

# The RS-485 unit load and maximum number of bus connections

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## Introduction

TIA/EIA-485 (RS-485) is a popular electrical standard for data interchange over a multipoint differential bus. Multipoint buses are three or more stations connected to a common transmission medium that allow bidirectional data communication between any two nodes. Figure 1 schematically shows an example of a multipoint bus.

Maintaining a practical limit to the output-drive capability of an RS-485 driver requires that a limit be imposed on the steady-state load presented by the bus. This in turn constrains the input resistance of stations and, ultimately, the maximum number of connections.

RS-485 does not specify the maximum number of bus connections. Instead, the standard defines the steady-state electrical load presented by a bus connection in unit loads. The following paragraphs explain the unit load and how it is used to determine the maximum number of nodes connected to an RS-485 bus segment.

## The unit load

TIA/EIA-485-A defines a unit load as a 15-k $\Omega$  resistor connected to a -3- or 5-V source (see Figure 2). The -3-V case applies for positive input current, and the 5-V case applies for negative bus current. The definition and model are valid for input voltages from -7 to 12 V to account for driver outputs between 0 and 5 V, with up to  $\pm 7$  V of common-mode noise voltage between a driver and receiver.

Figure 2. Electrical model of 1 unit load

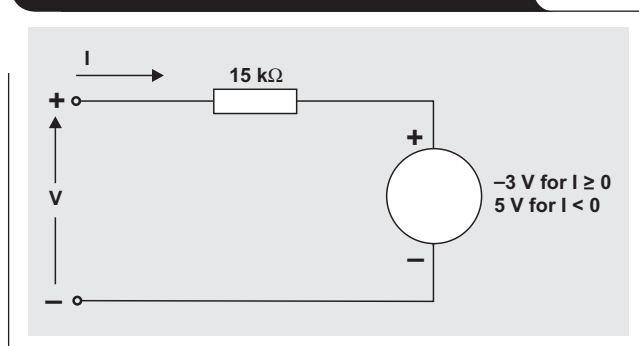
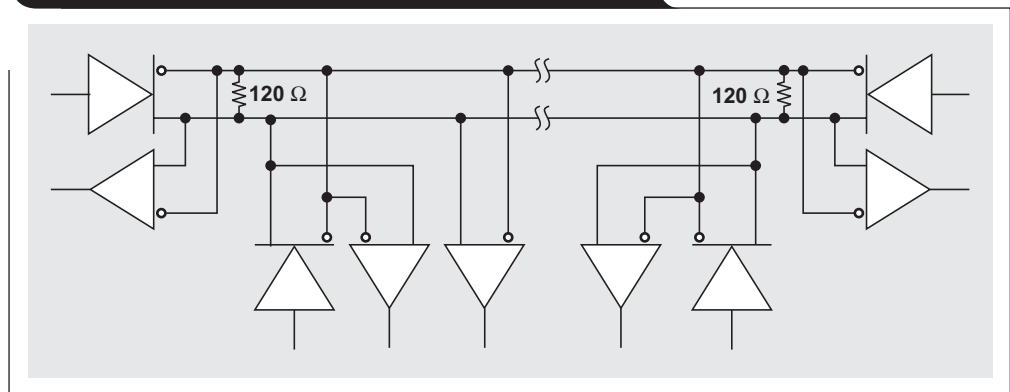


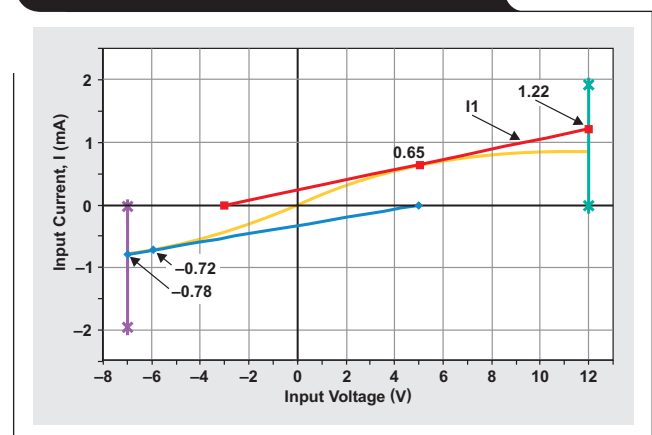
Figure 1. Schematic of an example multipoint bus



