

[SN55LVDS31](https://www.ti.com/product/SN55LVDS31), [SN65LVDS31](https://www.ti.com/product/SN65LVDS31), [SN65LVDS3487](https://www.ti.com/product/SN65LVDS3487), [SN65LVDS9638](https://www.ti.com/product/SN65LVDS9638) SLLS261N – JULY 1997 – REVISED APRIL 2021

SNx5LVDSxx High-Speed Differential Line Drivers

1 Features

- Meet or Exceed the Requirements of ANSI TIA/ EIA-644 Standard
- Low-Voltage Differential Signaling With Typical Output Voltage of 350 mV and 100-Ω Load
- Typical Output Voltage Rise and Fall Times of 500 ps (400 Mbps)
- Typical Propagation Delay Times of 1.7 ns
- Operate From a Single 3.3-V Supply
- Power Dissipation 25 mW Typical Per Driver at 200 MHz
- Driver at High-Impedance When Disabled or With $V_{CC} = 0$
- Bus-Terminal ESD Protection Exceeds 8 kV
- Low-Voltage TTL (LVTTL) Logic Input Levels
- Pin Compatible With AM26LS31, MC3487, and μA9638
- Cold Sparing for Space and High-Reliability Applications Requiring Redundancy

2 Applications

- [Wireless Infrastructure](https://www.ti.com/applications/communications-equipment/wireless-infrastructure/overview.html)
- **[Telecom Infrastructure](https://www.ti.com/solution/merchant-telecom-rectifiers)**
- **[Printers](https://www.ti.com/solution/home-printer)**

3 Description

The SN55LVDS31, SN65LVDS31, SN65LVDS3487, and SN65LVDS9638 devices are differential line drivers that implement the electrical characteristics of low-voltage differential signaling (LVDS). This signaling technique lowers the output voltage levels of 5-V differential standard levels (such as TIA/ EIA-422B) to reduce the power, increase the switching speeds, and allow operation with a 3.3-V supply rail. Any of the four current-mode drivers will deliver a minimum differential output voltage magnitude of 247 mV into a 100-Ω load when enabled.

Device Information(1)

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Equivalent Input and Output Schematic Diagrams

An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, $\overline{\textbf{44}}$ intellectual property matters and other important disclaimers. PRODUCTION DATA.

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4 Revision History

5 Description (Continued)

The intended application of these devices and signaling technique is both point-to-point and multidrop (one driver and multiple receivers) data transmission over controlled impedance media of approximately 100 Ω. The transmission media may be printed-circuit board traces, backplanes, or cables. The ultimate rate and distance of data transfer is dependent upon the attenuation characteristics of the media and the noise coupling to the environment.

The SN65LVDS31, SN65LVDS3487, and SN65LVDS9638 devices are characterized for operation from –40°C to 85°C. The SN55LVDS31 device is characterized for operation from –55°C to 125°C.

6 Pin Configuration and Functions

Table 6-1. Pin Functions: SN55LVDS31 J or W, SN65LVDS31 D or PW

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Table 6-1. Pin Functions: SN55LVDS31 J or W, SN65LVDS31 D or PW (continued)

Table 6-2. Pin Functions: SN65LVDS31FK

Table 6-3. Pin Functions: SN65LVDS3487D

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Table 6-3. Pin Functions: SN65LVDS3487D (continued)

Table 6-4. Pin Functions: SN65LVDS9638D, SN65LVDS9638DGN, SN65LVDS9638DGK

7 Specifications

7.1 Absolute Maximum Ratings(1)

over operating free-air temperature range (unless otherwise noted)

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Section 7.3* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltages, except differential I/O bus voltages, are with respect to the network ground terminal.

7.2 ESD Ratings

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

7.4 Thermal Information

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[SN55LVDS31,](https://www.ti.com/product/SN55LVDS31) [SN65LVDS31,](https://www.ti.com/product/SN65LVDS31) [SN65LVDS3487,](https://www.ti.com/product/SN65LVDS3487) [SN65LVDS9638](https://www.ti.com/product/SN65LVDS9638) SLLS261N – JULY 1997 – REVISED APRIL 2021 **www.ti.com**

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953.](https://www.ti.com/lit/pdf/spra953)

(2) The PowerPAD™ must be soldered to a thermal land on the printed-circuit board. See the application note *PowerPAD Thermally Enhanced Package* [\(SLMA002](https://www.ti.com/lit/pdf/SLMA002)).

