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ .

### Device Information

PART NUMBER <sup>(1)</sup>	PACKAGE	BODY SIZE (NOM)
TLV9351	SOT-23 (5)	2.90 mm × 1.60 mm
	SC70 (5)	2.00 mm × 1.25 mm
TLV9352	SOIC (8)	4.90 mm × 3.90 mm
	SOT-23 (8)	1.60 mm × 2.90 mm
	TSSOP (8)	3.00 mm × 4.40 mm
	VSSOP (8)	3.00 mm × 3.00 mm
TLV9354	SOIC (14)	8.65 mm × 3.90 mm
	SOT-23 (14)	4.20 mm × 1.90 mm
	TSSOP (14)	5.00 mm × 4.40 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.



$$f_{-3 \text{ dB}} = \frac{1}{2\pi R_1 C_1}$$

$$\frac{V_{\text{OUT}}}{V_{\text{IN}}} = \left(1 + \frac{R_F}{R_G}\right) \left(\frac{1}{1 + sR_1 C_1}\right)$$

### TLV935x in a Single-Pole, Low-Pass Filter



## Table of Contents

<b>1 Features</b> .....	1	7.4 Device Functional Modes.....	27
<b>2 Applications</b> .....	1	<b>8 Application Information Disclaimer</b> .....	28
<b>3 Description</b> .....	1	8.1 Application Information.....	28
<b>4 Revision History</b> .....	2	8.2 Typical Applications.....	28
<b>5 Pin Configuration and Functions</b> .....	4	<b>9 Power Supply Recommendations</b> .....	30
<b>6 Specifications</b> .....	7	<b>10 Layout</b> .....	30
6.1 Absolute Maximum Ratings.....	7	10.1 Layout Guidelines.....	30
6.2 ESD Ratings.....	7	10.2 Layout Example.....	31
6.3 Recommended Operating Conditions.....	7	<b>11 Device and Documentation Support</b> .....	33
6.4 Thermal Information for Single Channel.....	8	11.1 Device Support.....	33
6.5 Thermal Information for Dual Channel.....	8	11.2 Documentation Support.....	33
6.6 Thermal Information for Quad Channel.....	8	11.3 Receiving Notification of Documentation Updates..	33
6.7 Electrical Characteristics.....	9	11.4 Support Resources.....	33
6.8 Typical Characteristics.....	12	11.5 Trademarks.....	33
<b>7 Detailed Description</b> .....	19	11.6 Electrostatic Discharge Caution.....	34
7.1 Overview.....	19	11.7 Glossary.....	34
7.2 Functional Block Diagram.....	19	<b>12 Mechanical, Packaging, and Orderable Information</b> .....	35
7.3 Feature Description.....	20		

## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision D (May 2021) to Revision E (January 2022)	Page
• Added SOT-23-14 (DYY) package in <i>Device Information</i> .....	1
• Added SOT-23-14 (DYY) package and pin functions in <i>Pin Configurations and Functions</i> section.....	4
• Added SOT-23-14 (DYY) package in <i>Thermal Information for Quad Channel</i> section.....	8
• Changed input resistor values in <i>Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application in Electrical Overstress</i> section to more closely resemble device .....	25

Changes from Revision C (December 2020) to Revision D (May 2021)	Page
• Changed VSSOP (8) package in <i>Device Information</i> from Preview to Active.....	1
• Removed preview notation on VSSOP-8 (DGK) package in <i>Pin Configurations and Functions</i> section.....	4

Changes from Revision B (August 2020) to Revision C (December 2020)	Page
• Changed SOIC (14) package in <i>Device Information</i> from Preview to Active.....	1
• Changed TSSOP (14) package in <i>Device Information</i> from Preview to Active.....	1
• Changed SOT-23 (5) package in <i>Device Information</i> from Preview to Active.....	1
• Changed SC70 (5) package in <i>Device Information</i> from Preview to Active.....	1
• Removed preview notation on SOT-23 (DBV) package in <i>Pin Configurations and Functions</i> section.....	4
• Removed preview notation on SC70 (DCK) package in <i>Pin Configurations and Functions</i> section.....	4
• Removed preview notation on SOIC-14 (D) and TSSOP-14 (PW) packages in <i>Pin Configurations and Functions</i> section.....	4
• Corrected package type column headings in the Pin Functions: TLV9351 table.....	4
• Added updates to the <i>Related Documentation</i> section.....	33

Changes from Revision A (March 2020) to Revision B (August 2020)	Page
• Updated the numbering format for tables, figures, and cross-references throughout the document.....	1
• Added SOT-23 (8) package on <i>Device Information</i> section.....	1
• Removed preview notation on SOT-23 (DDF) package in <i>Pin Configurations and Functions</i> section.....	4

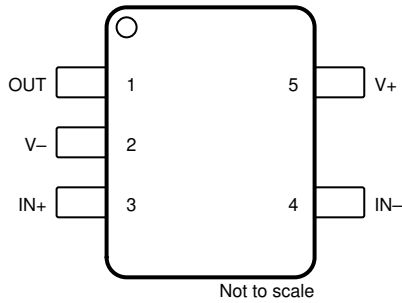
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**Changes from Revision \* (November 2019) to Revision A (March 2020)**

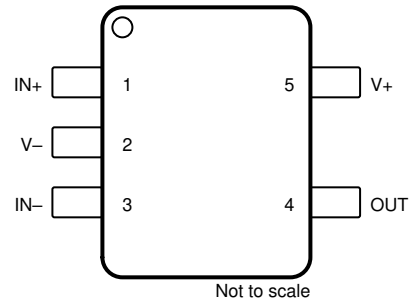
**Page**

- Changed SOIC (8) package status on *Device Information* from Preview to Active ..... 1
  - Changed TSSOP (8) package status on *Device Information* from Preview to Active ..... 1
  - Removed preview notation on SOIC-8 (D) and TSSOP-8 (PW) packages in *Pin Configurations and Functions* ..... 4
  - Added *Typical Characteristics* section in *Specifications* section..... 12
-

## 5 Pin Configuration and Functions



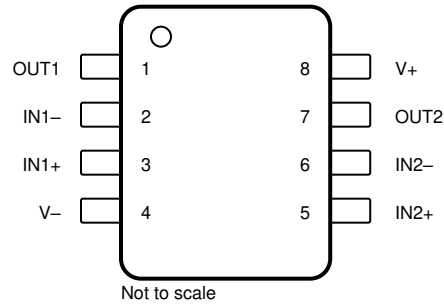
**Figure 5-1. TLV9351 DBV Package  
5-Pin SOT-23  
(Top View)**



**Figure 5-2. TLV9351 DCK Package  
5-Pin SC70  
(Top View)**

**Table 5-1. Pin Functions: TLV9351**

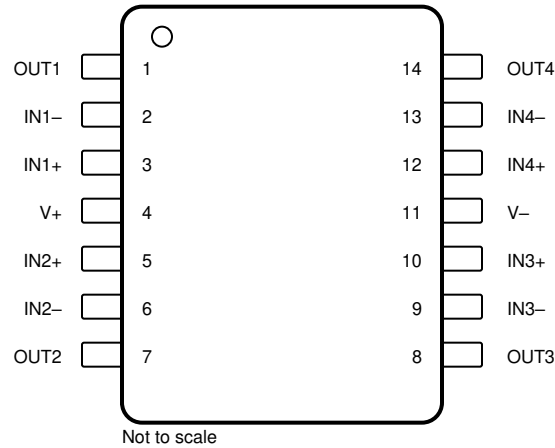
NAME	PIN		I/O	DESCRIPTION
	SOT-23	SC70		
+IN	3	1	I	Noninverting input
-IN	4	3	I	Inverting input
OUT	1	4	O	Output
V+	5	5	—	Positive (highest) power supply
V-	2	2	—	Negative (lowest) power supply



**Figure 5-3. TLV9352 D, DDF, DGK, and PW Package  
8-Pin SOIC, SOT-23, TSSOP, and VSSOP  
(Top View)**

**Table 5-2. Pin Functions: TLV9352**

PIN		I/O	DESCRIPTION
NAME	NO.		
+IN A	3	I	Noninverting input, channel A
+IN B	5	I	Noninverting input, channel B
-IN A	2	I	Inverting input, channel A
-IN B	6	I	Inverting input, channel B
OUT A	1	O	Output, channel A
OUT B	7	O	Output, channel B
V+	8	—	Positive (highest) power supply
V-	4	—	Negative (lowest) power supply



**Figure 5-4. TLV9354 D, PW, and DYY Packages  
14-Pin SOIC, TSSOP, and SOT-23  
(Top View)**

**Table 5-3. Pin Functions: TLV9354**

PIN		I/O	DESCRIPTION
NAME	NO.		
+IN A	3	I	Noninverting input, channel A
+IN B	5	I	Noninverting input, channel B
+IN C	10	I	Noninverting input, channel C
+IN D	12	I	Noninverting input, channel D
-IN A	2	I	Inverting input, channel A
-IN B	6	I	Inverting input, channel B
-IN C	9	I	Inverting input, channel C
-IN D	13	I	Inverting input, channel D
OUT A	1	O	Output, channel A
OUT B	7	O	Output, channel B
OUT C	8	O	Output, channel C
OUT D	14	O	Output, channel D
V+	4	—	Positive (highest) power supply
V-	11	—	Negative (lowest) power supply

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating ambient temperature range (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage, $V_S = (V+) - (V-)$		0	42	V
Signal input pins	Common-mode voltage <sup>(3)</sup>	$(V-) - 0.5$	$(V+) + 0.5$	V
	Differential voltage <sup>(3)</sup>		$V_S + 0.2$	V
	Current <sup>(3)</sup>	-10	10	mA
Output short-circuit <sup>(2)</sup>		Continuous		
Operating ambient temperature, $T_A$		-55	150	°C
Junction temperature, $T_J$			150	°C
Storage temperature, $T_{stg}$		-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Short-circuit to ground, one amplifier per package.
- (3) Input pins are diode-clamped to the power-supply rails. Input signals that may swing more than 0.5 V beyond the supply rails must be current limited to 10 mA or less.

### 6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±1000	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating ambient temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_S$	Supply voltage, $(V+) - (V-)$	4.5	40	V
$V_I$	Input voltage range	$(V-) - 0.1$	$(V+) - 2$	V
$T_A$	Specified temperature	-40	125	°C

## 6.4 Thermal Information for Single Channel

THERMAL METRIC <sup>(1)</sup>		TLV9351		UNIT
		DBV (SOT-23)	DCK (SC70)	
		5 PINS	5 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	185.7	202.6	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	108.2	101.5	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	54.5	47.8	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	31.2	18.8	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	54.2	47.4	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.5 Thermal Information for Dual Channel

THERMAL METRIC <sup>(1)</sup>		TLV9352				UNIT
		D (SOIC)	DDF (SOT-23)	DGK (VSSOP)	PW (TSSOP)	
		8 PINS	8 PINS	8 PINS	8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	138.7	143.5	177.1	185.1	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	78.7	79.9	68.1	74.0	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	82.2	61.6	98.4	115.7	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	27.8	5.7	12.1	12.3	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	81.4	61.3	96.6	114.0	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	TBD	N/A	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).

## 6.6 Thermal Information for Quad Channel

THERMAL METRIC <sup>(1)</sup>		TLV9354			UNIT
		D (SOIC)	DYY (SOT-23)	PW (TSSOP)	
		14 PINS	14 PINS	14 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	101.2	110.6	131.1	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	57.8	53.7	52.1	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	57.2	35.3	75.6	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	18.6	2.2	8.1	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	56.5	35.0	74.6	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	N/A	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, [SPRA953](#).



## 6.7 Electrical Characteristics

For  $V_S = (V+) - (V-) = 4.5\text{ V to }40\text{ V}$  ( $\pm 2.25\text{ V to } \pm 20\text{ V}$ ) at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>OFFSET VOLTAGE</b>							
$V_{OS}$	Input offset voltage	$V_{CM} = V-$		$\pm 0.35$	$\pm 1.8$		mV
			$T_A = -40^\circ\text{C to } 125^\circ\text{C}$			$\pm 2$	
$dV_{OS}/dT$	Input offset voltage drift		$T_A = -40^\circ\text{C to } 125^\circ\text{C}$		$\pm 1.5$		$\mu\text{V}/^\circ\text{C}$
PSRR	Input offset voltage versus power supply	$V_{CM} = V-$	$T_A = -40^\circ\text{C to } 125^\circ\text{C}$		$\pm 2$	$\pm 5$	$\mu\text{V}/\text{V}$
	Channel separation	$f = 0\text{ Hz}$			5		$\mu\text{V}/\text{V}$
<b>INPUT BIAS CURRENT</b>							
$I_B$	Input bias current				$\pm 10$		pA
$I_{OS}$	Input offset current				$\pm 10$		pA
<b>NOISE</b>							
$E_N$	Input voltage noise	$f = 0.1\text{ Hz to } 10\text{ Hz}$			2		$\mu\text{V}_{PP}$
					0.33		$\mu\text{V}_{RMS}$
$e_N$	Input voltage noise density	$f = 1\text{ kHz}$			15		$\text{nV}/\sqrt{\text{Hz}}$
		$f = 10\text{ kHz}$			14		
$i_N$	Input current noise	$f = 1\text{ kHz}$			2		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>							
$V_{CM}$	Common-mode voltage range			$(V-) - 0.2$		$(V+) - 2$	V
CMRR	Common-mode rejection ratio	$V_S = 40\text{ V}, (V-) - 0.1\text{ V} < V_{CM} < (V+) - 2\text{ V}$ (Main input pair)	$T_A = -40^\circ\text{C to } 125^\circ\text{C}$	95	110		dB
		$V_S = 4.5\text{ V}, (V-) - 0.1\text{ V} < V_{CM} < (V+) - 2\text{ V}$ (Main input pair)		84	90		
<b>INPUT CAPACITANCE</b>							
$Z_{ID}$	Differential				$100 \parallel 3$		$\text{M}\Omega \parallel \text{pF}$
$Z_{ICM}$	Common-mode				$6 \parallel 1$		$\text{T}\Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>							
$A_{OL}$	Open-loop voltage gain	$V_S = 40\text{ V}, V_{CM} = V-$ $(V-) + 0.1\text{ V} < V_O < (V+) - 0.1\text{ V}$		120	130		dB
			$T_A = -40^\circ\text{C to } 125^\circ\text{C}$			127	

## 6.7 Electrical Characteristics (continued)

For  $V_S = (V+) - (V-) = 4.5\text{ V to }40\text{ V}$  ( $\pm 2.25\text{ V to } \pm 20\text{ V}$ ) at  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$ , unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>FREQUENCY RESPONSE</b>						
GBW	Gain-bandwidth product			3.5		MHz
SR	Slew rate	$V_S = 40\text{ V}$ , $G = +1$ , $C_L = 20\text{ pF}$		20		V/ $\mu\text{s}$
$t_s$	Settling time	To 0.01%, $V_S = 40\text{ V}$ , $V_{STEP} = 10\text{ V}$ , $G = +1$ , $CL = 20\text{ pF}$		5		$\mu\text{s}$
		To 0.01%, $V_S = 40\text{ V}$ , $V_{STEP} = 2\text{ V}$ , $G = +1$ , $CL = 20\text{ pF}$		4		
		To 0.1%, $V_S = 40\text{ V}$ , $V_{STEP} = 10\text{ V}$ , $G = +1$ , $CL = 20\text{ pF}$		4		
		To 0.1%, $V_S = 40\text{ V}$ , $V_{STEP} = 2\text{ V}$ , $G = +1$ , $CL = 20\text{ pF}$		3		
	Phase margin	$G = +1$ , $R_L = 10\text{ k}\Omega$		60		$^\circ$
	Overload recovery time	$V_{IN} \times \text{gain} > V_S$		600		ns
THD+N	Total harmonic distortion + noise	$V_S = 40\text{ V}$ , $V_O = 1\text{ V}_{RMS}$ , $G = 1$ , $f = 1\text{ kHz}$		0.001%		
<b>OUTPUT</b>						
	Voltage output swing from rail	Positive and negative rail headroom	$V_S = 40\text{ V}$ , $R_L = \text{no load}^{(1)}$	5	10	mV
			$V_S = 40\text{ V}$ , $R_L = 10\text{ k}\Omega$	50	55	
			$V_S = 40\text{ V}$ , $R_L = 2\text{ k}\Omega$	200	250	
			$V_S = 4.5\text{ V}$ , $R_L = \text{no load}^{(1)}$	1		
			$V_S = 4.5\text{ V}$ , $R_L = 10\text{ k}\Omega$	20	30	
			$V_S = 4.5\text{ V}$ , $R_L = 2\text{ k}\Omega$	40	75	
$I_{SC}$	Short-circuit current			$\pm 60$		mA
$C_{LOAD}$	Capacitive load drive			300		pF
$Z_O$	Open-loop output impedance	$f = 1\text{ MHz}$ , $I_O = 0\text{ A}$		600		$\Omega$
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current per amplifier	$V_{CM} = V-$ , $I_O = 0\text{ A}$		650	800	$\mu\text{A}$
			$T_A = -40^\circ\text{C to }125^\circ\text{C}$		850	

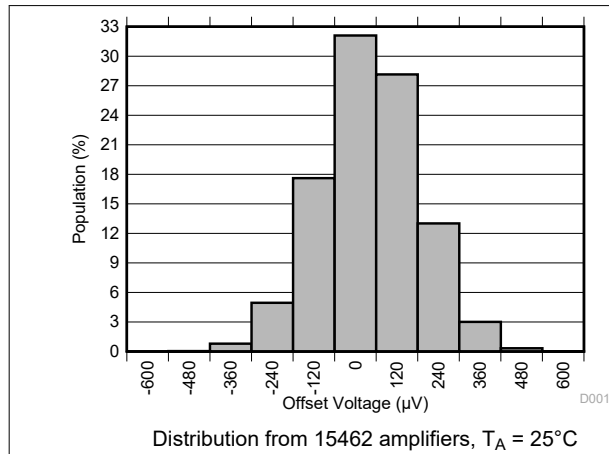
(1) Specified by characterization only.