The number of unit loads (nUL) presented by any proposed connection to the RS-485 bus is then determined as the ratio of its measured input current and the current of 1 unit load. Since the current of 1 unit load is a function of voltage, the input current must be measured and the ratio determined throughout the entire -7- to 12-V input-voltage range, with the highest ratio determining the unit-load rating.

Figure 3 shows a hypothetical example where the measured input current of a circuit is nonlinear. It can be shown (see sidebar on next page) that, at its maximum value, the ratio of the measured and unit-load current is equal to the ratio of the slopes of the two functions and lies on a line with an intercept at -3 V for positive current and 5 V for negative current. Conceptually, this amounts to rotating a line pivoted at  $I = 0$  mA and  $V = -3$  V until it is tangent to the curve of measured positive current versus

Figure 3. Example unit-load analysis



**Proof that nUL is the slope ratios**

Let the input current of a unit load be defined by  $f_1(V)$  and the measured circuit by  $f_2(V)$ . The number of unit loads (nUL) is then

$$nUL = \frac{f_2(V)}{f_1(V)}$$

for  $-7\text{ V} < V < 12\text{ V}$ .

The maximum nUL occurs when the first derivative equals zero, or

$$\frac{d}{dV} \frac{f_2(V)}{f_1(V)} = \frac{1}{f_1(V)} \frac{d}{dV} f_2(V) - \frac{f_2(V)}{f_1^2(V)} \frac{d}{dV} f_1(V) = 0.$$

$$\frac{d}{dV} f_2(V) = \frac{f_2(V)}{f_1(V)} \frac{d}{dV} f_1(V).$$

$$\frac{f_2(V)}{f_1(V)} = \frac{\frac{d}{dV} f_2(V)}{\frac{d}{dV} f_1(V)}. \quad (1)$$

Therefore, the maximum nUL is equal to the ratio of the first derivative (slopes) of the input-current function.

The following equations are used to solve for the unit-load circuit:

$$f_1(V) = \frac{V+3}{15} \text{ mA or}$$

$$f_1(V) = \frac{V-5}{15} \text{ mA and } \frac{d}{dV} f_1(V) = \frac{1}{15} \text{ mho.}$$

Substituting these into Equation 1 yields

$$\frac{f_2(V)}{\frac{V+3}{15}} = \frac{\frac{d}{dV} f_2(V)}{\frac{1}{15}}$$

$$f_2(V) = \frac{d}{dV} f_2(V) \times (V+3)$$

or

$$\frac{f_2(V)}{\frac{V-5}{15}} = \frac{\frac{d}{dV} f_2(V)}{\frac{1}{15}}$$

$$f_2(V) = \frac{d}{dV} f_2(V) \times (V-5).$$

These line equations mean that the input current where the nUL is maximum lies on a line that intersects the points  $I = 0\text{ mA}$  and  $V = -3\text{ V}$  for positive current and  $I = 0\text{ mA}$  and  $V = 5\text{ V}$  for negative current.