7.5 Electrical Characteristics: SN55LVDS31

over operating free-air temperature range (unless otherwise noted)

(1) All typical values are at $T_A = 25^{\circ}$ C and with $V_{CC} = 3.3$ V.

7.6 Electrical Characteristics: SN65LVDSxxxx

over recommended operating conditions (unless otherwise noted)

(1) All typical values are at $T_A = 25^{\circ}$ C and with $V_{CC} = 3.3$ V.

7.7 Switching Characteristics: SN55LVDS31

over recommended operating conditions (unless otherwise noted)

(1) All typical values are at $T_A = 25^{\circ}$ C and with $V_{CC} = 3.3$ V.

(2) $t_{sk(o)}$ is the maximum delay time difference between drivers on the same device.

7.8 Switching Characteristics: SN65LVDSxxxx

over recommended operating conditions (unless otherwise noted)

(1) All typical values are at $T_A = 25^{\circ}$ C and with $V_{CC} = 3.3$ V.

(2) $t_{sk(o)}$ is the skew between specified outputs of a single device with all driving inputs connected together and the outputs switching in the same direction while driving identical specified loads.

 $t_{sk(pp)}$ is the magnitude of the difference in propagation delay times between any specified terminals of two devices when both devices operate with the same supply voltages, same temperature, and have identical packages and test circuits.

7.9 Typical Characteristics

8 Parameter Measurement Information

8.1

Figure 8-1. Voltage and Current Definitions

- NOTES: A. All input pulses are supplied by a generator having the following characteristics: t_r or $t_f \le 1$ ns, pulse repetition rate (PRR) = 50 Mpps, pulse width = 10 ± 0.2 ns.
	- B. C_L includes instrumentation and fixture capacitance within 6 mm of the D.U.T.

Figure 8-2. Test Circuit, Timing, and Voltage Definitions for the Differential Output Signal

- NOTES: A. All input pulses are supplied by a generator having the following characteristics: t_r or t_f ≤ 1 ns, pulse repetition rate (PRR) = 50 Mpps, pulse width = 10 ± 0.2 ns.
	- B. C_L includes instrumentation and fixture capacitance within 6 mm of the D.U.T.
	- C. The measurement of $V_{\text{OC(PP)}}$ is made on test equipment with a -3-dB bandwidth of at least 300 MHz.

Figure 8-3. Test Circuit and Definitions for the Driver Common-Mode Output Voltage

- NOTES: A. All input pulses are supplied by a generator having the following characteristics: t_r or t_f < 1 ns, pulse repetition rate (PRR) = 0.5 Mpps, pulse width = 500 ± 10 ns.
	- B. C_L includes instrumentation and fixture capacitance within 6 mm of the D.U.T.

Figure 8-4. Enable or Disable Time Circuit and Definitions

9 Detailed Description

9.1 Overview

The SNx5LVDSxx devices are dual- and quad-channel LVDS line drivers. They operate from a single supply that is nominally 3.3 V, but can be as low as 3 V and as high as 3.6 V. The input signal to the SN65LVDS1 device is an LVTTL signal. The output of the device is a differential signal complying with the LVDS standard (TIA/ EIA-644A). The differential output signal operates with a signal level of 340 mV, nominally, at a common-mode voltage of 1.2 V. This low differential output voltage results in a low emitted radiated energy, which is dependent on the signal slew rate. The differential nature of the output provides immunity to common-mode coupled signals.

The SNx5LVDSxx devices are intended to drive a 100-Ω transmission line. This transmission line may be a printed-circuit board (PCB) or cabled interconnect. With transmission lines, the optimum signal quality and power delivery is reached when the transmission line is terminated with a load equal to the characteristic impedance of the interconnect. Likewise, the driven 100-Ω transmission line should be terminated with a matched resistance.

9.2 Functional Block Diagram

'LVDS31 logic diagram (positive logic)

SN65LVDS3487 logic diagram (positive logic)

SN65LVDS9638 logic diagram (positive logic)

9.3 Feature Description

9.3.1 Driver Disabled Output

When the SNx5LVDSxx driver is disabled, or when power is removed from the device, the driver outputs are high-impedance.