**Table 6-1. Table of Graphs**

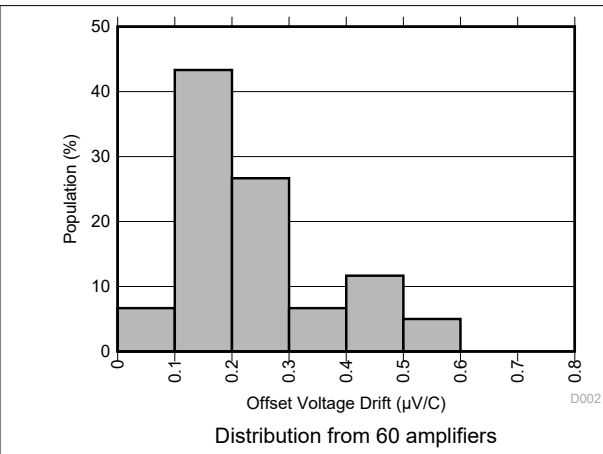
DESCRIPTION	FIGURE
Offset Voltage Production Distribution	Figure 6-1
Offset Voltage Drift Distribution	Figure 6-2
Offset Voltage vs Temperature	Figure 6-3, Figure 6-4
Offset Voltage vs Common-Mode Voltage	Figure 6-5, Figure 6-6, Figure 6-7, Figure 6-8
Offset Voltage vs Power Supply	Figure 6-9
Open-Loop Gain and Phase vs Frequency	Figure 6-10
Closed-Loop Gain and Phase vs Frequency	Figure 6-11
Input Bias Current vs Common-Mode Voltage	Figure 6-12
Input Bias Current vs Temperature	Figure 6-13
Output Voltage Swing vs Output Current	Figure 6-14, Figure 6-15
CMRR and PSRR vs Frequency	Figure 6-16
CMRR vs Temperature	Figure 6-17
PSRR vs Temperature	Figure 6-18
0.1-Hz to 10-Hz Noise	Figure 6-19
Input Voltage Noise Spectral Density vs Frequency	Figure 6-20
THD+N Ratio vs Frequency	Figure 6-21
THD+N vs Output Amplitude	Figure 6-22
Quiescent Current vs Supply Voltage	Figure 6-23
Quiescent Current vs Temperature	Figure 6-24
Open Loop Voltage Gain vs Temperature	Figure 6-25
Open Loop Output Impedance vs Frequency	Figure 6-26
Small Signal Overshoot vs Capacitive Load (100-mV Output Step)	Figure 6-27, Figure 6-28
Phase Margin vs Capacitive Load	Figure 6-29
No Phase Reversal	Figure 6-30
Positive Overload Recovery	Figure 6-31
Negative Overload Recovery	Figure 6-32
Small-Signal Step Response (100 mV)	Figure 6-33, Figure 6-34
Large-Signal Step Response	Figure 6-35, Figure 6-36, Figure 6-37
Short-Circuit Current vs Temperature	Figure 6-38
Maximum Output Voltage vs Frequency	Figure 6-39
Channel Separation vs Frequency	Figure 6-40
EMIRR vs Frequency	Figure 6-41

## 6.8 Typical Characteristics

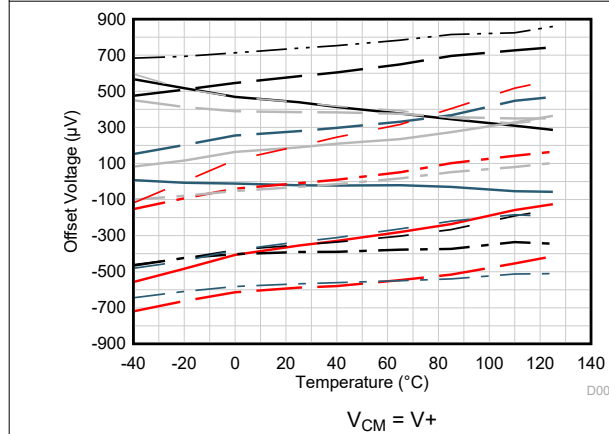
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)



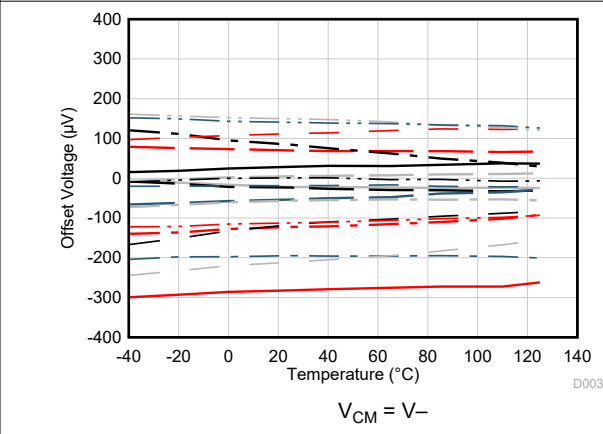
**Figure 6-1. Offset Voltage Production Distribution**



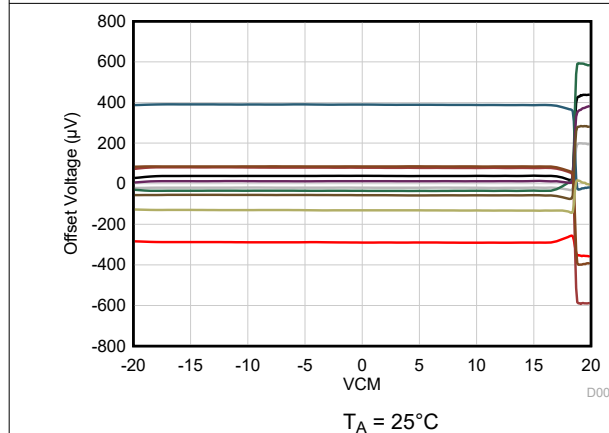
**Figure 6-2. Offset Voltage Drift Distribution**



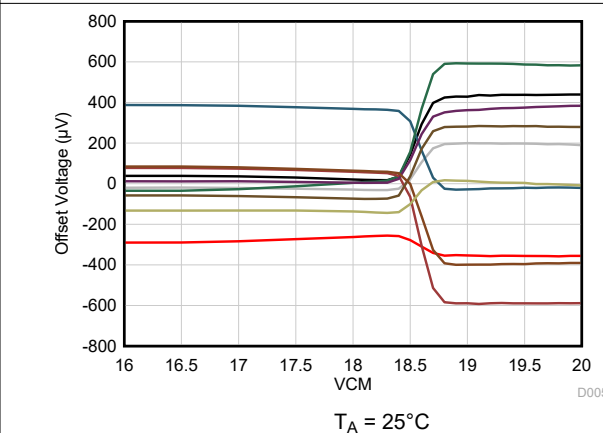
**Figure 6-3. Offset Voltage vs Temperature**



**Figure 6-4. Offset Voltage vs Temperature**



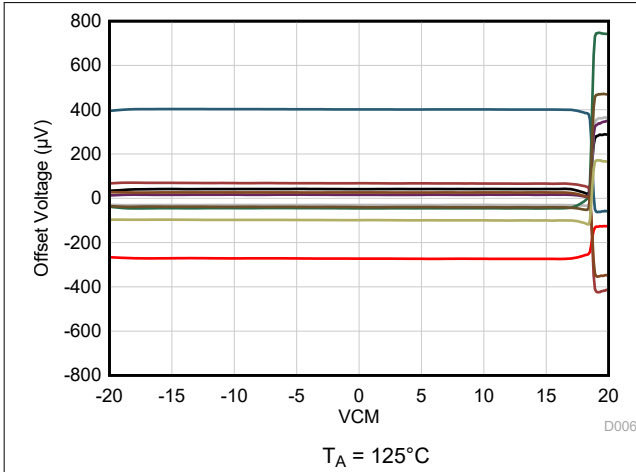
**Figure 6-5. Offset Voltage vs Common-Mode Voltage**



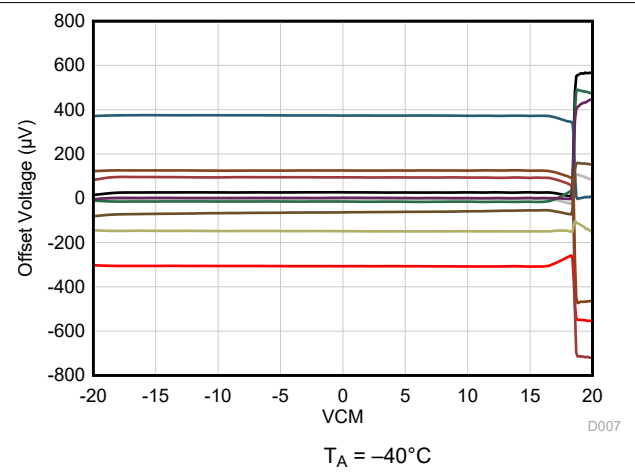
**Figure 6-6. Offset Voltage vs Common-Mode Voltage (Transition Region)**

### 6.8 Typical Characteristics (continued)

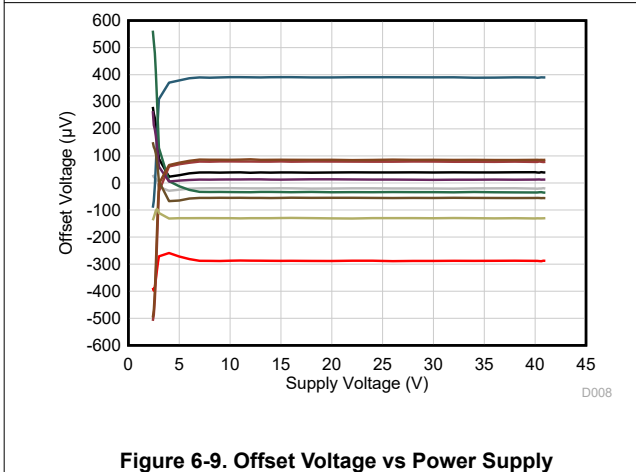
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)



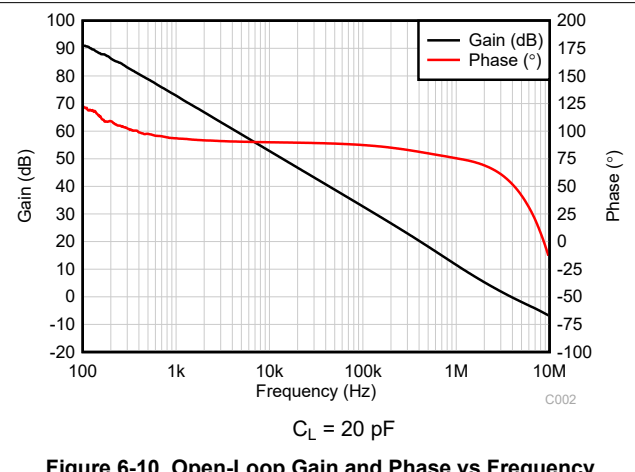
**Figure 6-7. Offset Voltage vs Common-Mode Voltage**



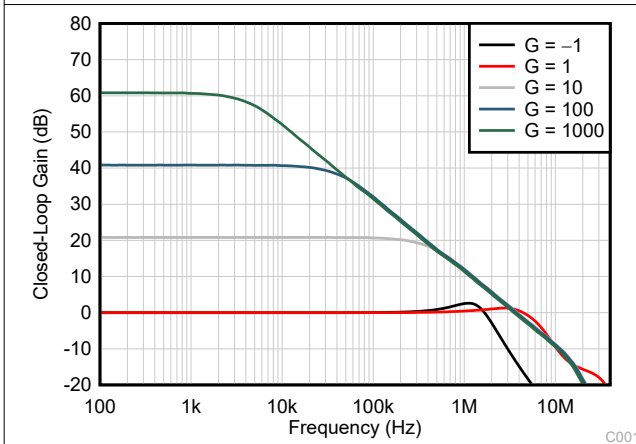
**Figure 6-8. Offset Voltage vs Common-Mode Voltage**



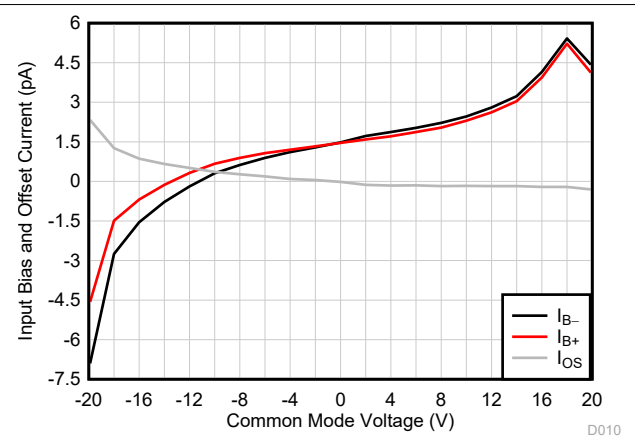
**Figure 6-9. Offset Voltage vs Power Supply**



**Figure 6-10. Open-Loop Gain and Phase vs Frequency**



**Figure 6-11. Closed-Loop Gain vs Frequency**



**Figure 6-12. Input Bias Current vs Common-Mode Voltage**

## 6.8 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)

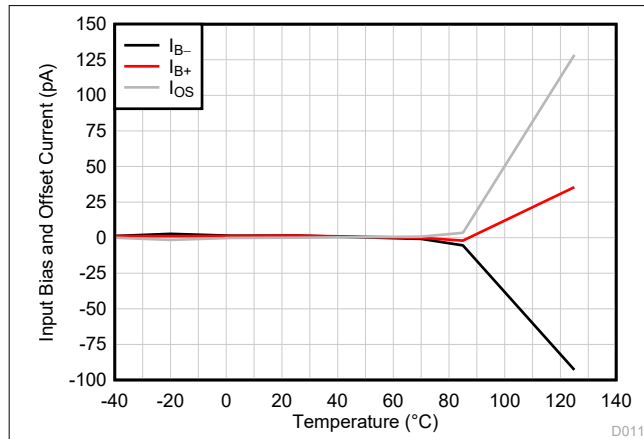


Figure 6-13. Input Bias Current vs Temperature

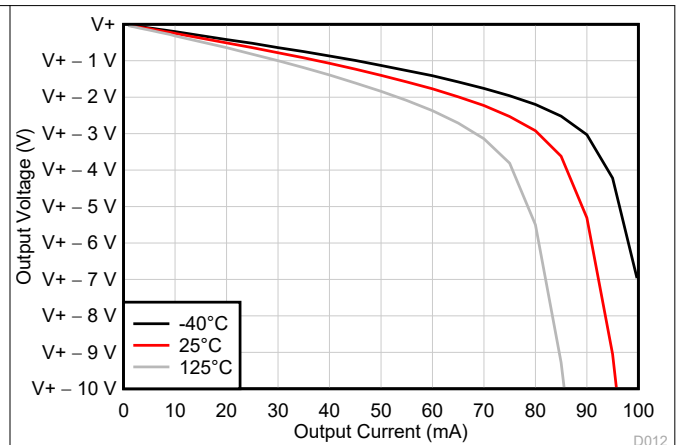


Figure 6-14. Output Voltage Swing vs Output Current (Sourcing)

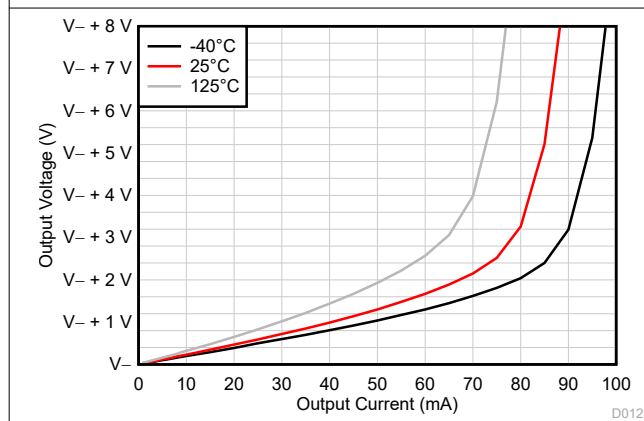


Figure 6-15. Output Voltage Swing vs Output Current (Sinking)