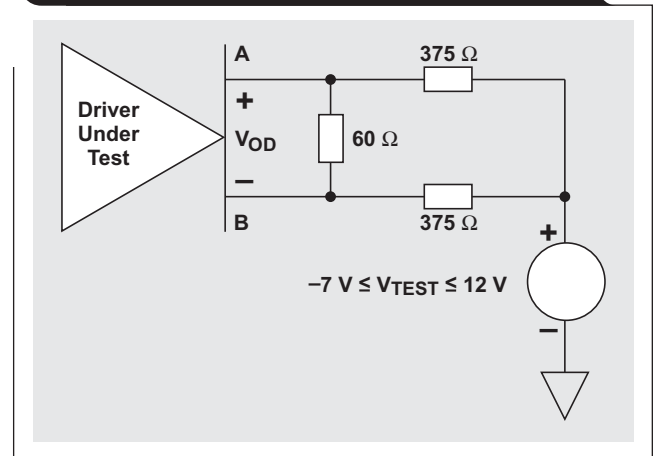
voltage. For negative currents, the line is pivoted at  $I = 0\text{ mA}$  and  $V = 5\text{ V}$ . In our example, the maximum ratio occurs at measured input currents of  $0.65\text{ mA}$  and  $-0.72\text{ mA}$ .

The ratio and nUL may be calculated by dividing the measured value at the intercept by the value derived from solving the unit-load circuit; or, for convenience, the lines are often extended to the  $12\text{-}$  or  $-7\text{-V}$  intercept. Since the slopes for 1 unit load and the tangential lines are constants, their ratios are constant and may be determined at any voltage. By definition, the current into 1 unit load at  $12\text{ V}$  will be  $1\text{ mA}$ , and at  $-7\text{ V}$  will be  $-0.8\text{ mA}$ . These values are respectively divided into the current-intercept values of the tangential lines at  $12\text{ V}$  and  $-7\text{ V}$ , and the maximum number determines the nUL for the circuit. In the example, the input-current-versus-voltage characteristics of the hypothetical circuit result in  $1.22$  unit loads.

**Maximum unit loads**

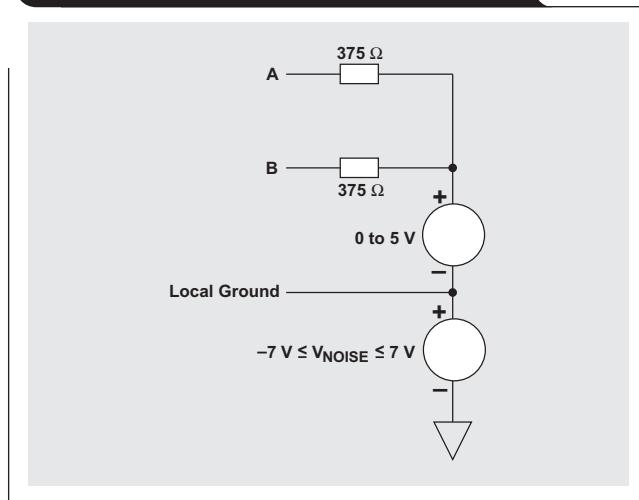
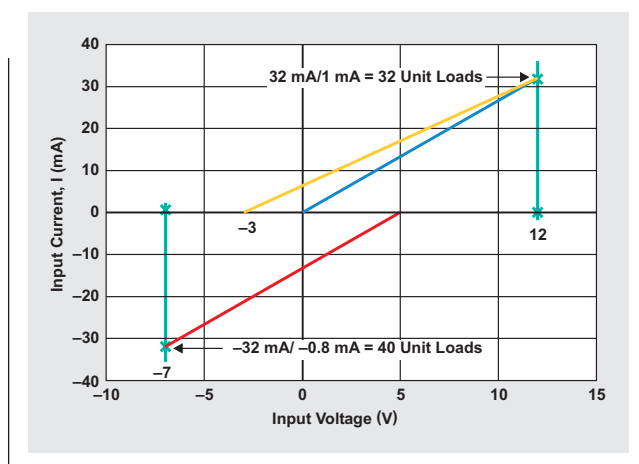
The minimum output-drive capability of a standard RS-485 driver is established in clause 4.2.3 of TIA/EIA-485-A, which specifies a differential output voltage of at least  $1.5\text{ V}$  with a common-mode load. Figure 4 shows a schematic of this test circuit.