9.3.2 NC Pins

NC (not connected) pins are pins where the die is not physically connected to the lead frame or package. For optimum thermal performance, a good rule of thumb is to ground the NC pins at the board level.

9.3.3 Unused Enable Pins

Unused enable pins should be tied to V_{CC} or GND as appropriate.

9.3.4 Driver Equivalent Schematics

The driver input is represented by a CMOS inverter stage with a 7-V Zener diode. The input stage is highimpedance, and includes an internal pulldown to ground. If the driver input is left open, the driver input provides

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a low-level signal to the rest of the driver circuitry, resulting in a low-level signal at the driver output pins. The Zener diode provides ESD protection. The driver output stage is a differential pair, one half of which is shown in Figure 9-1. Like the input stage, the driver output includes Zener diodes for ESD protection. The schematic shows an output stage that includes a set of current sources (nominally 3.5 mA) that are connected to the output load circuit based upon the input stage signal. To the first order, the SNx5LVDSxx output stage acts a constant-current source.

Figure 9-1. Equivalent Input and Output Schematic Diagrams

9.4 Device Functional Modes

Table 9-1. SN55LVDS31, SN65LVDS31(1)

(1) $H = high level, L = low level, X = irrelevant, Z = high-impedance$ (off)

Table 9-2. SN65LVDS3487(1)

(1) $H = high level, L = low level, X = irrelevant, Z = high-impedance$ (off)

Table 9-3. SN65LVDS9638(1)

(1) $H = high level, L = low level$

10 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

10.1 Application Information

The SNx5LVDSxx devices are dual- and quad-channel LVDS drivers. These devices are generally used as building blocks for high-speed, point-to-point, data transmission where ground differences are less than 1 V. LVDS drivers and receivers provide high-speed signaling rates that are often implemented with ECL class devices without the ECL power and dual-supply requirements. A common question with any class of driver is how far and how fast can the devices operate. While individual drivers and receivers have specifications that define their inherent switching rate, a communication link will quite often be limited by the impairments introduced by the interconnecting media. Figure 10-1 shows the typical relationship between signaling rate and distance achievable depends on the quality of the eye pattern at the receiver that is either desired or needed. Figure 10-1 shows the curves representing 5% and 30% eye closure due to inter-symbol interference (ISI).

A. This parameter is the percentage of distortion of the unit interval (UI) with a pseudorandom data pattern.

Figure 10-1. Typical Transmission Distance vs Signaling Rate

10.2 Typical Application

10.2.1 Point-to-Point Communications

The most basic application for LVDS buffers, as found in this data sheet, is for point-to-point communications of digital data, as shown in [Figure 10-2](#page-18-0).

Figure 10-2. Point-to-Point Topology

A point-to-point communications channel has a single transmitter (driver) and a single receiver. This communications topology is often referred to as simplex. In Figure 10-2 the driver receives a single-ended input signal and the receiver outputs a single-ended recovered signal. The LVDS driver converts the single-ended input to a differential signal for transmission over a balanced interconnecting media of 100-Ω characteristic impedance. The conversion from a single-ended signal to an LVDS signal retains the digital data payload while translating to a signal whose features are more appropriate for communication over extended distances or in a noisy environment.

10.2.1.1 Design Requirements

10.2.1.2 Detailed Design Procedure

10.2.1.2.1 Driver Supply Voltage

The SNx5LVDSxx driver is operated from a single supply. The device can support operation with a supply as low as 3 V and as high as 3.6 V. The differential output voltage is nominally 340 mV over the complete output range. The minimum output voltage stays within the specified LVDS limits (247 mV to 454 mV) for a 3.3-V supply.

10.2.1.2.2 Driver Bypass Capacitance

Bypass capacitors play a key role in power distribution circuitry. Specifically, they create low-impedance paths between power and ground. At low frequencies, a good digital power supply offers very-low-impedance paths between its terminals. However, as higher frequency currents propagate through power traces, the source is quite often incapable of maintaining a low-impedance path to ground. Bypass capacitors are used to address this shortcoming. Usually, large bypass capacitors (10 to 1000 μF) at the board-level do a good job up into the kHz range. Due to their size and length of their leads, they tend to have large inductance values at the switching frequencies of modern digital circuitry. To solve this problem, one should resort to the use of smaller capacitors (nF to μF range) installed locally next to the integrated circuit.