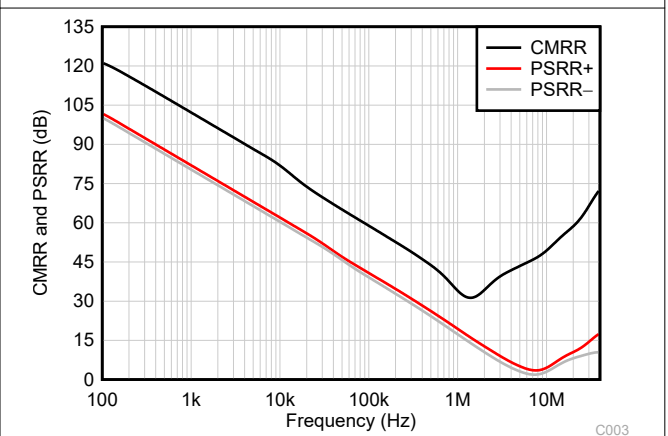


Figure 6-16. CMRR and PSRR vs Frequency

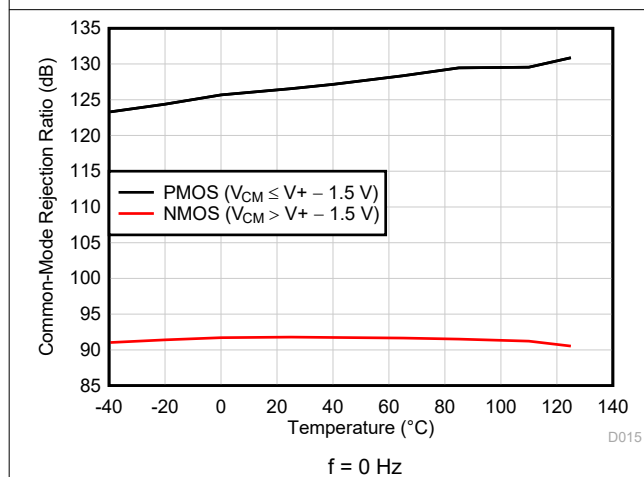


Figure 6-17. CMRR vs Temperature (dB)

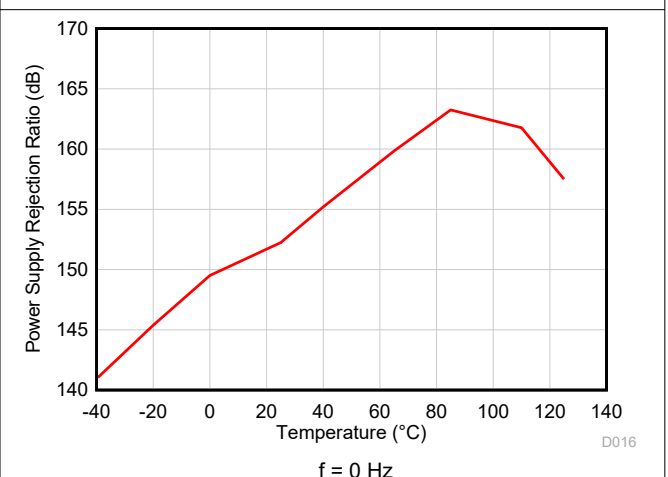
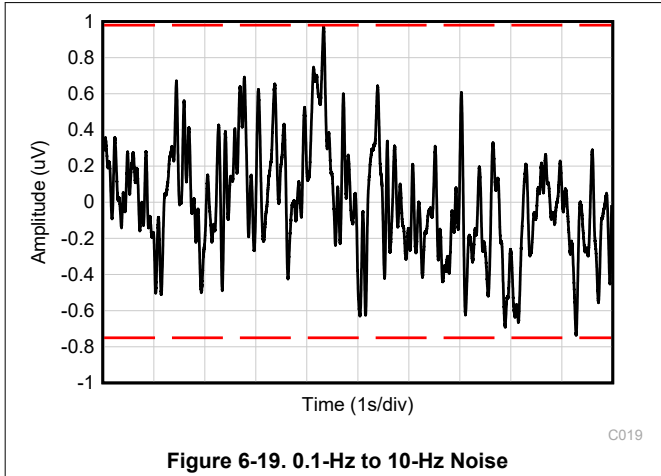


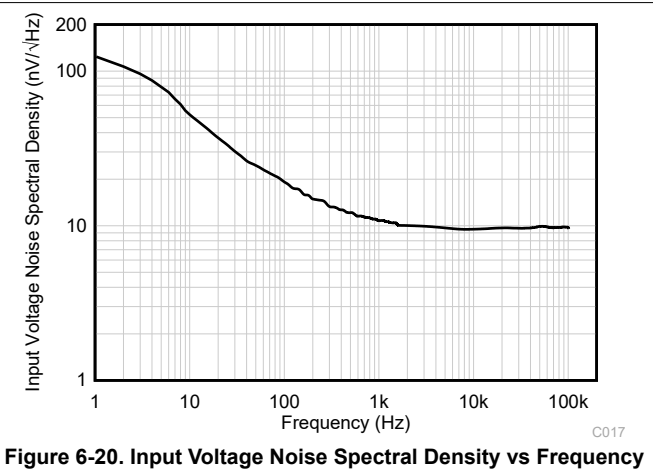
Figure 6-18. PSRR vs Temperature (dB)

### 6.8 Typical Characteristics (continued)

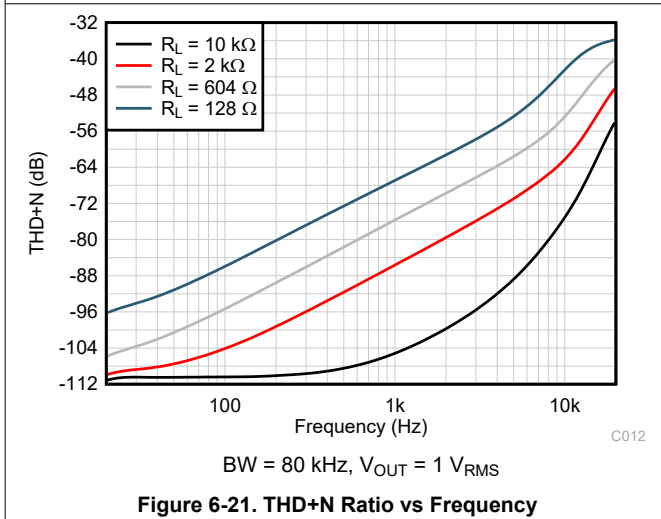
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)



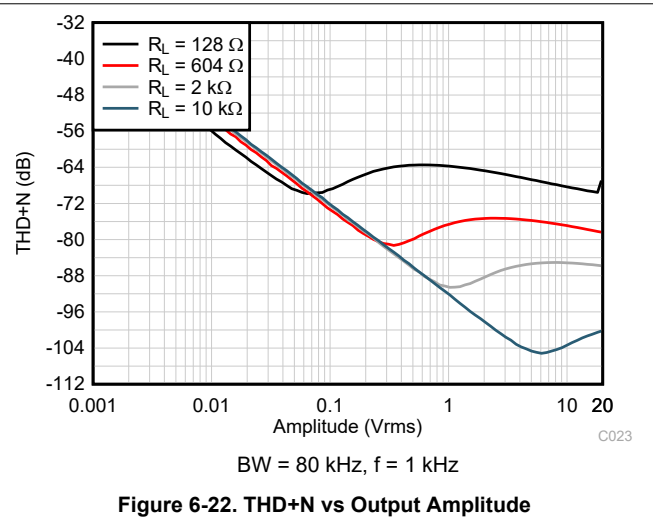
**Figure 6-19. 0.1-Hz to 10-Hz Noise**



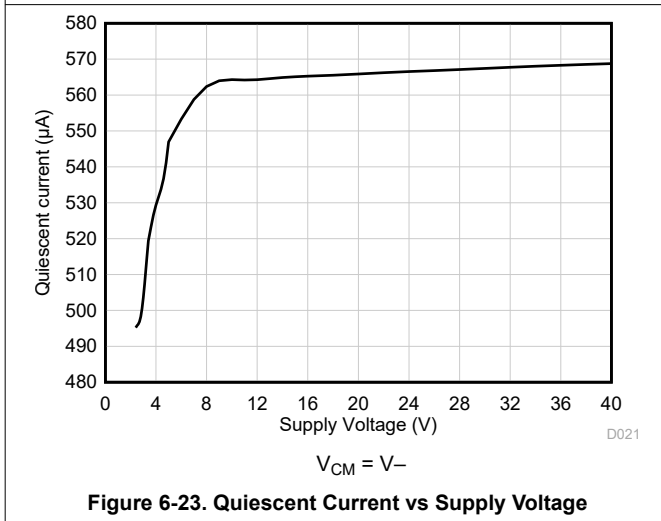
**Figure 6-20. Input Voltage Noise Spectral Density vs Frequency**



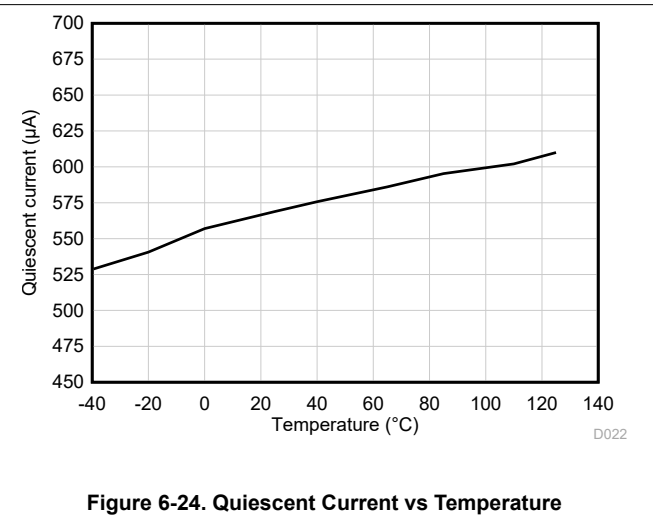
**Figure 6-21. THD+N Ratio vs Frequency**



**Figure 6-22. THD+N vs Output Amplitude**



**Figure 6-23. Quiescent Current vs Supply Voltage**



**Figure 6-24. Quiescent Current vs Temperature**

### 6.8 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)

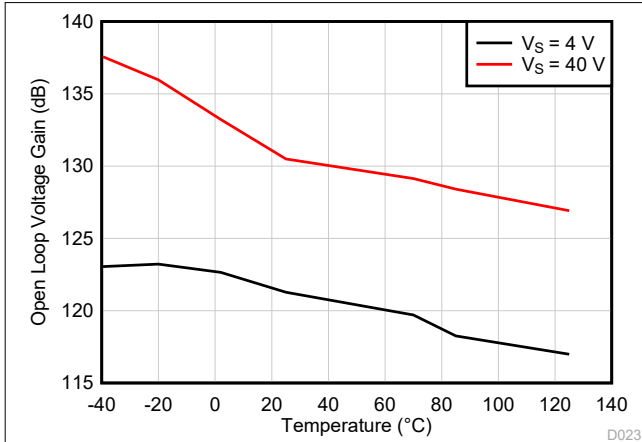


Figure 6-25. Open-Loop Voltage Gain vs Temperature (dB)

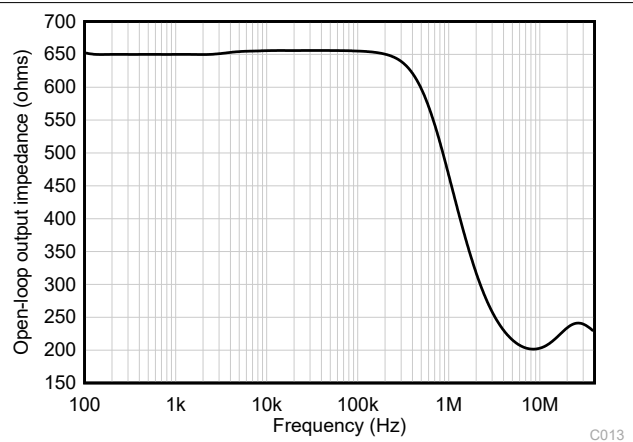
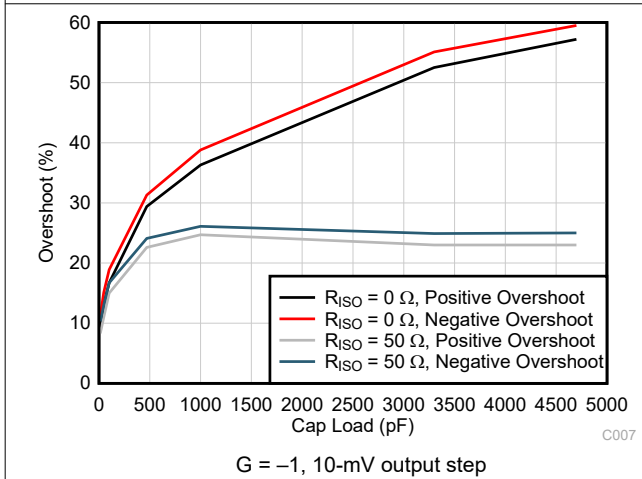
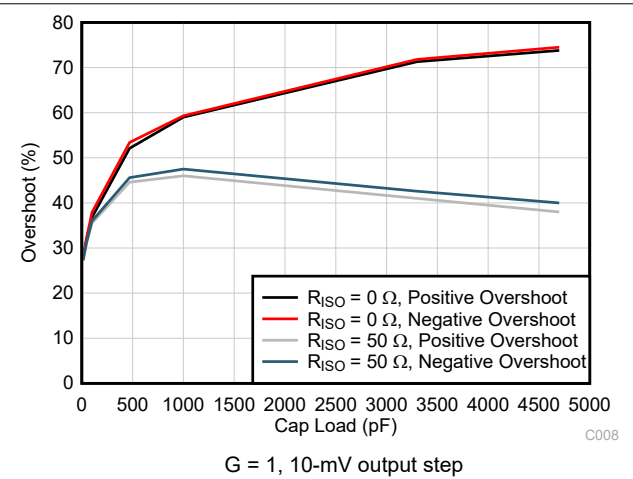


Figure 6-26. Open-Loop Output Impedance vs Frequency



G = -1, 10-mV output step

Figure 6-27. Small-Signal Overshoot vs Capacitive Load



G = 1, 10-mV output step

Figure 6-28. Small-Signal Overshoot vs Capacitive Load

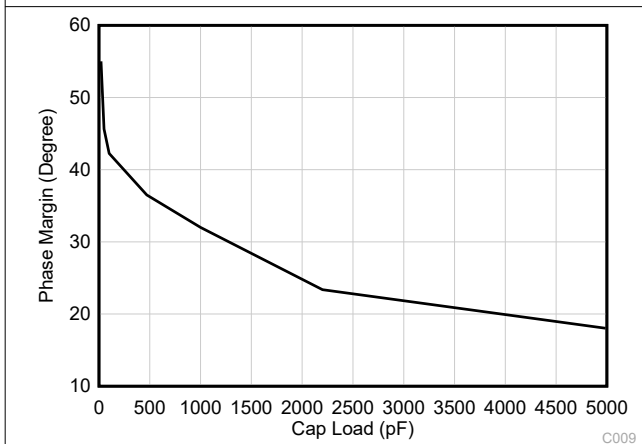
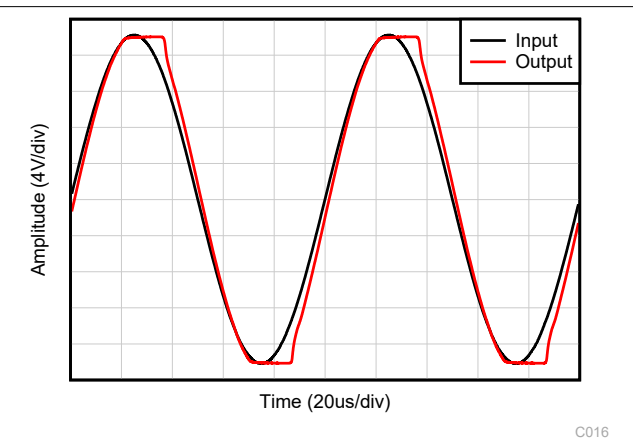


Figure 6-29. Phase Margin vs Capacitive Load



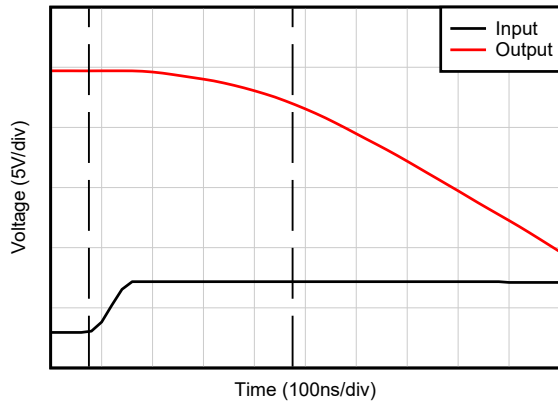
$V_{IN} = \pm 20\text{ V}$ ;  $V_S = V_{OUT} = \pm 17\text{ V}$

Figure 6-30. No Phase Reversal



### 6.8 Typical Characteristics (continued)

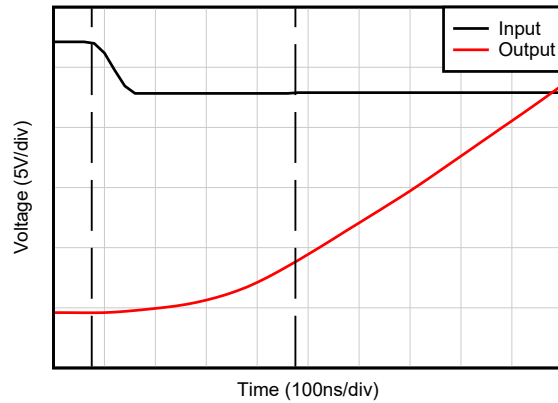
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)