**Figure 4. Differential output voltages with a common-mode load**



The  $375\text{-}\Omega$  resistors are certainly part of the common-mode load. What is not obvious is that the test voltage of  $-7$  to  $12\text{ V}$  actually represents a  $\pm 7\text{-V}$  common-mode noise source and a  $0$ - to  $5\text{-V}$  local supply voltage at the load(s). This is important in that the local supply is included in the unit-load determination for this test circuit. Figure 5 shows the common-mode test circuit with the insertion of a “local” ground used as the reference for the unit-load calculation.

To determine the unit load of this test circuit, we plot the input-current-versus-voltage function between point A or B and the “local” ground of Figure 5, then apply the unit-load definition described earlier. This is done in Figure 6, and we find that the current at the intercepts of the tangential lines is  $32\text{ mA}$  at  $V = 12\text{ V}$ , and  $-32\text{ mA}$  at  $V = -7\text{ V}$ . By definition, this represents  $32$  unit loads and  $40$  unit loads, respectively.

**Figure 5. Physical representation of the test circuit****Figure 6. Unit load of common-mode test circuit**

The reader may have noted the discrepancy between the unit-load model and the driver test circuit. One can only assume that this was an oversight or compromise by the authors of TIA/EIA-485. As tested, the unit-load model should consist of a 12-k $\Omega$  resistor to a 0- to 5-V source rather than 15 k $\Omega$  to a -3- to 5-V source. If we use this modified definition, the differential output voltage with common-mode load test of TIA/EIA-485-A ensures that a standard driver will work with 32 unit loads.

### Using the unit load

Other than a refresher on analytic geometry, of what use is the unit-load concept to the designer of a data-interchange circuit? Primarily, it provides a single standard parameter for calculating the maximum number of connections and for specifying the input characteristics of possible line circuits. Since we know a driver will support 32 unit loads in a standard bus configuration, we need only divide 32 by the total number of nodes (N) to derive the maximum

unit-load rating for each of the line circuits. For example, if 48 nodes were to be connected, each line receiver or transceiver would have to have no more than 0.67 unit loads (32/48).

The unit load also can be useful when nonstandard bus configurations are implemented. In addition to the differential termination of the differential signal pair, pull-up and pull-down resistors often are connected to the lines to provide a known bus state when all of the connected drivers are idle. The resistor values used for this fail-safe termination are usually around 1 k $\Omega$ . If so, this termination would consume 12 unit loads (12 mA at 12 V) out of the budget of 32 unit loads. This leaves 20 unit loads for the line circuits; and, if 48 nodes are still to be connected, each of the line circuits must now be no more than 0.42 unit loads (20/48).

Texas Instruments (TI) offers numerous options, some of which are shown in Table 1, for supporting a large number of RS-485 bus connections.

**Table 1. Fractional unit-load devices from TI**

UNIT LOADS	MAXIMUM NUMBER OF DEVICES ON A SINGLE BUS SEGMENT	PART NUMBER
0.5	64	SN65HVD05
		SN65HVD10
		SN65HVD20
		SN65HVD23
0.25	128	SN65LBC182
		SN65LBC184
0.125	256	SN65HVD06
		SN65HVD07
		SN65HVD08
		SN65HVD11
		SN65HVD12
		SN65HVD21
		SN65HVD22
		SN65HVD24

### Conclusion

The unit load is a relative parameter that provides a basis for determining the maximum number of connections to an RS-485 bus segment or for specifying the input characteristics of line circuits. A standard RS-485 driver will handle 32 unit loads that could consist of 256 devices with a rating of  $\frac{1}{8}$  unit load.

### Related Web sites

[analog.ti.com](http://analog.ti.com)

[www.ti.com/sc/device/partnumber](http://www.ti.com/sc/device/partnumber)

Replace *partnumber* with SN65HVD05, SN65HVD06, SN65HVD07, SN65HVD08, SN65HVD10, SN65HVD11, SN65HVD12, SN65HVD20, SN65HVD21, SN65HVD22, SN65HVD23, SN65HVD24, SN65LBC182 or SN65LBC184

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