Multilayer ceramic chip or surface-mount capacitors (size 0603 or 0805) minimize lead inductances of bypass capacitors in high-speed environments, because their lead inductance is about 1 nH. For comparison purposes, a typical capacitor with leads has a lead inductance around 5 nH.

The value of the bypass capacitors used locally with LVDS chips can be determined by the following formula according to Johnson^{[1](#page-19-0)}, equations 8.18 to 8.21. A conservative rise time of 200 ps and a worst-case change in supply current of 1 A covers the whole range of LVDS devices offered by Texas Instruments. In this example,

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the maximum power supply noise tolerated is 200 mV; however, this figure varies depending on the noise budget available in your design. ¹

$$
C_{\text{chip}} = \left(\frac{\Delta \text{Imaximum Step Change Supply Current}}{\Delta \text{Varimum Power Supply Noise}}\right) \times T_{\text{Rise Time}}
$$
\n
$$
C_{\text{LVDS}} = \left(\frac{1A}{0.2V}\right) \times 200 \text{ ps} = 0.001 \,\mu\text{F}
$$
\n
$$
(2)
$$

The following example lowers lead inductance and covers intermediate frequencies between the board-level capacitor (>10 µF) and the value of capacitance found above (0.001 µF). You should place the smallest value of capacitance as close as possible to the chip.

Figure 10-3. Recommended LVDS Bypass Capacitor Layout

10.2.1.2.3 Driver Output Voltage

The SNx5LVDSxx driver output is a 1.2-V common-mode voltage, with a nominal differential output signal of 340 mV. This 340 mV is the absolute value of the differential swing (V_{OD} = $|V^+ - V^-|$). The peak-to-peak differential voltage is twice this value, or 680 mV.

10.2.1.2.4 Interconnecting Media

The physical communication channel between the driver and the receiver may be any balanced paired metal conductors meeting the requirements of the LVDS standard, the key points which will be included here. This media may be a twisted pair, twinax, flat ribbon cable, or PCB traces. The nominal characteristic impedance of the interconnect should be between 100 Ω and 120 Ω with a variation of no more than 10% (90 Ω to 132 Ω).

10.2.1.2.5 PCB Transmission Lines

As per [SNLA187](https://www.ti.com/lit/pdf/SNLA187), [Figure 10-4](#page-20-0) depicts several transmission line structures commonly used in printed-circuit boards (PCBs). Each structure consists of a signal line and a return path with uniform cross-section along its length. A microstrip is a signal trace on the top (or bottom) layer, separated by a dielectric layer from its return path in a ground or power plane. A stripline is a signal trace in the inner layer, with a dielectric layer in between a ground plane above and below the signal trace. The dimensions of the structure along with the dielectric material properties determine the characteristic impedance of the transmission line (also called controlled-impedance transmission line).

When two signal lines are placed close by, they form a pair of coupled transmission lines. [Figure 10-4](#page-20-0) shows examples of edge-coupled microstrips, and edge-coupled or broad-side-coupled striplines. When excited by differential signals, the coupled transmission line is referred to as a differential pair. The characteristic impedance of each line is called odd-mode impedance. The sum of the odd-mode impedances of each line is the differential impedance of the differential pair. In addition to the trace dimensions and dielectric material properties, the spacing between the two traces determines the mutual coupling and impacts the differential impedance. When the two lines are immediately adjacent; for example, S is less than 2W, the differential pair is called a tightly-coupled differential pair. To maintain constant differential impedance along the length, it is important to keep the trace width and spacing uniform along the length, as well as maintain good symmetry between the two lines.

¹ Howard Johnson & Martin Graham.1993. High Speed Digital Design – A Handbook of Black Magic. Prentice Hall PRT. ISBN number 013395724.

Figure 10-4. Controlled-Impedance Transmission Lines

10.2.1.2.6 Termination Resistor

As shown earlier, an LVDS communication channel employs a current source driving a transmission line which is terminated with a resistive load. This load serves to convert the transmitted current into a voltage at the receiver input. To ensure incident wave switching (which is necessary to operate the channel at the highest signaling rate), the termination resistance should be matched to the characteristic impedance of the transmission line. The designer should ensure that the termination resistance is within 10% of the nominal media characteristic impedance. If the transmission line is targeted for 100-Ω impedance, the termination resistance should be between 90 and 110 $Ω$.