$G = -10$

C018

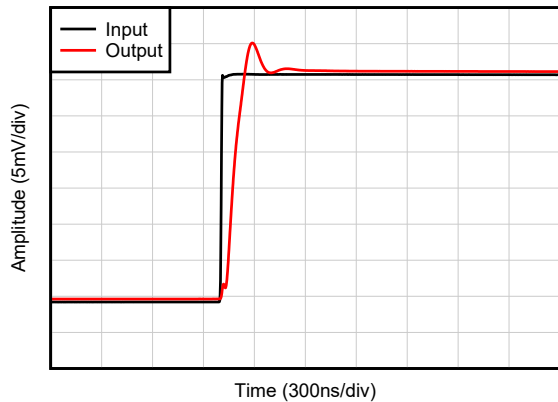
**Figure 6-31. Positive Overload Recovery**



$G = -10$

C018

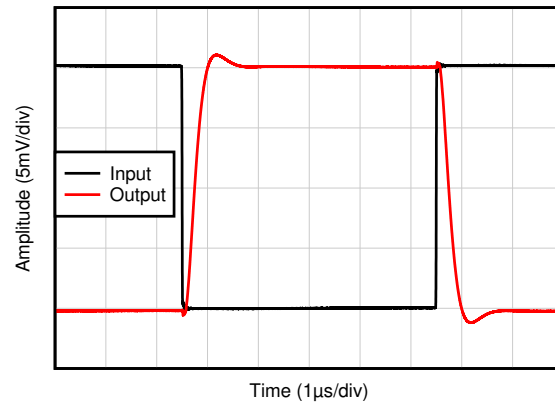
**Figure 6-32. Negative Overload Recovery**



$C_L = 20\text{ pF}$ ,  $G = 1$ , 20-mV step response

C010

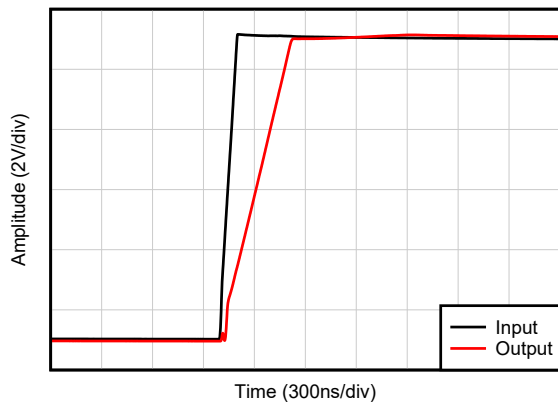
**Figure 6-33. Small-Signal Step Response, Rising**



$C_L = 20\text{ pF}$ ,  $G = 1$ , 20-mV step response

C011

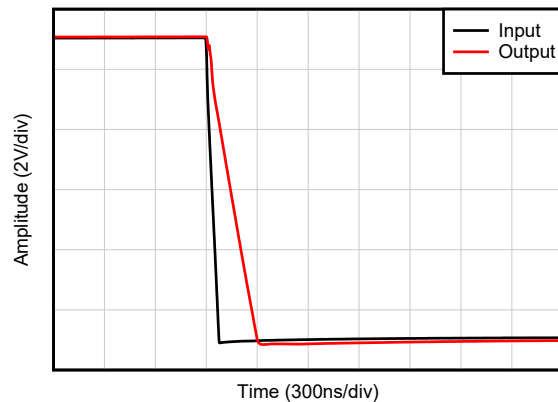
**Figure 6-34. Small-Signal Step Response, Falling**



$C_L = 20\text{ pF}$ ,  $G = 1$

C005

**Figure 6-35. Large-Signal Step Response (Rising)**



$C_L = 20\text{ pF}$ ,  $G = 1$

C005

**Figure 6-36. Large-Signal Step Response (Falling)**

### 6.8 Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 20\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_{LOAD} = 10\text{ k}\Omega$  connected to  $V_S / 2$ , and  $C_L = 10\text{ pF}$  (unless otherwise noted)

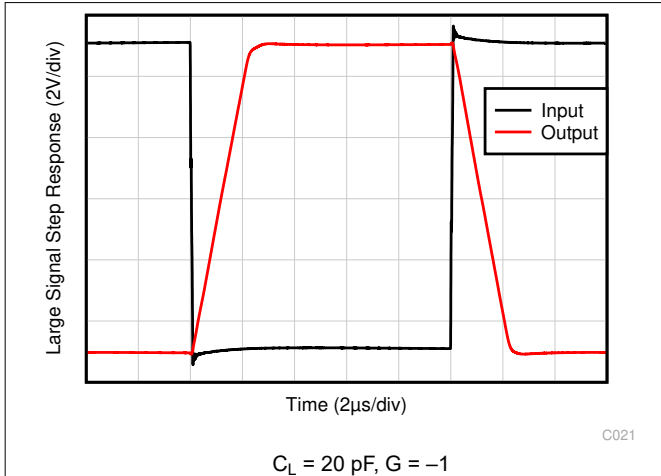


Figure 6-37. Large-Signal Step Response

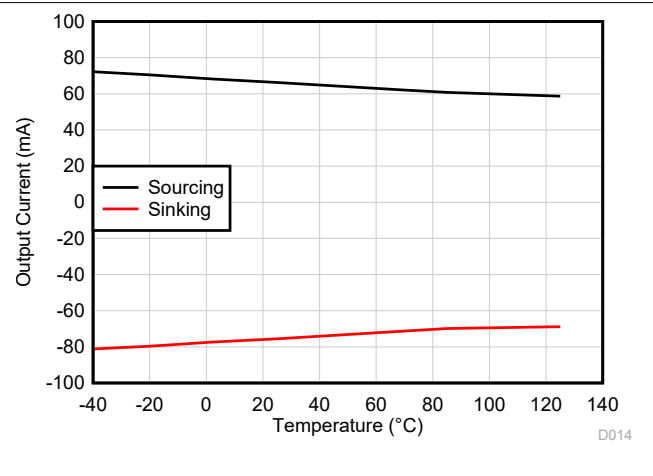


Figure 6-38. Short-Circuit Current vs Temperature

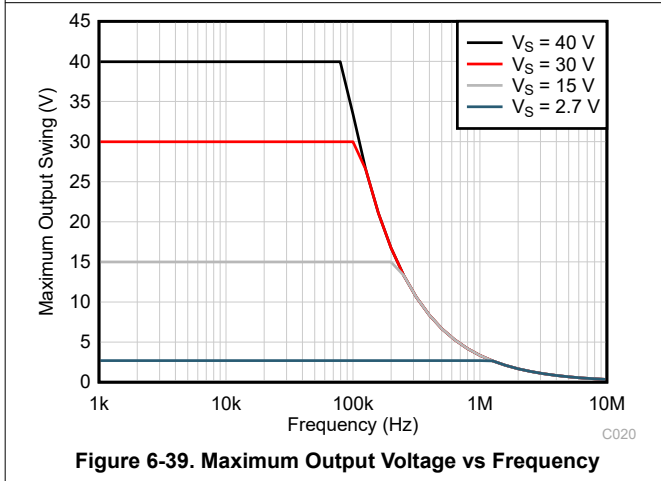


Figure 6-39. Maximum Output Voltage vs Frequency

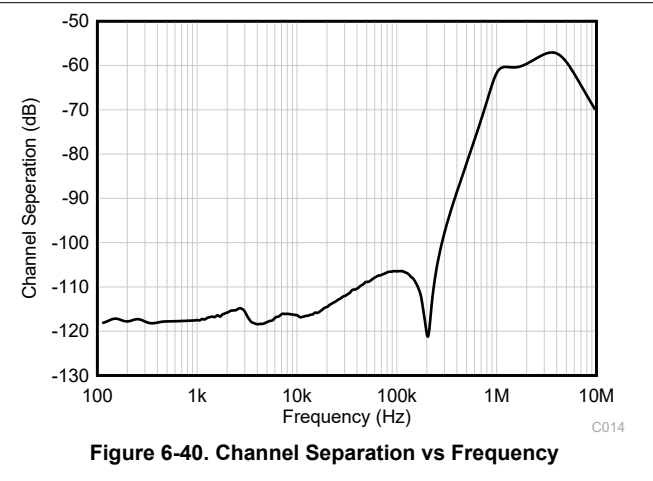


Figure 6-40. Channel Separation vs Frequency

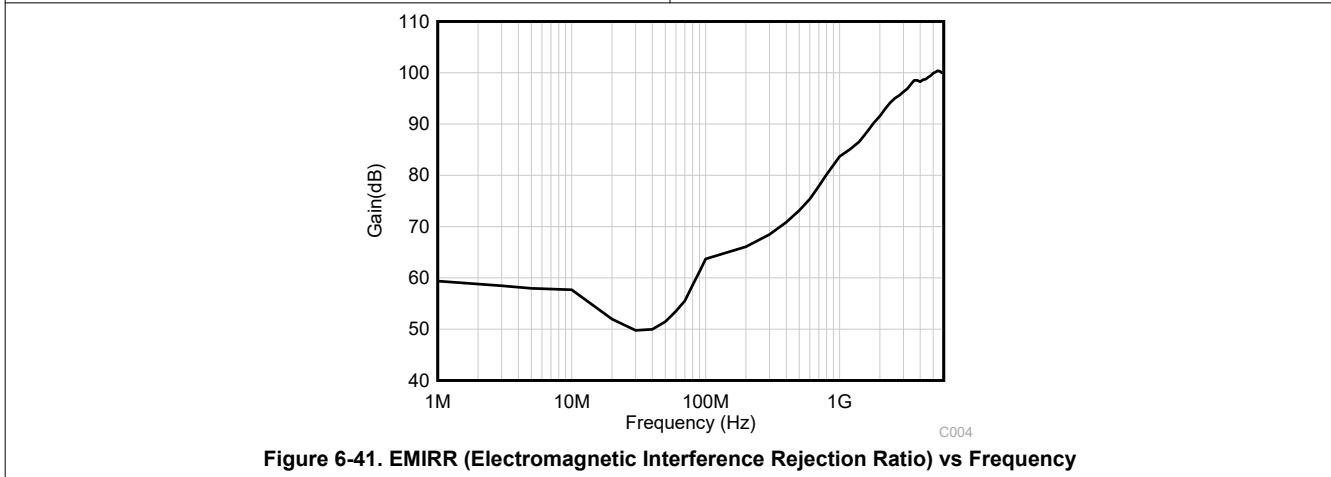


Figure 6-41. EMIRR (Electromagnetic Interference Rejection Ratio) vs Frequency

## 7 Detailed Description

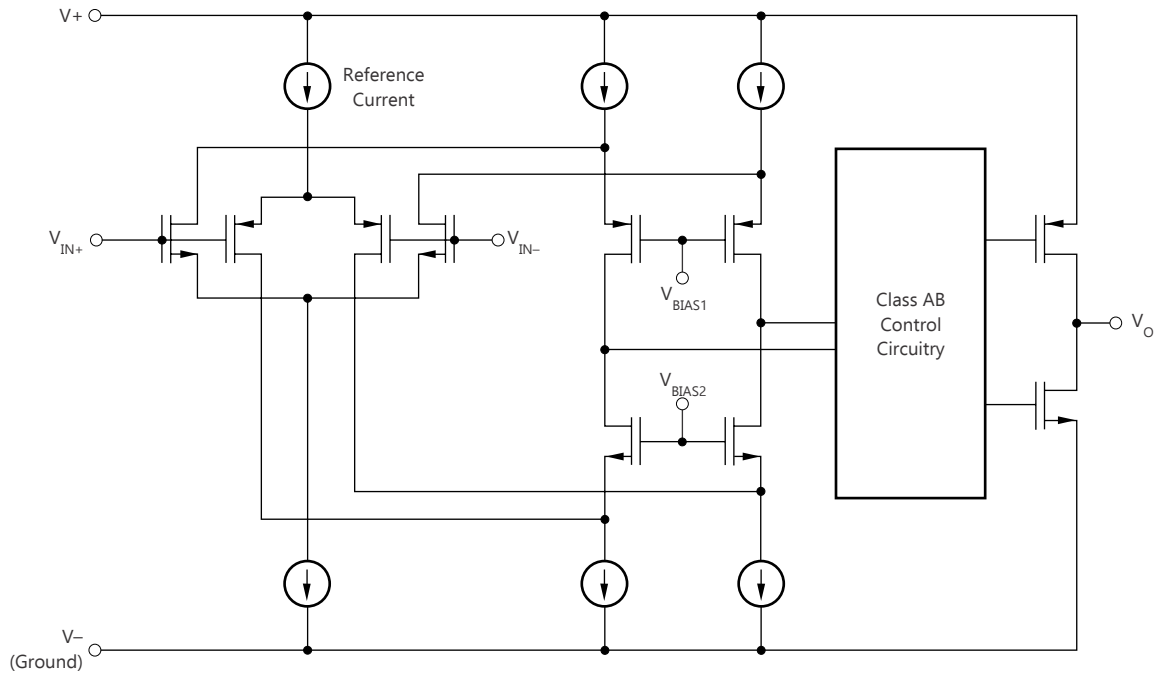
### 7.1 Overview

The TLV935x family (TLV9351, TLV9352, and TLV9354) is a family of 40-V, cost-optimized operational amplifiers. These devices offer strong general-purpose DC and AC specifications, including rail-to-rail output, low offset ( $\pm 350 \mu\text{V}$ , typ), low offset drift ( $\pm 1.5 \mu\text{V}/^\circ\text{C}$ , typ), and 3.5-MHz bandwidth.

Convenient features such as wide differential input-voltage range, high output current ( $\pm 60 \text{ mA}$ ), and high slew rate ( $20 \text{ V}/\mu\text{s}$ ) make the TLV935x a robust operational amplifier for high-voltage, cost-sensitive applications.

The TLV935x family of op amps is available in standard packages and is specified from  $-40^\circ\text{C}$  to  $125^\circ\text{C}$ .

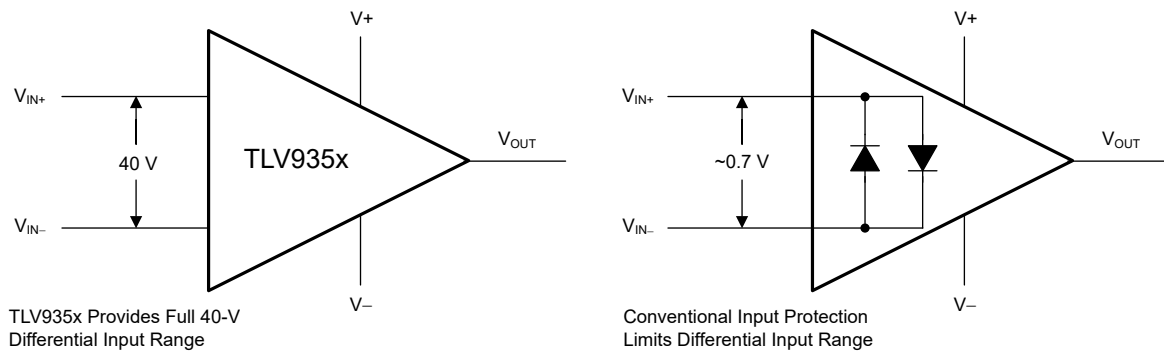
### 7.2 Functional Block Diagram



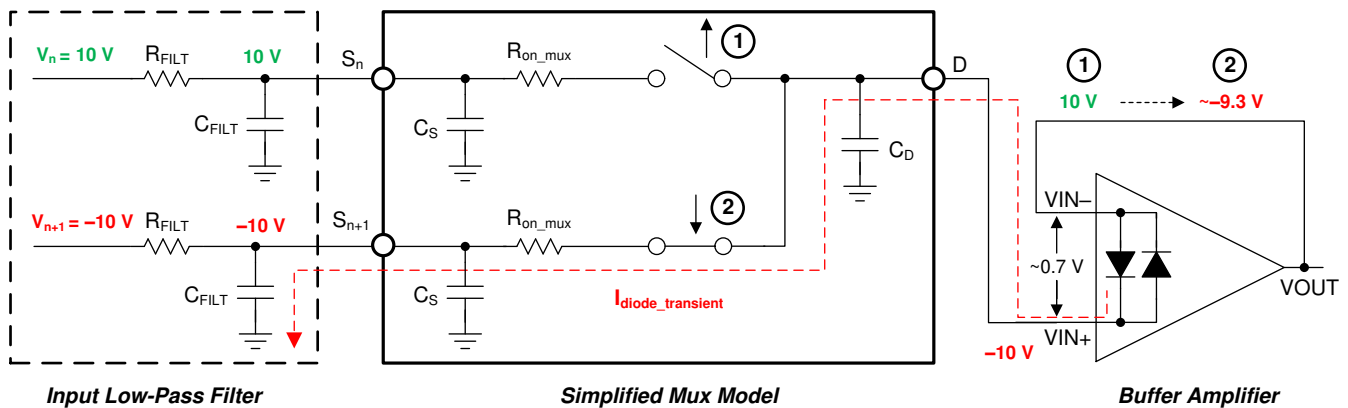
## 7.3 Feature Description

### 7.3.1 Input Protection Circuitry

The TLV935x uses a patented input architecture to eliminate the requirement for input protection diodes but still provides robust input protection under transient conditions. Figure 7-1 shows conventional input diode protection schemes that are activated by fast transient step responses and introduce signal distortion and settling time delays because of alternate current paths, as shown in Figure 7-2. For low-gain circuits, these fast-ramping input signals forward-bias back-to-back diodes, causing an increase in input current and resulting in extended settling time.



**Figure 7-1. TLV935x Input Protection Does Not Limit Differential Input Capability**

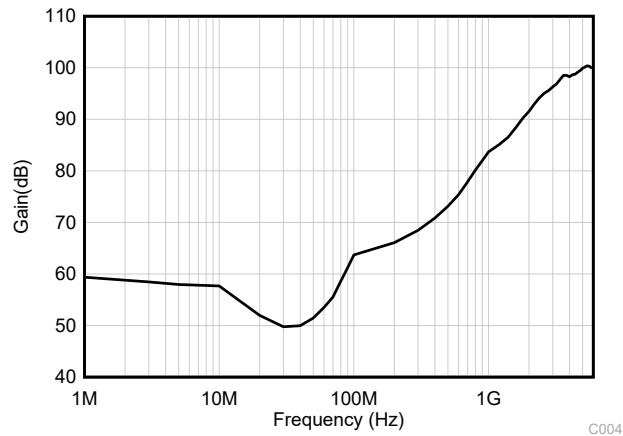


**Figure 7-2. Back-to-Back Diodes Create Settling Issues**

The TLV935x family of operational amplifiers provides a true high-impedance differential input capability for high-voltage applications. This patented input protection architecture does not introduce additional signal distortion or delayed settling time, making the device an optimal op amp for multichannel, high-switched, input applications. The TLV935x tolerates a maximum differential swing (voltage between inverting and noninverting pins of the op amp) of up to 40 V, making the device suitable for use as a comparator or in applications with fast-ramping input signals.

### 7.3.2 EMI Rejection

The TLV935x uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the TLV935x benefits from these design improvements. Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. Figure 7-3 shows the results of this testing on the TLV935x. Table 7-1 shows the EMIRR IN+ values for the TLV935x at particular frequencies commonly encountered in real-world applications. Table 7-1 lists applications that may be centered on or operated near the particular frequency shown. The *EMI Rejection Ratio of Operational Amplifiers* application report contains detailed information on the topic of EMIRR performance as it relates to op amps and is available for download from [www.ti.com](http://www.ti.com).



**Figure 7-3. EMIRR Testing**

**Table 7-1. TLV935x EMIRR IN+ for Frequencies of Interest**

FREQUENCY	APPLICATION OR ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	71 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	80 dB
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	87 dB
2.4 GHz	802.11b, 802.11g, 802.11n, Bluetooth®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	90 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	92 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	94 dB

### 7.3.3 Phase Reversal Protection

The TLV935x family has internal phase-reversal protection. Many op amps exhibit a phase reversal when the input is driven beyond its linear common-mode range. This condition is most often encountered in noninverting circuits when the input is driven beyond the specified common-mode voltage range, causing the output to reverse into the opposite rail. The TLV935x is a rail-to-rail input op amp; therefore, the common-mode range can extend up to the rails. Input signals beyond the rails do not cause phase reversal; instead, the output limits into the appropriate rail.

### 7.3.4 Thermal Protection

The internal power dissipation of any amplifier causes its internal (junction) temperature to rise. This phenomenon is called *self heating*. The absolute maximum junction temperature of the TLV935x is 150°C. Exceeding this temperature causes damage to the device. The TLV935x has a thermal protection feature that prevents damage from self heating. The protection works by monitoring the temperature of the device and turning off the op amp output drive for temperatures above 140°C. Figure 7-4 shows an application example for the TLV9351 that has significant self heating (159°C) because of its power dissipation (0.81 W). Thermal calculations indicate that for an ambient temperature of 65°C the device junction temperature must reach 187°C. The actual device, however, turns off the output drive to maintain a safe junction temperature. Figure 7-4 shows how the circuit behaves during thermal protection. During normal operation, the device acts as a buffer so the output is 3 V. When self heating causes the device junction temperature to increase above 140°C, the thermal protection forces the output to a high-impedance state and the output is pulled to ground through resistor  $R_L$ .

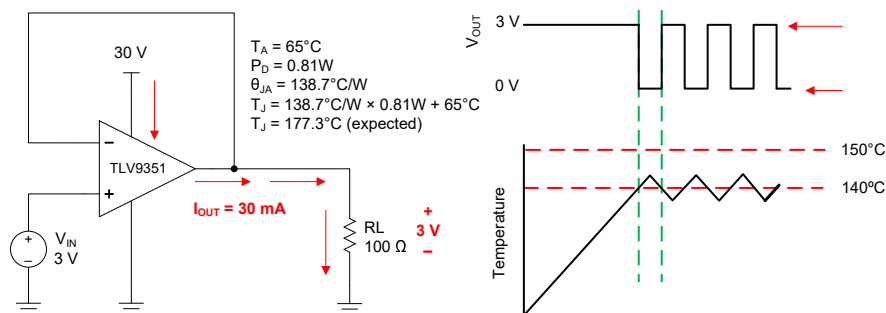
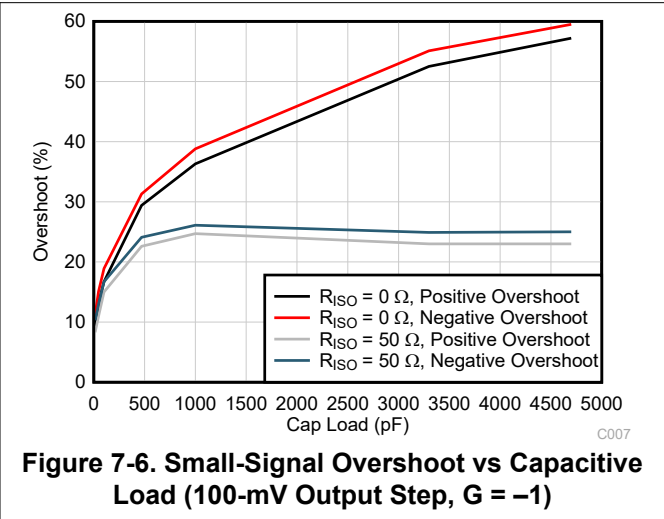
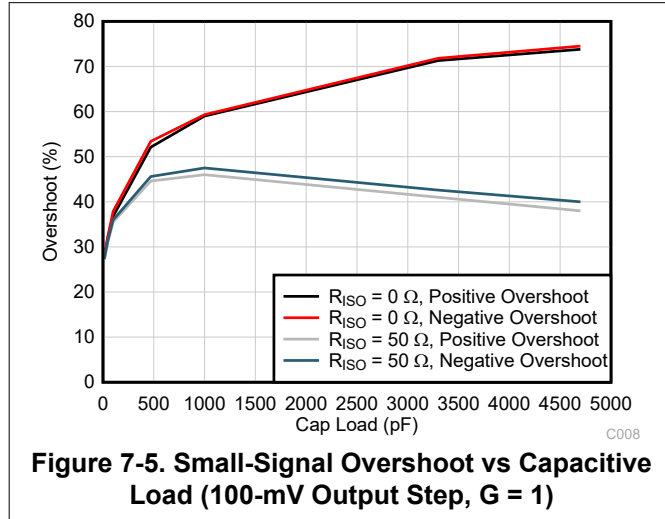


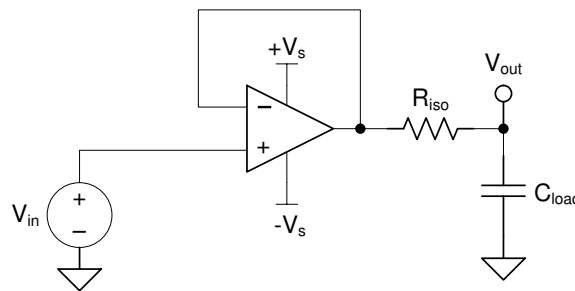
Figure 7-4. Thermal Protection

### 7.3.5 Capacitive Load and Stability

The TLV935x features a resistive output stage capable of driving smaller capacitive loads, and by leveraging an isolation resistor, the device can easily be configured to drive large capacitive loads. Increasing the gain enhances the ability of the amplifier to drive greater capacitive loads; see [Figure 7-5](#) and [Figure 7-6](#). The particular op amp circuit configuration, layout, gain, and output loading are some of the factors to consider when establishing whether an amplifier is stable in operation.



For additional drive capability in unity-gain configurations, improve capacitive load drive by inserting a small (10  $\Omega$  to 20  $\Omega$ ) resistor,  $R_{ISO}$ , in series with the output, as shown in [Figure 7-7](#). This resistor significantly reduces ringing and maintains DC performance for purely capacitive loads. However, if a resistive load is in parallel with the capacitive load, then a voltage divider is created, thus introducing a gain error at the output and slightly reducing the output swing. The error introduced is proportional to the ratio  $R_{ISO} / R_L$ , and is generally negligible at low output levels. A high capacitive load drive makes the TLV935x well suited for applications such as reference buffers, MOSFET gate drives, and cable-shield drives. The circuit shown in [Figure 7-7](#) uses an isolation resistor,  $R_{ISO}$ , to stabilize the output of an op amp.  $R_{ISO}$  modifies the open-loop gain of the system for increased phase margin. For additional information on techniques to optimize and design using this circuit, TI Precision Design [TIDU032](#) details complete design goals, simulation, and test results.



**Figure 7-7. Extending Capacitive Load Drive With the TLV9351**

### 7.3.6 Common-Mode Voltage Range

The TLV935x is a 40-V, rail-to-rail output operational amplifier with an input common-mode range that extends 100 mV beyond  $V_{-}$  and within 2 V of  $V_{+}$  for normal operation. The device accomplishes this performance through a complementary input stage, using a P-channel differential pair. Additionally, a complementary N-channel differential pair has been included in parallel with the P-channel pair to eliminate common undesirable op amp behaviors, such as phase reversal.

The TLV935x can operate with common mode ranges beyond 100 mV of the top rail, but with reduced performance above  $(V_{+}) - 2$  V. The N-channel pair is active for input voltages close to the positive rail, typically  $(V_{+}) - 1$  V to 100 mV above the positive supply. The P-channel pair is active for inputs from 100 mV below the negative supply to approximately  $(V_{+}) - 2$  V. There is a small transition region, typically  $(V_{+}) - 2$  V to  $(V_{+}) - 1$  V in which both input pairs are on. This transition region can vary modestly with process variation, and within the transition region and N-channel region, many specifications of the op amp, including PSRR, CMRR, offset voltage, offset drift, noise and THD performance may be degraded compared to operation within the P-channel region.

**Table 7-2. Typical Performance for Common-Mode Voltages Within 2 V of the Positive Supply**

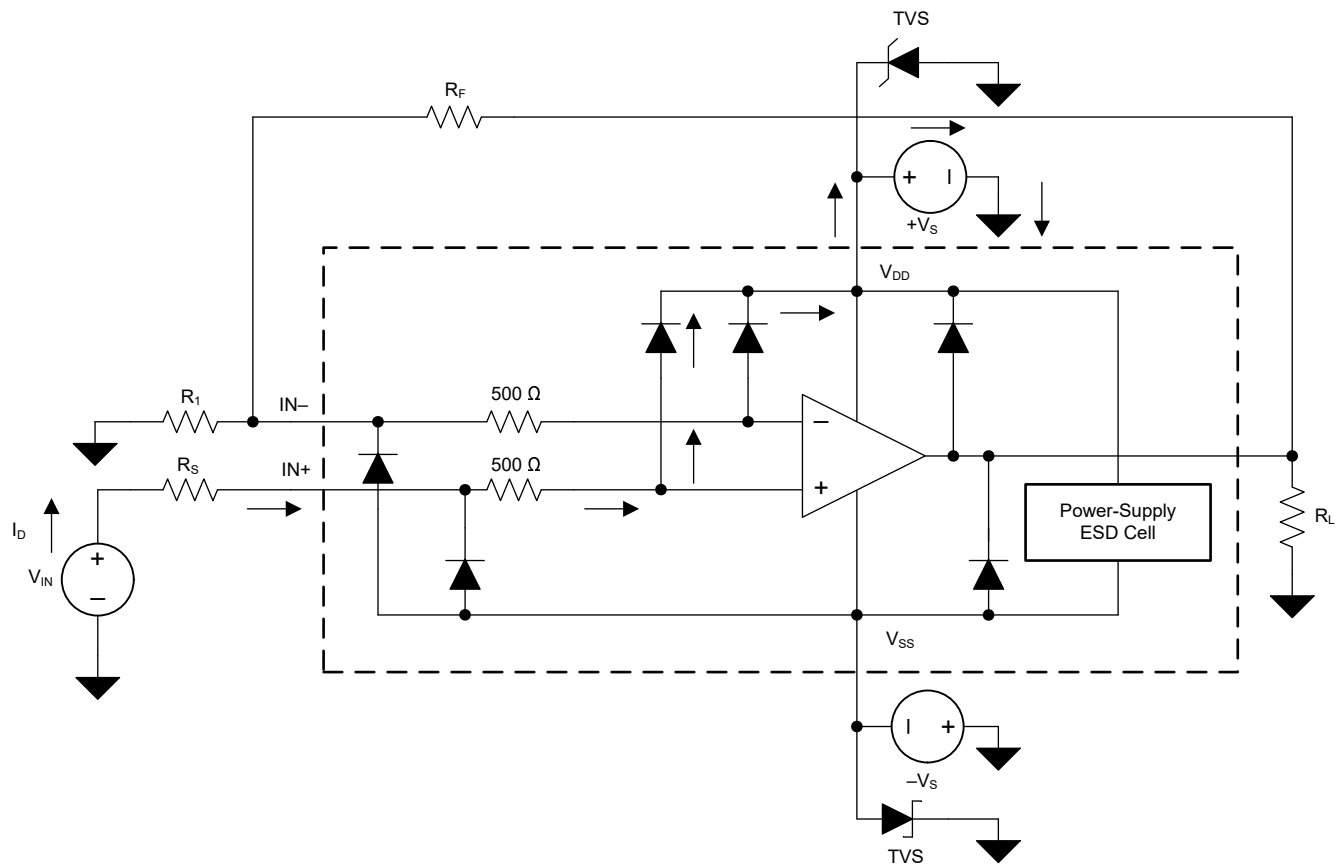
PARAMETER	MIN	TYP	MAX	UNIT
Input common-mode voltage	$(V_{+}) - 2$		$(V_{+}) + 0.1$	V
Offset voltage		1.5		mV
Offset voltage drift		2		$\mu\text{V}/^{\circ}\text{C}$
Common-mode rejection		75		dB
Open-loop gain		75		dB
Gain-bandwidth product		1.5		MHz



### 7.3.7 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress (EOS). These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

Having a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event is helpful. Figure 7-8 shows an illustration of the ESD circuits contained in the TLV935x (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where the diodes meet at an absorption device or the power-supply ESD cell, internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.



**Figure 7-8. Equivalent Internal ESD Circuitry Relative to a Typical Circuit Application**

An ESD event is very short in duration and very high voltage (for example, 1 kV, 100 ns), whereas an EOS event is long duration and lower voltage (for example, 50 V, 100 ms). The ESD diodes are designed for out-of-circuit ESD protection (that is, during assembly, test, and storage of the device before being soldered to the PCB). During an ESD event, the ESD signal is passed through the ESD steering diodes to an absorption circuit (labeled ESD power-supply circuit). The ESD absorption circuit clamps the supplies to a safe level.

Although this behavior is necessary for out-of-circuit protection, excessive current and damage is caused if activated in-circuit. A transient voltage suppressors (TVS) can be used to prevent against damage caused by turning on the ESD absorption circuit during an in-circuit ESD event. Using the appropriate current limiting resistors and TVS diodes allows for the use of device ESD diodes to protect against EOS events.

### 7.3.8 Overload Recovery

Overload recovery is defined as the time required for the op amp output to recover from a saturated state to a linear state. The output devices of the op amp enter a saturation region when the output voltage exceeds the rated operating voltage, either due to the high input voltage or the high gain. After the device enters the saturation region, the charge carriers in the output devices require time to return back to the linear state. After the charge carriers return back to the linear state, the device begins to slew at the specified slew rate. Thus, the propagation delay in case of an overload condition is the sum of the overload recovery time and the slew time. The overload recovery time for the TLV935x is approximately 1  $\mu$ s.

### 7.3.9 Typical Specifications and Distributions

Designers often have questions about a typical specification of an amplifier in order to design a more robust circuit. Due to natural variation in process technology and manufacturing procedures, every specification of an amplifier will exhibit some amount of deviation from the ideal value, like an amplifier's input offset voltage. These deviations often follow *Gaussian* ("bell curve"), or *normal* distributions, and circuit designers can leverage this information to guardband their system, even when there is not a minimum or maximum specification in the [Electrical Characteristics](#) table.