The line termination resistance should be located as close as possible to the receiver, thereby minimizing the stub length from the resistor to the receiver. The limiting case would be to incorporate the termination resistor into the receiver, which is exactly what is offered with a device like the SN65LVDT386. The SN65LVDT386 provides all the functionality and performance of the SN65LVDT386 receiver, with the added feature of an integrated termination load.

While we talk in this section about point-to-point communications, a word of caution is useful when a multidrop topology is used. In such topologies, line termination resistors are to be located only at the end(s) of the transmission line. In such an environment, SN65LVDT386 receivers could be used for loads branching off the main bus with an SN65LVDT386 used only at the bus end.

10.2.1.2.7 Driver NC Pins

NC (not connected) pins are pins where the die is not physically connected to the lead frame and package. For optimum thermal performance, a good rule of thumb is to ground the NC pins at the board level.

10.2.1.3 Application Curve

Figure 10-5. Typical Driver Output Eye Pattern in Point-to-Point System

10.2.2 Multidrop Communications

A second common application of LVDS buffers is a multidrop topology. In a multidrop configuration, a single driver and a shared bus are present along with two or more receivers (with a maximum permissible number of 32 receivers). Figure 10-6 shows an example of a multidrop system.

Figure 10-6. Multidrop Topology

10.2.2.1 Design Requirements

10.2.2.2 Detailed Design Procedure

10.2.2.2.1 Interconnecting Media

The interconnect in a multidrop system differs considerably from a point-to-point system. While point-to-point interconnects are straightforward and well understood, the bus type architecture encountered with multidrop systems requires more careful attention. We will use Figure 10-6 above to explore these details.

The most basic multidrop system would include a single driver, located at a bus origin, with multiple receiver nodes branching off the main line, and a final receiver at the end of the transmission line, co-located with a bus termination resistor. While this would be the most basic multidrop system, it has several considerations not yet explored.

The location of the transmitter at one bus end allows the design concerns to be simplified, but this comes at the cost of flexibility. With a transmitter located at the origin, a single bus termination at the far-end is required. The far-end termination absorbs the incident traveling wave. The flexibility lost with this arrangement is thus: if the single transmitter needed to be relocated on the bus, at any location other than the origin, we would be faced with a bus with one open-circuited end, and one properly terminated end. Locating the transmitter say in the middle of the bus may be desired to reduce (by $\frac{1}{2}$) the maximum flight time from the transmitter to receiver.

Another new feature in [Figure 10-6](#page-21-0) is clear in that every node branching off the main line results in stubs. The stubs should be minimized in any case, but have the unintended effect of locally changing the loaded impedance of the bus.

To a good approximation, the characteristic transmission line impedance seen into any cut point in the unloaded multipoint or multidrop bus is defined by \sqrt{LC} , where L is the inductance per unit length and C is the capacitance per unit length. As capacitance is added to the bus in the form of devices and interconnections, the bus characteristic impedance is lowered. This may result in signal reflections from the impedance mismatch between the unloaded and loaded segments of the bus.

If the number of loads is constant and can be distributed evenly along the line, reflections can be reduced by changing the bus termination resistors to match the loaded characteristic impedance. Normally, the number of loads are not constant or distributed evenly and the reflections resulting from any mismatching should be accounted for in the noise budget.

10.2.2.3 Application Curve

Figure 10-7. Typical Driver Output Eye Pattern in Multi-Drop System

11 Power Supply Recommendations

11.1

The LVDS drivers in this data sheet are designed to operate from a single power supply, with supply voltages in the range of 3.0 V to 3.6 V. In a typical application, a driver and a receiver may be on separate boards or even separate equipment. In these cases, separate supplies would be used at each location. The expected ground potential difference between the driver power supply and the receiver power supply would be less than |±1 V|. Board-level and local device-level bypass capacitance should be used and are covered in *[Section 10.2.1.2.2](#page-18-0)*.