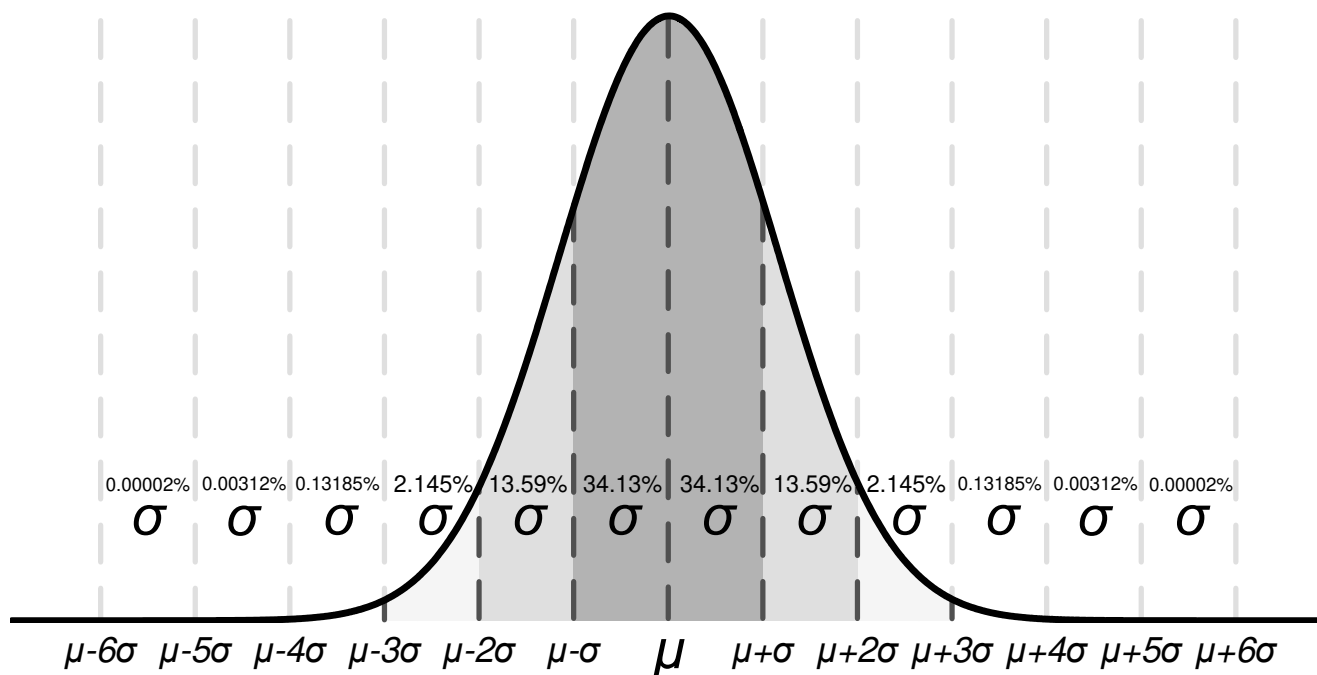


Figure 7-9. Ideal Gaussian Distribution

Figure 7-9 shows an example distribution, where  $\mu$ , or *mu*, is the mean of the distribution, and where  $\sigma$ , or *sigma*, is the standard deviation of a system. For a specification that exhibits this kind of distribution, approximately two-thirds (68.26%) of all units can be expected to have a value within one standard deviation, or one sigma, of the mean (from  $\mu - \sigma$  to  $\mu + \sigma$ ).

Depending on the specification, values listed in the *typical* column of the [Electrical Characteristics](#) table are represented in different ways. As a general rule of thumb, if a specification naturally has a nonzero mean (for example, like gain bandwidth), then the typical value is equal to the mean ( $\mu$ ). However, if a specification naturally has a mean near zero (like input offset voltage), then the typical value is equal to the mean plus one standard deviation ( $\mu + \sigma$ ) in order to most accurately represent the typical value.

You can use this chart to calculate approximate probability of a specification in a unit; for example, for TLV935x, the typical input voltage offset is 350  $\mu$ V, so 68.2% of all TLV935x devices are expected to have an offset from

–350  $\mu\text{V}$  to 350  $\mu\text{V}$ . At 4  $\sigma$  ( $\pm 1400$   $\mu\text{V}$ ), 99.9937% of the distribution has an offset voltage less than  $\pm 1400$   $\mu\text{V}$ , which means 0.0063% of the population is outside of these limits, which corresponds to about 1 in 15,873 units.

Specifications with a value in the minimum or maximum column are assured by TI, and units outside these limits will be removed from production material. For example, the TLV935x family has a maximum offset voltage of 1.8 mV at 125°C, and even though this corresponds to about 5  $\sigma$  ( $\approx 1$  in 1.7 million units), which is extremely unlikely, TI assures that any unit with larger offset than 1.8 mV will be removed from production material.

For specifications with no value in the minimum or maximum column, consider selecting a sigma value of sufficient guardband for your application, and design worst-case conditions using this value. For example, the 6- $\sigma$  value corresponds to about 1 in 500 million units, which is an extremely unlikely chance, and could be an option as a wide guardband to design a system around. In this case, the TLV935x family does not have a maximum or minimum for offset voltage drift, but based on the typical value of 1.5  $\mu\text{V}/^\circ\text{C}$  in the [Electrical Characteristics](#) table, it can be calculated that the 6- $\sigma$  value for offset voltage drift is about 9  $\mu\text{V}/^\circ\text{C}$ . When designing for worst-case system conditions, this value can be used to estimate the worst possible offset across temperature without having an actual minimum or maximum value.

However, process variation and adjustments over time can shift typical means and standard deviations, and unless there is a value in the minimum or maximum specification column, TI cannot assure the performance of a device. This information should be used only to estimate the performance of a device.

## 7.4 Device Functional Modes

The TLV935x has a single functional mode and is operational when the power-supply voltage is greater than 4.5 V ( $\pm 2.25$  V). The maximum power supply voltage for the TLV935x is 40 V ( $\pm 20$  V).

## 8 Application Information Disclaimer

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 8.1 Application Information

The TLV935x family offers excellent DC precision and DC performance. These devices operate up to 40-V supply rails and offer true rail-to-rail output, low offset voltage and offset voltage drift, as well as 3.5-MHz bandwidth and high output drive. These features make the TLV935x a robust, high-performance operational amplifier for high-voltage cost-sensitive applications.

### 8.2 Typical Applications

#### 8.2.1 High Voltage Precision Comparator

Many different systems require controlled voltages across numerous system nodes to ensure robust operation. A comparator can be used to monitor and control voltages by comparing a reference threshold voltage with an input voltage and providing an output when the input crosses this threshold.

The TLV935x family of op amps make excellent high voltage comparators due to their MUX-friendly input stage (see the [Input Protection Circuitry](#) section). Previous generation high-voltage op amps often use back-to-back diodes across the inputs to prevent damage to the op amp which greatly limits these op amps to be used as comparators, but the TLV935x's patented input stage allows the device to have a wide differential voltage between the inputs.

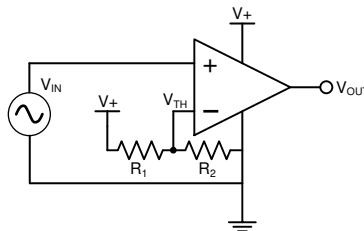


Figure 8-1. Typical Comparator Application

##### 8.2.1.1 Design Requirements

The primary objective is to design a 40-V precision comparator.

- System supply voltage ( $V_+$ ): 40 V
- Resistor 1 value: 100 k $\Omega$
- Resistor 2 value: 100 k $\Omega$
- Reference threshold voltage ( $V_{TH}$ ): 20 V
- Input voltage range ( $V_{IN}$ ): 0 V – 40 V
- Output voltage range ( $V_{OUT}$ ): 0 V – 40 V

### 8.2.1.2 Detailed Design Procedure

This noninverting comparator circuit applies the input voltage ( $V_{IN}$ ) to the noninverting terminal of the op amp. Two resistors ( $R_1$  and  $R_2$ ) divide the supply voltage ( $V_+$ ) to create a mid-supply threshold voltage ( $V_{TH}$ ) as calculated in Equation 1. The circuit is shown in Figure 8-1. When  $V_{IN}$  is less than  $V_{TH}$ , the output voltage transitions to the negative supply and equals the low-level output voltage. When  $V_{IN}$  is greater than  $V_{TH}$ , the output voltage transitions to the positive supply and equals the high-level output voltage.

In this example, resistor 1 and 2 have been selected to be 100 k $\Omega$ , which sets the reference threshold at 20 V. However, resistor 1 and 2 can be adjusted to modify the threshold using Equation 1. Resistor 1 and 2's values have also been selected to reduce power consumption, but these values can be further increased to reduce power consumption, or reduced to improve noise performance.

$$V_{TH} = \frac{R_2}{R_1 + R_2} \times V_+ \tag{1}$$

### 8.2.1.3 Application Curve

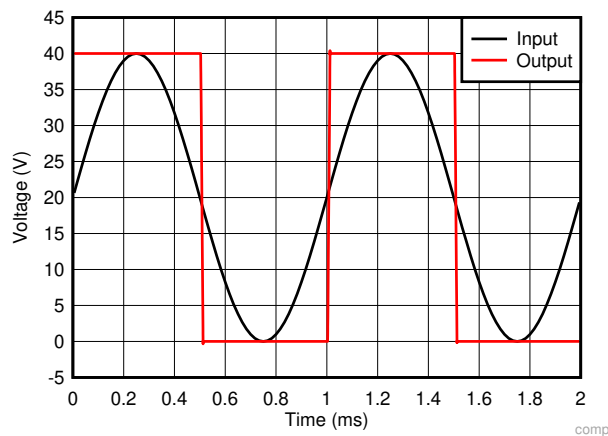


Figure 8-2. Comparator Output Response to Input Voltage

## 9 Power Supply Recommendations

The TLV935x is specified for operation from 4.5 V to 40 V ( $\pm 2.25$  V to  $\pm 20$  V); many specifications apply from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ .

### CAUTION

Supply voltages larger than 40 V can permanently damage the device; see the [Absolute Maximum Ratings](#) table.

Place 0.1- $\mu\text{F}$  bypass capacitors close to the power-supply pins to reduce errors coupling in from noisy or high-impedance power supplies. For more detailed information on bypass capacitor placement, refer to the [Layout](#) section.

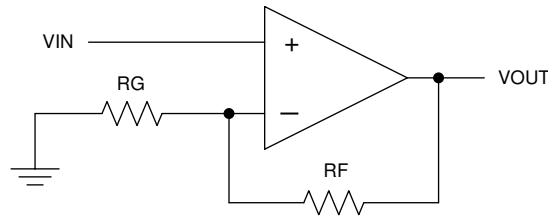
## 10 Layout

### 10.1 Layout Guidelines

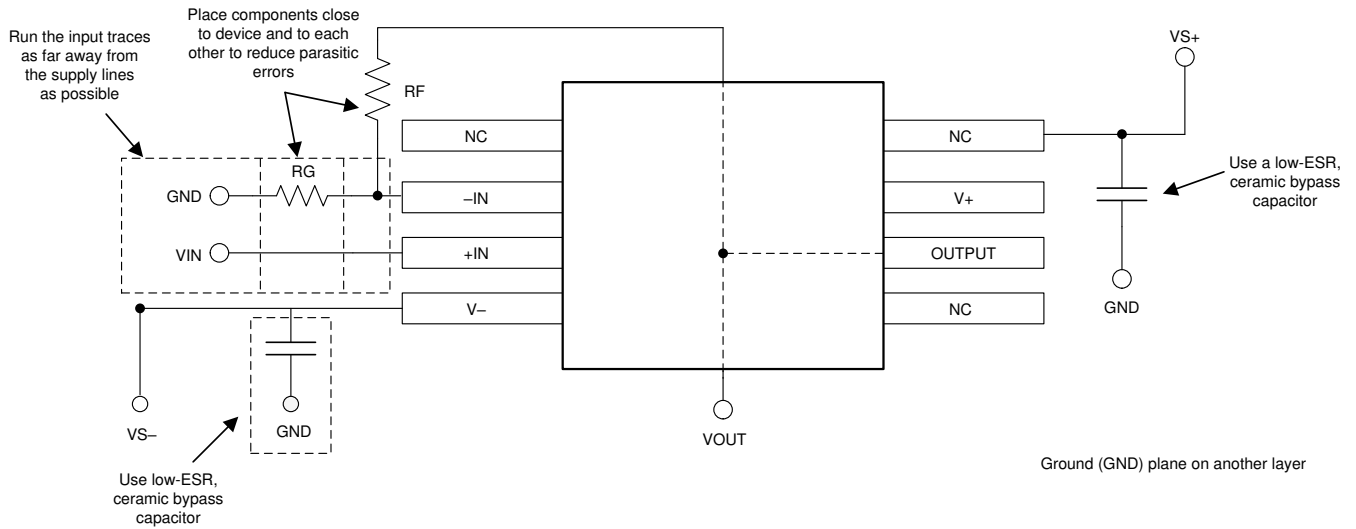
For best operational performance of the device, use good PCB layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and op amp itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1- $\mu\text{F}$  ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds paying attention to the flow of the ground current.
- In order to reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. As illustrated in [Figure 10-2](#), keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.
- Cleaning the PCB following board assembly is recommended for best performance.
- Any precision integrated circuit may experience performance shifts due to moisture ingress into the plastic package. Following any aqueous PCB cleaning process, baking the PCB assembly is recommended to remove moisture introduced into the device packaging during the cleaning process. A low temperature, post cleaning bake at  $85^{\circ}\text{C}$  for 30 minutes is sufficient for most circumstances.

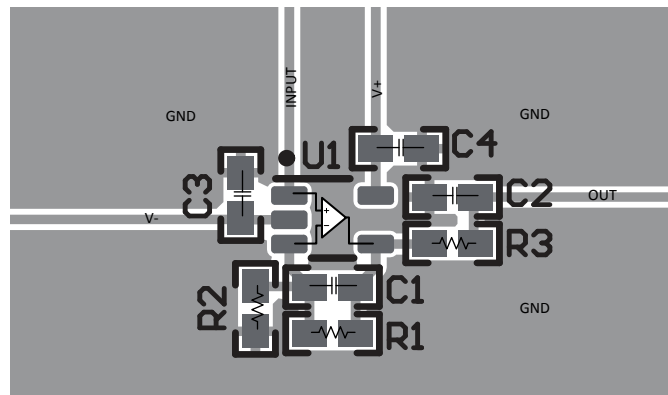
## 10.2 Layout Example



**Figure 10-1. Schematic Representation**



**Figure 10-2. Operational Amplifier Board Layout for Noninverting Configuration**



**Figure 10-3. Example Layout for SC70 (DCK) Package**

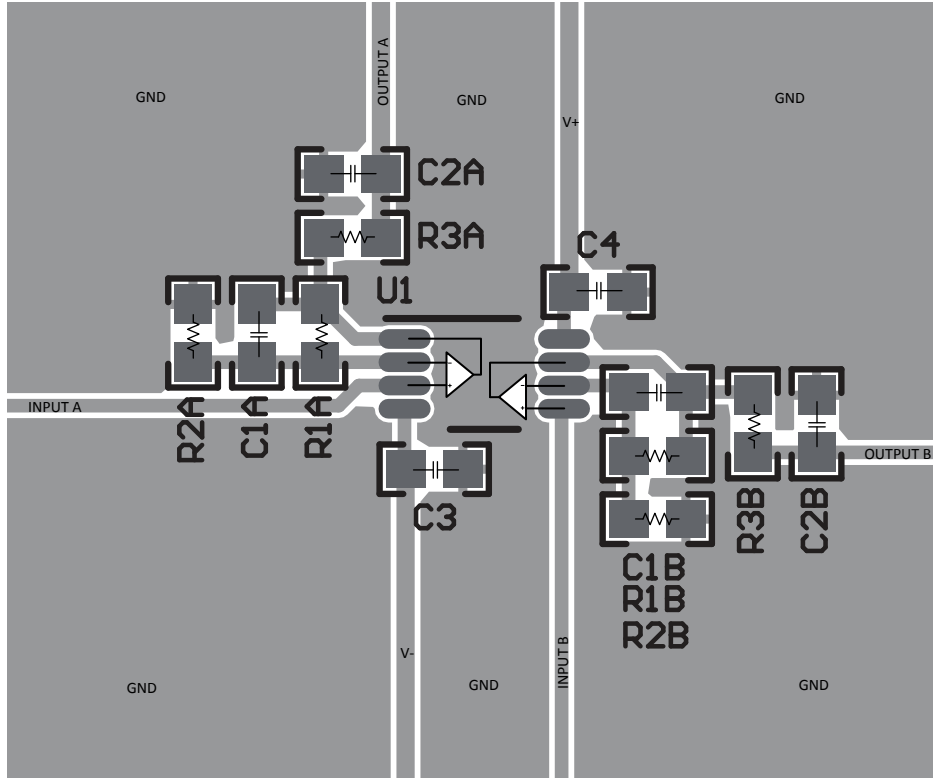


Figure 10-4. Example Layout for VSSOP-8 (DGK) Package



## 11 Device and Documentation Support

### 11.1 Device Support

#### 11.1.1 Development Support

##### 11.1.1.1 TINA-TI™ (Free Software Download)

TINA™ is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI is a free, fully-functional version of the TINA software, preloaded with a library of macro models in addition to a range of both passive and active models. TINA-TI provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a [free download](#) from the Analog eLab Design Center, TINA-TI offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

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#### Note

These files require that either the TINA software (from DesignSoft™) or TINA-TI software be installed. Download the free TINA-TI software from the [TINA-TI folder](#).

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##### 11.1.1.2 TI Precision Designs

The TLV935x is featured in several TI Precision Designs, available online at <http://www.ti.com/ww/en/analog/precision-designs/>. TI Precision Designs are analog solutions created by TI's precision analog applications experts and offer the theory of operation, component selection, simulation, complete PCB schematic and layout, bill of materials, and measured performance of many useful circuits.