12 Layout

12.1 Layout Guidelines

12.1.1 Microstrip vs. Stripline Topologies

As per [SLLD009,](https://www.ti.com/lit/pdf/SLLD009) printed-circuit boards usually offer designers two transmission line options: Microstrip and stripline. Microstrips are traces on the outer layer of a PCB, as shown in Figure 12-1.

Figure 12-1. Microstrip Topology

On the other hand, striplines are traces between two ground planes. Striplines are less prone to emissions and susceptibility problems because the reference planes effectively shield the embedded traces. However, from the standpoint of high-speed transmission, juxtaposing two planes creates additional capacitance. TI recommends routing LVDS signals on microstrip transmission lines, if possible. The PCB traces allow designers to specify the necessary tolerances for Z_O based on the overall noise budget and reflection allowances. Footnotes 1², 2³, and 3⁴ provide formulas for Z_O and t_{PD} for differential and single-ended traces. ^{2 3 4}

Figure 12-2. Stripline Topology

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² Howard Johnson & Martin Graham.1993. High Speed Digital Design – A Handbook of Black Magic. Prentice Hall PRT. ISBN number 013395724.

³ Mark I. Montrose. 1996. Printed Circuit Board Design Techniques for EMC Compliance. IEEE Press. ISBN number 0780311310.

⁴ Clyde F. Coombs, Jr. Ed, Printed Circuits Handbook, McGraw Hill, ISBN number 0070127549.

12.1.2 Dielectric Type and Board Construction

The speeds at which signals travel across the board dictates the choice of dielectric. FR-4, or equivalent, usually provides adequate performance for use with LVDS signals. If rise or fall times of TTL/CMOS signals are less than 500 ps, empirical results indicate that a material with a dielectric constant near 3.4, such as Rogers™ 4350 or Nelco N4000-13 is better suited. Once the designer chooses the dielectric, there are several parameters pertaining to the board construction that can affect performance. The following set of guidelines were developed experimentally through several designs involving LVDS devices:

- Copper weight: 15 g or 1/2 oz start, plated to 30 g or 1 oz
- All exposed circuitry should be solder-plated (60/40) to 7.62 μm or 0.0003 in (minimum).
- Copper plating should be 25.4 μm or 0.001 in (minimum) in plated-through-holes.
- Solder mask over bare copper with solder hot-air leveling

12.1.3 Recommended Stack Layout

Following the choice of dielectrics and design specifications, you should decide how many levels to use in the stack. To reduce the TTL/CMOS to LVDS crosstalk, it is a good practice to have at least two separate signal planes as shown in Figure 12-3.

Layer 1: Routed Plane (LVDS Signals)
Layer 2: Ground Plane
Layer 3: Power Plane
Layer 4: Routed Plane (TTL/CMOS Signals)

Figure 12-3. Four-Layer PCB Board

Note

The separation between layers 2 and 3 should be 127 μm (0.005 in). By keeping the power and ground planes tightly coupled, the increased capacitance acts as a bypass for transients.

One of the most common stack configurations is the six-layer board, as shown in Figure 12-4.

Layer 1: Routed Plane (LVDS Signals)
Layer 2: Ground Plane
Layer 3: Power Plane
Layer 4: Ground Plane
Layer 5: Ground Plane
Layer 6: Routed Plane (TTL Signals)

Figure 12-4. Six-Layer PCB Board

In this particular configuration, it is possible to isolate each signal layer from the power plane by at least one ground plane. The result is improved signal integrity; however, fabrication is more expensive. Using the 6-layer board is preferable, because it offers the layout designer more flexibility in varying the distance between signal layers and referenced planes, in addition to ensuring reference to a ground plane for signal layers 1 and 6.

12.1.4 Separation Between Traces

The separation between traces depends on several factors; however, the amount of coupling that can be tolerated usually dictates the actual separation. Low-noise coupling requires close coupling between the differential pair of an LVDS link to benefit from the electromagnetic field cancellation. The traces should be 100-Ω differential and thus coupled in the manner that best fits this requirement. In addition, differential pairs should have the same electrical length to ensure that they are balanced, thus minimizing problems with skew and signal reflection.

In the case of two adjacent single-ended traces, one should use the 3-W rule, which stipulates that the distance between two traces should be greater than two times the width of a single trace, or three times its width

measured from trace center to trace center. This increased separation effectively reduces the potential for crosstalk. The same rule should be applied to the separation between adjacent LVDS differential pairs, whether the traces are edge-coupled or broad-side-coupled.