### 11.2 Documentation Support

#### 11.2.1 Related Documentation

Texas Instruments, [Analog Engineer's Circuit Cookbook: Amplifiers](#)

Texas Instruments, [AN31 amplifier circuit collection](#) application report

Texas Instruments, [EMI Rejection Ratio of Operational Amplifiers](#) application report

Texas Instruments, [Capacitive Load Drive Solution using an Isolation Resistor](#) reference design

### 11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](http://ti.com). Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 11.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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### 11.5 Trademarks

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TI E2E™ is a trademark of Texas Instruments.

Bluetooth® is a registered trademark of Bluetooth SIG, Inc.

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## 11.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## 11.7 Glossary

### [TI Glossary](#)

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TLV93511DBVR	ACTIVE	SOT-23	DBV	5	3000	RoHS & Green	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 125	T93V	<a href="#">Samples</a>
TLV93511DCKR	ACTIVE	SC70	DCK	5	3000	RoHS & Green	SN	Level-2-260C-1 YEAR	-40 to 125	1HE	<a href="#">Samples</a>
TLV93521DDFR	ACTIVE	SOT-23-THIN	DDF	8	3000	RoHS & Green	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 125	T935	<a href="#">Samples</a>
TLV93521DGKR	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	SN	Level-1-260C-UNLIM	-40 to 125	2DXT	<a href="#">Samples</a>
TLV93521DR	ACTIVE	SOIC	D	8	2500	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T9352D	<a href="#">Samples</a>
TLV93521PWR	ACTIVE	TSSOP	PW	8	2000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	T9352P	<a href="#">Samples</a>
TLV93541DR	ACTIVE	SOIC	D	14	2500	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	TLV9354D	<a href="#">Samples</a>
TLV93541DYR	ACTIVE	SOT-23-THIN	DYY	14	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	TLV9354I	<a href="#">Samples</a>
TLV93541PWR	ACTIVE	TSSOP	PW	14	2000	RoHS & Green	NIPDAU   SN	Level-2-260C-1 YEAR	-40 to 125	(TL9354, TL9354PW)	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

**OTHER QUALIFIED VERSIONS OF TLV9351, TLV9352, TLV9354 :**

- Automotive : [TLV9351-Q1](#), [TLV9352-Q1](#), [TLV9354-Q1](#)

NOTE: Qualified Version Definitions:

- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects

**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV9351IDBVR	SOT-23	DBV	5	3000	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TLV9351IDCKR	SC70	DCK	5	3000	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3
TLV9352IDDFR	SOT-23-THIN	DDF	8	3000	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
TLV9352IDGKR	VSSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
TLV9352IDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TLV9352IPWR	TSSOP	PW	8	2000	330.0	12.4	7.0	3.6	1.6	8.0	12.0	Q1
TLV9354IDR	SOIC	D	14	2500	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1
TLV9354IDYYR	SOT-23-THIN	DYY	14	3000	330.0	12.4	4.8	3.6	1.6	8.0	12.0	Q3
TLV9354IPWR	TSSOP	PW	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV9351IDBVR	SOT-23	DBV	5	3000	210.0	185.0	35.0
TLV9351IDCKR	SC70	DCK	5	3000	190.0	190.0	30.0
TLV9352IDDFR	SOT-23-THIN	DDF	8	3000	210.0	185.0	35.0
TLV9352IDGKR	VSSOP	DGK	8	2500	366.0	364.0	50.0
TLV9352IDR	SOIC	D	8	2500	356.0	356.0	35.0
TLV9352IPWR	TSSOP	PW	8	2000	356.0	356.0	35.0
TLV9354IDR	SOIC	D	14	2500	356.0	356.0	35.0
TLV9354IDYYR	SOT-23-THIN	DYY	14	3000	336.6	336.6	31.8
TLV9354IPWR	TSSOP	PW	14	2000	356.0	356.0	35.0

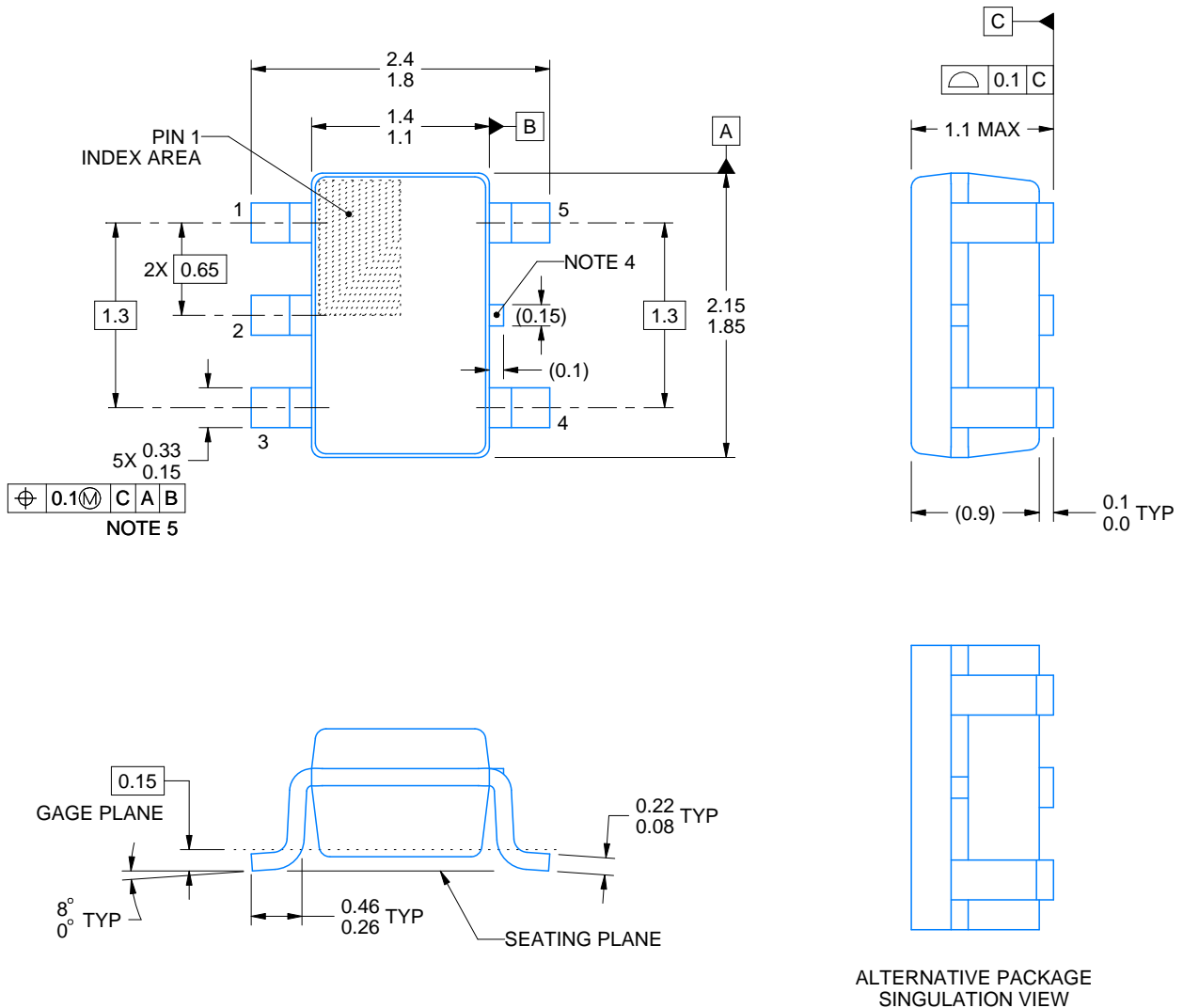
# DCK0005A



# PACKAGE OUTLINE

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



4214834/E 06/2024

## NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-203.
4. Support pin may differ or may not be present.
5. Lead width does not comply with JEDEC.
6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side

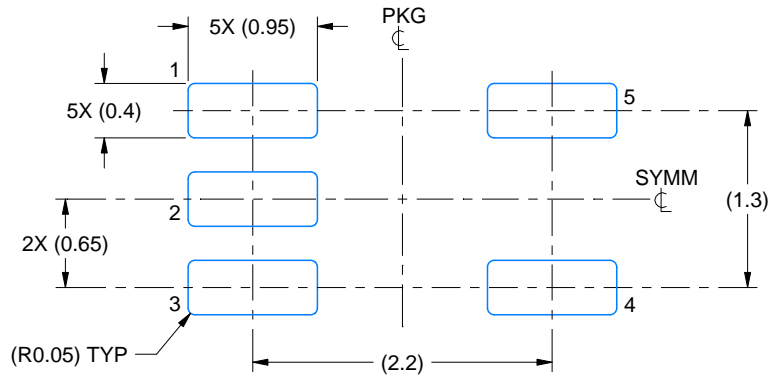


# EXAMPLE BOARD LAYOUT

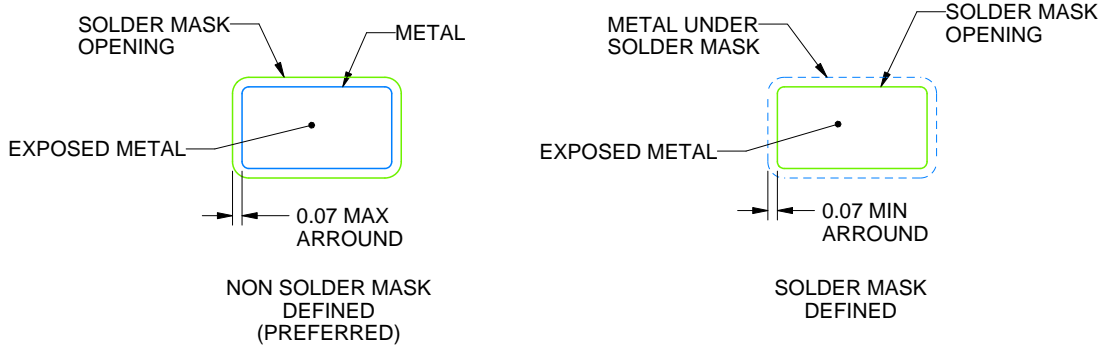
DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:18X



SOLDER MASK DETAILS

4214834/E 06/2024

NOTES: (continued)

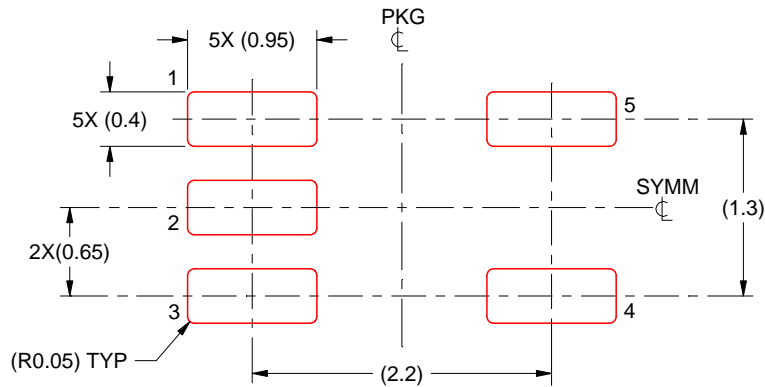
- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE: 18X

4214834/E 06/2024

NOTES: (continued)

9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
10. Board assembly site may have different recommendations for stencil design.

# DGK0008A



# PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



4214862/A 04/2023

**NOTES:**

PowerPAD is a trademark of Texas Instruments.

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-187.

# EXAMPLE BOARD LAYOUT

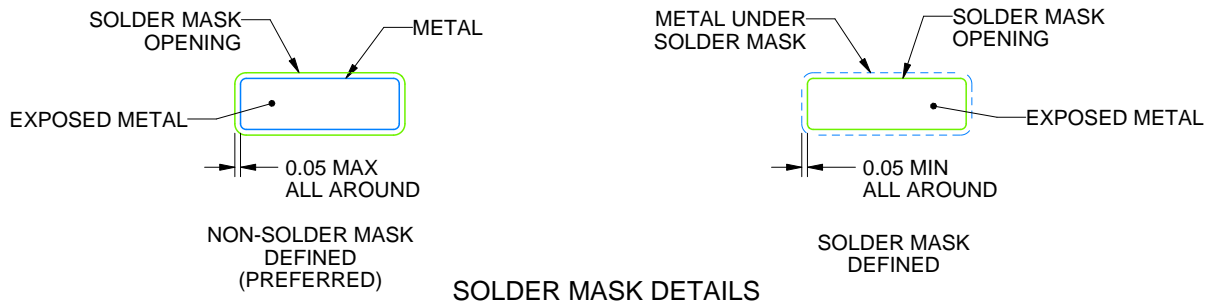
DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 15X



SOLDER MASK DETAILS

4214862/A 04/2023

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
9. Size of metal pad may vary due to creepage requirement.

# EXAMPLE STENCIL DESIGN

DGK0008A

™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE

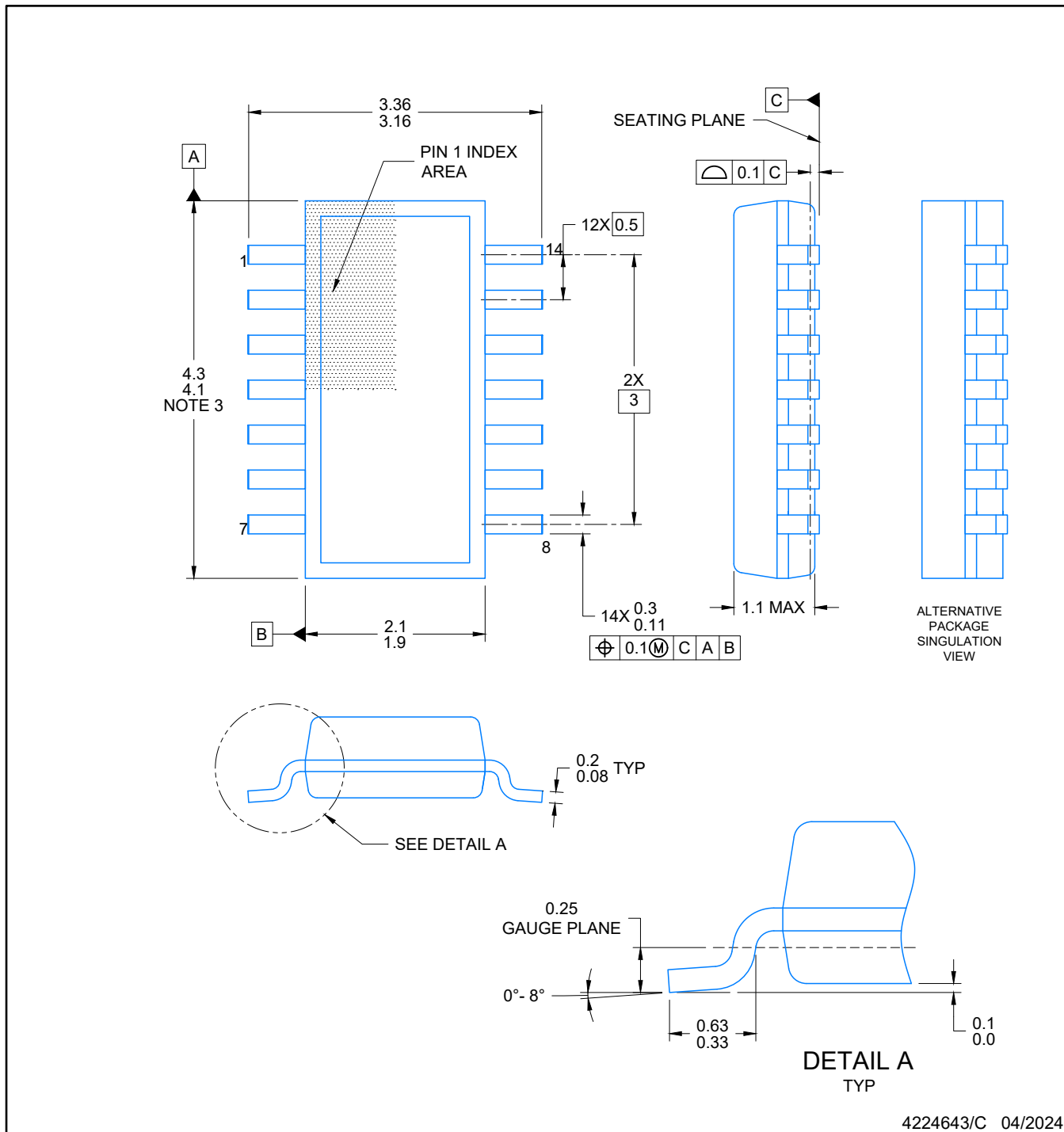


SOLDER PASTE EXAMPLE  
SCALE: 15X

4214862/A 04/2023

NOTES: (continued)

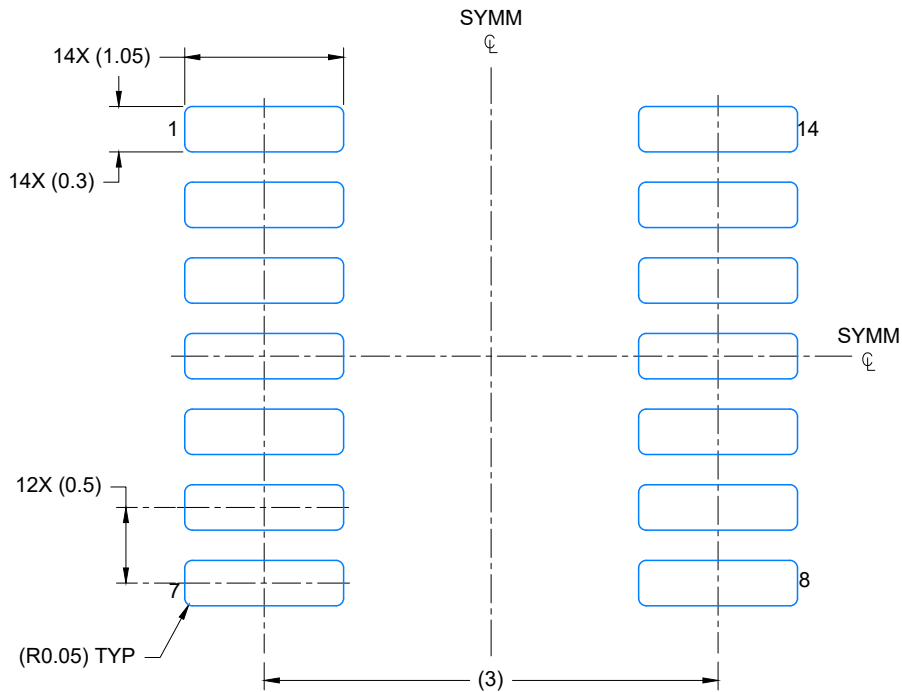
11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
12. Board assembly site may have different recommendations for stencil design.