You should exercise caution when using autorouters, because they do not always account for all factors affecting crosstalk and signal reflection. For instance, it is best to avoid sharp 90° turns to prevent discontinuities in the signal path. Using successive 45° turns tends to minimize reflections.

12.1.5 Crosstalk and Ground Bounce Minimization

To reduce crosstalk, it is important to provide a return path to high-frequency currents that is as close as possible to its originating trace. A ground plane usually achieves this. Because the returning currents always choose the path of lowest inductance, they are most likely to return directly under the original trace, thus minimizing crosstalk. Lowering the area of the current loop lowers the potential for crosstalk. Traces kept as short as possible with an uninterrupted ground plane running beneath them emit the minimum amount of electromagnetic field strength. Discontinuities in the ground plane increase the return path inductance and should be avoided.

12.2 Layout Example

At least two or three times the width of an individual trace should separate single-ended traces and differential pairs to minimize the potential for crosstalk. Single-ended traces that run in parallel for less than the wavelength of the rise or fall times usually have negligible crosstalk. Increase the spacing between signal paths for long parallel runs to reduce crosstalk. Boards with limited real estate can benefit from the staggered trace layout, as shown in Figure 12-6.

Figure 12-6. Staggered Trace Layout

This configuration lays out alternating signal traces on different layers; thus, the horizontal separation between traces can be less than 2 or 3 times the width of individual traces. To ensure continuity in the ground signal path, TI recommends having an adjacent ground via for every signal via, as shown in [Figure 12-7](#page-27-0). Note that vias create additional capacitance. For example, a typical via has a lumped capacitance effect of 0.5 pF to 1 pF in FR4.

Figure 12-7. Ground Via Location (Side View)

Short and low-impedance connection of the device ground pins to the PCB ground plane reduces ground bounce. Holes and cutouts in the ground planes can adversely affect current return paths if they create discontinuities that increase returning current loop areas.

To minimize EMI problems, TI recommends avoiding discontinuities below a trace (for example, holes, slits, and so on) and keeping traces as short as possible. Zoning the board wisely by placing all similar functions in the same area, as opposed to mixing them together, helps reduce susceptibility issues.

13 Device and Documentation Support

13.1 Device Support

13.1.1 Other LVDS Products

For other products and application notes in the LVDS and LVDM product families visit our Web site at [http://](http://www.ti.com/sc/datatran) [www.ti.com/sc/datatran.](http://www.ti.com/sc/datatran)

13.2 Documentation Support

13.2.1 Related Information

IBIS modeling is available for this device. Contact the local TI sales office or the TI Web site at www.ti.com for more information.

For more application guidelines, see the following documents:

- *Low-Voltage Differential Signaling Design Notes* [\(SLLA014\)](https://www.ti.com/lit/pdf/SLLA014)
- *Interface Circuits for TIA/EIA-644* (LVDS) ([SLLA038\)](https://www.ti.com/lit/pdf/SLLA038)
- *Reducing EMI With LVDS* ([SLLA030\)](https://www.ti.com/lit/pdf/SLLA030)
- *Slew Rate Control of LVDS Circuits* [\(SLLA034](https://www.ti.com/lit/pdf/SLLA034))
- *Using an LVDS Receiver With RS-422 Data* [\(SLLA031](https://www.ti.com/lit/pdf/SLLA031))
- *Evaluating the LVDS EVM* [\(SLLA033](https://www.ti.com/lit/pdf/SLLA033))

13.2.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com.](https://www.ti.com) Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

13.2.3 Related Links

Table 13-1 lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

Table 13-1. Related Links

13.3 Support Resources

TI E2E™ [support forums](https://e2e.ti.com) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use.](https://www.ti.com/corp/docs/legal/termsofuse.shtml)

13.4 Trademarks

PowerPAD™ and TI E2E™ are trademarks of Texas Instruments. Rogers™ is a trademark of Rogers Corporation. All trademarks are the property of their respective owners.

13.5 Electrostatic Discharge Caution

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

13.6 Glossary

[TI Glossary](https://www.ti.com/lit/pdf/SLYZ022) This glossary lists and explains terms, acronyms, and definitions.