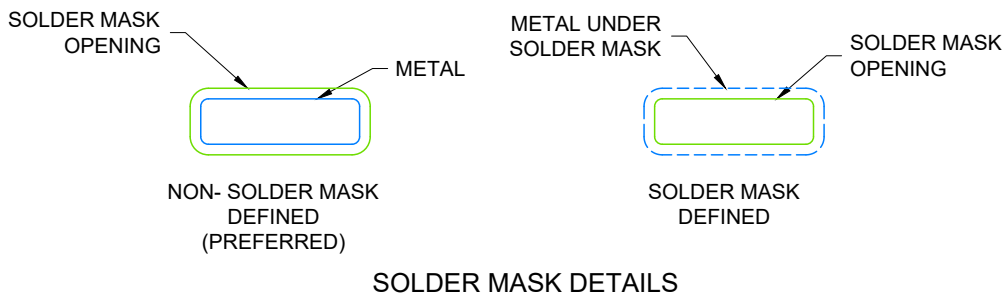
4224643/C 04/2024

NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
5. Reference JEDEC Registration MO-345, Variation AB



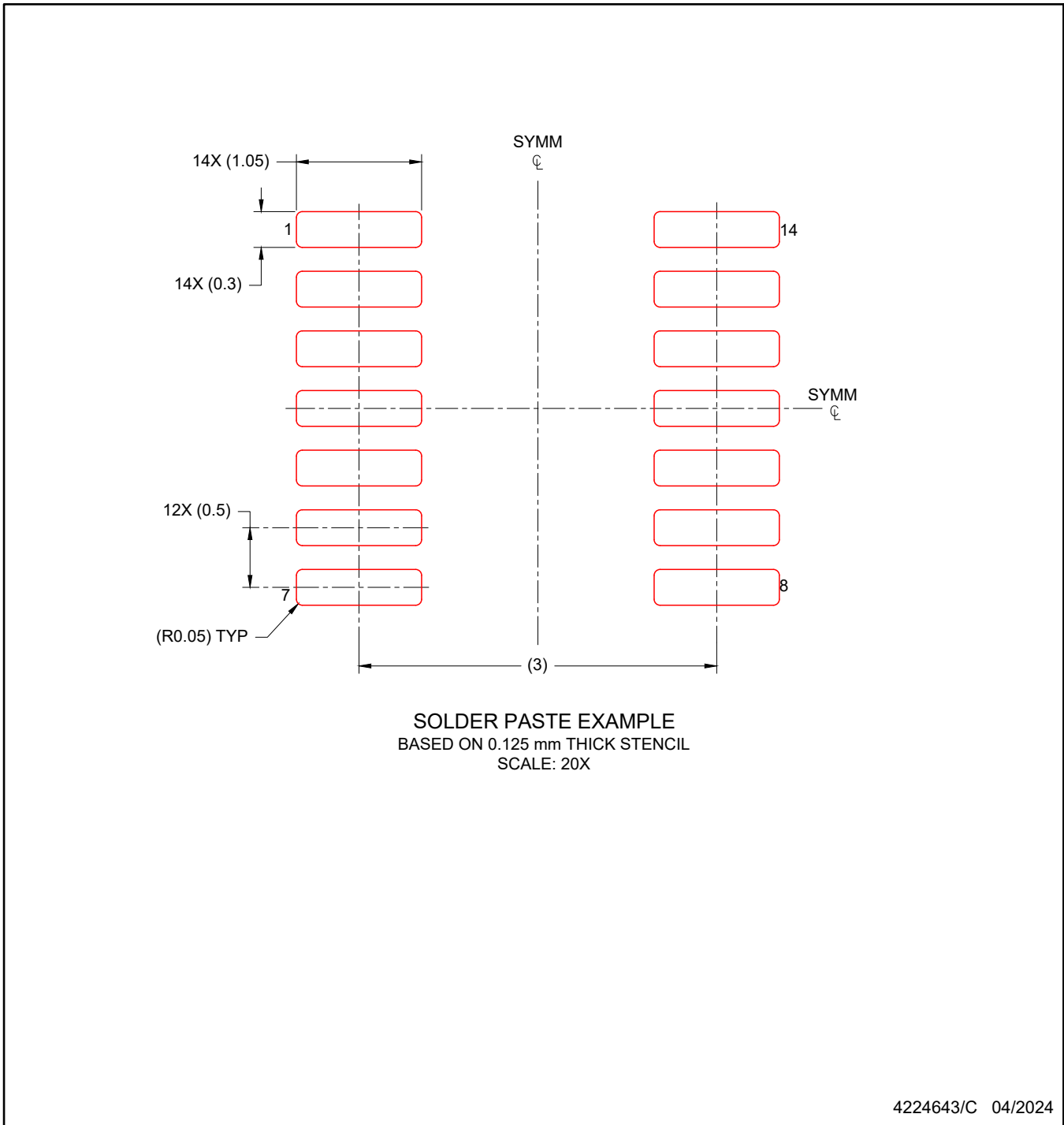
LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE: 20X



4224643/C 04/2024

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



4224643/C 04/2024

NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.





# EXAMPLE BOARD LAYOUT

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214839/J 02/2024

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/J 02/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

D (R-PDSO-G14)

PLASTIC SMALL OUTLINE





- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  - $\triangle C$  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
  - $\triangle D$  Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
  - E. Reference JEDEC MS-012 variation AB.

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  -  C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
  -  D. Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
  - E. Falls within JEDEC MO-153

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

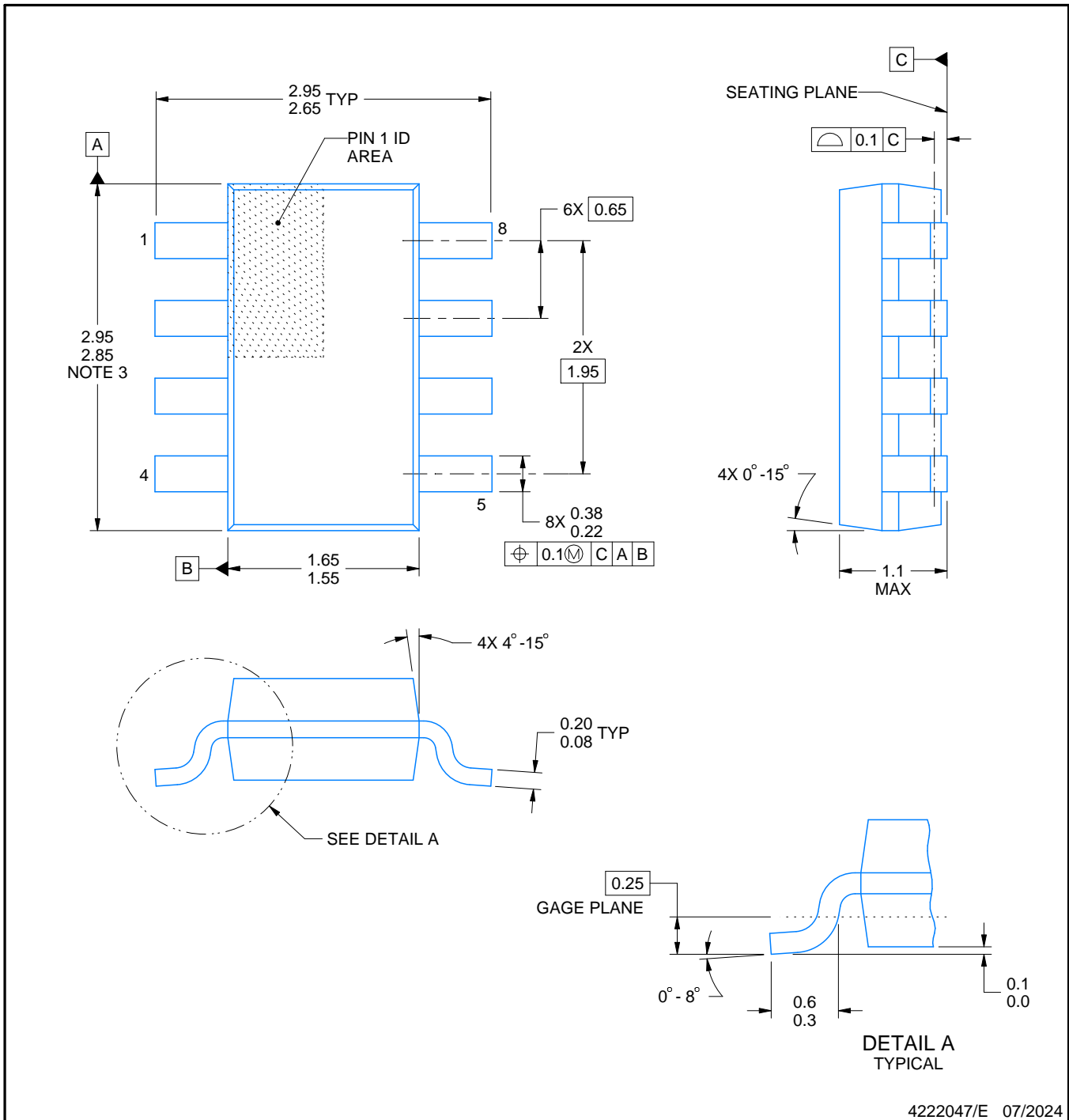
# DDF0008A



# PACKAGE OUTLINE

## SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



4222047/E 07/2024

### NOTES:

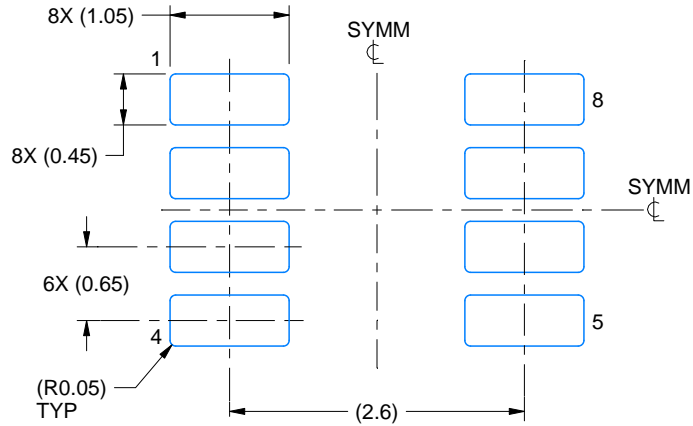
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.

# EXAMPLE BOARD LAYOUT

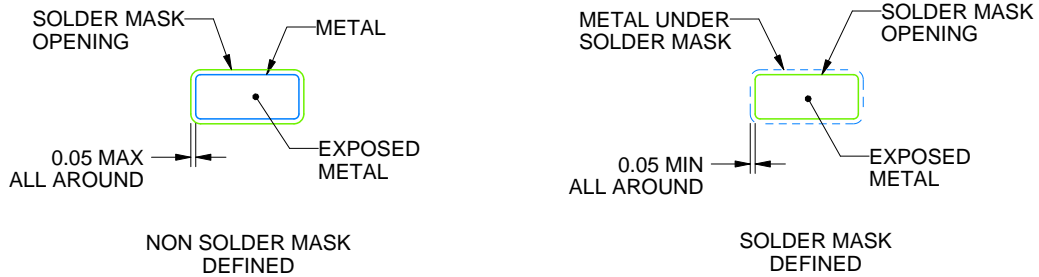
DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4222047/E 07/2024

NOTES: (continued)

- 4. Publication IPC-7351 may have alternate designs.
- 5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



# EXAMPLE STENCIL DESIGN

DDF0008A

SOT-23-THIN - 1.1 mm max height

PLASTIC SMALL OUTLINE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4222047/E 07/2024

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
7. Board assembly site may have different recommendations for stencil design.



# EXAMPLE BOARD LAYOUT

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



LAND PATTERN EXAMPLE  
 EXPOSED METAL SHOWN  
 SCALE:8X



SOLDER MASK DETAILS

4214825/C 02/2019

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

D0008A

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



SOLDER PASTE EXAMPLE  
BASED ON .005 INCH [0.125 MM] THICK STENCIL  
SCALE:8X

4214825/C 02/2019

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

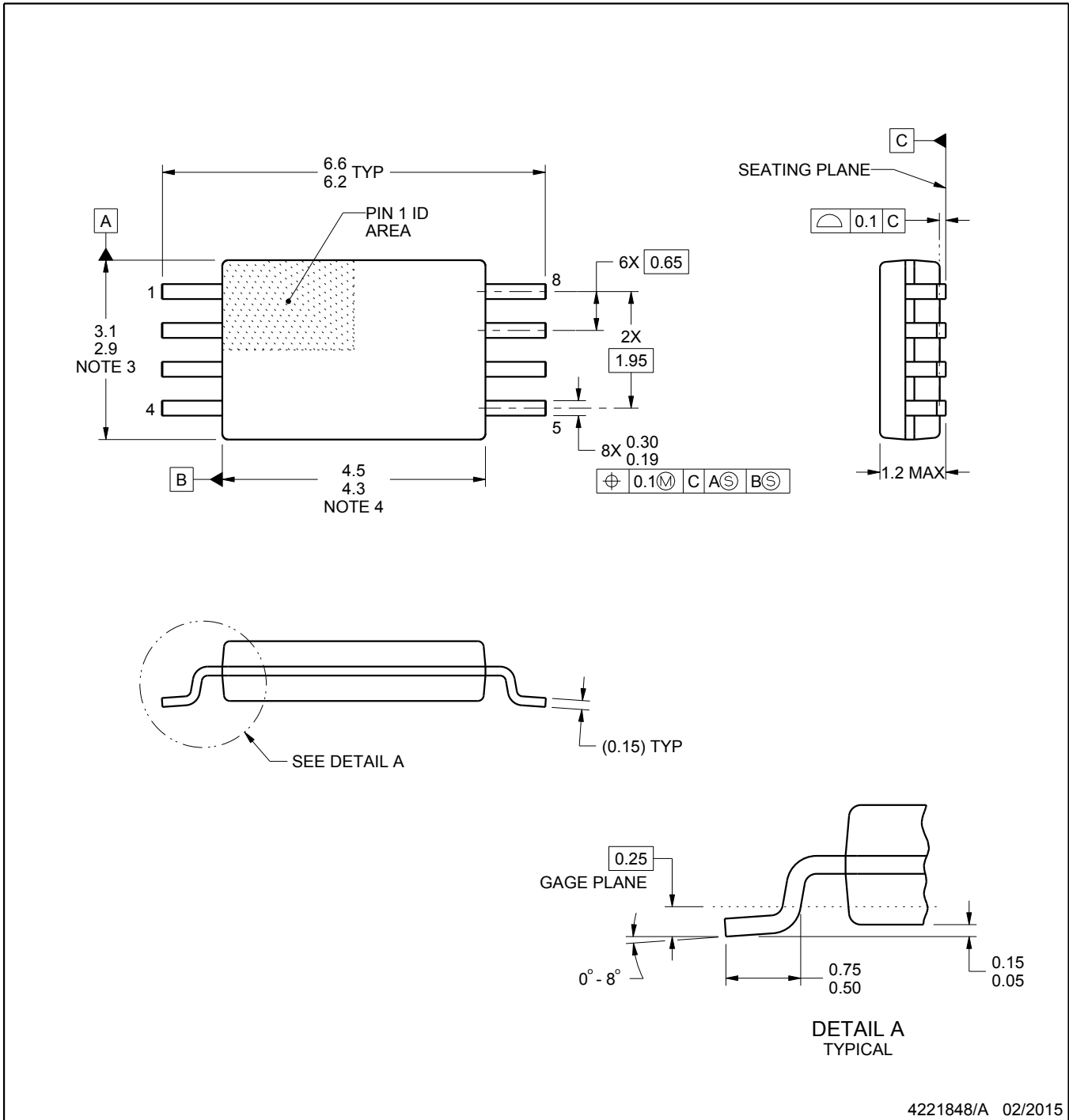
PW0008A



PACKAGE OUTLINE

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
5. Reference JEDEC registration MO-153, variation AA.

# EXAMPLE BOARD LAYOUT

PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



LAND PATTERN EXAMPLE  
SCALE:10X



SOLDER MASK DETAILS  
NOT TO SCALE

4221848/A 02/2015

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

PW0008A

TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:10X

4221848/A 02/2015

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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