14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

FYAS

NSTRUMENTS

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

PACKAGE OPTION ADDENDUM

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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OTHER QUALIFIED VERSIONS OF SN55LVDS31, SN65LVDS31 :

- _●Catalog : <mark>[SN75LVDS31](http://focus.ti.com/docs/prod/folders/print/sn75lvds31.html)</mark>
- Enhanced Product : [SN65LVDS31-EP](http://focus.ti.com/docs/prod/folders/print/sn65lvds31-ep.html)
- _● Space : <mark>[SN55LVDS31-SP](http://focus.ti.com/docs/prod/folders/print/sn55lvds31-sp.html)</mark>

NOTE: Qualified Version Definitions:

- Catalog TI's standard catalog product
- Enhanced Product Supports Defense, Aerospace and Medical Applications
- Space Radiation tolerant, ceramic packaging and qualified for use in Space-based application

TEXAS

TAPE AND REEL INFORMATION

ISTRUMENTS

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

PACKAGE MATERIALS INFORMATION

www.ti.com 25-Sep-2024

TEXAS INSTRUMENTS

www.ti.com 25-Sep-2024

TUBE

B - Alignment groove width

GENERIC PACKAGE VIEW

DGN 8 PowerPAD VSSOP - 1.1 mm max height

3 x 3, 0.65 mm pitch SMALL OUTLINE PACKAGE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

4225482/A

PACKAGE OUTLINE

DGN0008D PowerPAD™ VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.

EXAMPLE BOARD LAYOUT

DGN0008D PowerPAD VSSOP - 1.1 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown
- on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.

EXAMPLE STENCIL DESIGN

DGN0008D PowerPAD VSSOP - 1.1 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.

 $W (R-GDFP-F16)$

CERAMIC DUAL FLATPACK

- NOTES: A. All linear dimensions are in inches (millimeters).
	- B. This drawing is subject to change without notice.
	- C. This package can be hermetically sealed with a ceramic lid using glass frit.
	- D. Index point is provided on cap for terminal identification only.
	- E. Falls within MIL STD 1835 GDFP2-F16

GENERIC PACKAGE VIEW

FK 20 LCCC - 2.03 mm max height

8.89 x 8.89, 1.27 mm pitch LEADLESS CERAMIC CHIP CARRIER

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.

 $J (R-GDIP-T**)$ 14 LEADS SHOWN

CERAMIC DUAL IN-LINE PACKAGE

NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- C. This package is hermetically sealed with a ceramic lid using glass frit.
- D. Index point is provided on cap for terminal identification only on press ceramic glass frit seal only.
- E. Falls within MIL STD 1835 GDIP1-T14, GDIP1-T16, GDIP1-T18 and GDIP1-T20.

PACKAGE OUTLINE

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.

EXAMPLE BOARD LAYOUT

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

D0008A SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.

PACKAGE OUTLINE

DGK0008A VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE

NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.

EXAMPLE BOARD LAYOUT

DGK0008A VSSOP - 1.1 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown
- on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.

EXAMPLE STENCIL DESIGN

DGK0008A VSSOP - 1.1 mm max height TM

SMALL OUTLINE PACKAGE

NOTES: (continued)

11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.

PACKAGE OUTLINE

NS0016A SOP - 2.00 mm max height

SOP

NOTES:

- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm, per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm, per side.

EXAMPLE BOARD LAYOUT

NS0016A SOP - 2.00 mm max height

SOP

NOTES: (continued)

5. Publication IPC-7351 may have alternate designs.

6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

NS0016A SOP - 2.00 mm max height

SOP

NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

8. Board assembly site may have different recommendations for stencil design.

 $D (R-PDSO-G16)$

PLASTIC SMALL OUTLINE

NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- 6 Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
- E. Reference JEDEC MS-012 variation AC.

PACKAGE OUTLINE

PW0016A TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-153.

EXAMPLE BOARD LAYOUT

PW0016A TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

EXAMPLE STENCIL DESIGN

PW0016A TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE

NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.

MECHANICAL DATA

PLASTIC SMALL-OUTLINE PACKAGE

NS (R-PDSO-G**) 14-PINS SHOWN

NOTES: All linear dimensions are in millimeters. А.

- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion, not to exceed 0,15.

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